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TRACE TRAJECTORY ANALYSIS AND ORBIT
DETERMINATION PROGRAM. VOLUME VII.
USER'S GUIDE, PART B: APPENDICES
(REISSUE B)

Willard D. Downs, III, et al

Aerospace Corporation

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Approved

A. R. Sims
A. R. Sims, Director
Mathematics and Programming
Subdivision
Information Processing Division
Engineering Science Operations

D. C. Walker
D. C. Walker, Senior Staff Engineer
Project Management Staff
Information Processing Division
Engineering Science Operations

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SB J. J. J.
Technical Advisor
SAMSO/TM

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19. KEY WORDS (Continued)

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description for each specific input item is given, and input data structures are shown. The Usage Guide is published in two parts, A and B.

The TRACE documentation series is summarized as follows:

Volume I:	General Program Objectives, Description, and Summary
Volume II:	Coordinate and Timekeeping Systems with Associated Transformations
Volume III:	Trajectory Generation Equations and Methods
Volume IV:	Measurement Data Generation and Observational Measurement Partial
Volume V:	Differential Correction Procedure and Techniques
Volume VI:	Orbital Statistics via Covariance Analysis
Volume VII:	Usage Guide, Parts A and B
Volume VIII:	Not to be published
Volume IX:	Detailed Program Structure
Volume X:	Lunar Gravity Analysis
Volume XI:	LGA Data Processor
Volume XII:	Sequential Least Squares Procedures and Techniques

PREFACE

Certain volumes of the TRACE documentation series were published by The Aerospace Corporation as Technical Operating Reports. Volume III: Trajectory Generation Equations and Methods was published as TOR-0066(9320)-2, Vol. III, and Volume V: Differential Correction Procedure and Techniques was published as TOR-0066(9320)-2, Vol. V.

Volume I: General Program Objectives, Description, and Summary was published as TR-0059(9320)-1, Vol. I, and Volume X: Lunar Gravity Analysis was published as TR-0059(9320)-1, Vol. X. Future volumes in this series will be published as Technical Reports.

This report is published in two parts, A and B.

The TRACE Program could not have been developed to its present status without the assistance of many people working in the fields of astrodynamics and software design. The authors acknowledge with gratitude and analysis and/or programming efforts of A. B. Bierman, R. J. Farrar, W. A. Feess, E. H. Fletcher, R. B. Freund, T. P. Gabbard, C. G. Gibson, P. T. Gray, P. T. Guttman, J. A. Pearson, C. M. Price, W. F. Rearick, N. W. Rhodus, A. J. Rusick, L. J. Tedeschi, L. Wong, and K. R. Young. In addition, consultations with W. T. Kyner, A. Troesch, and H. H. Wertz have led to many significant improvements and added capabilities in the program.

This report supersedes the appendices to TR-0059(9320)-1, Vol. VII,
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APPENDIX A

DESCRIPTION OF THE GENERAL-PURPOSE INPUT ROUTINE GAIL1

A. 1 FUNCTION AND CAPABILITIES

A. 1. 1 Purpose and Description

The purpose of GAIL1* is to read a set of Hollerith punched data and/or header cards into core with one FORTRAN call statement. To achieve this, the data fields are converted to binary, while the header information is stored in Hollerith code; each piece of the data is converted and stored according to a specific conversion code. These data may be integers, real variables, arrays, alphanumeric data (short or long headers), matrices, or end-of-case indications.

The data cards can be printed as received, or they can be placed on a scratch I/O device and then listed when an end of file (EOF) is detected on the input file.

The subroutine will always return control to the driver program except in the case of tape errors, system malfunctions, or completely erroneous punched data cards that disobey all FORTRAN I/O format rules. Therefore, the user must supply and test a status cell after an exit from the subroutine to determine which of the following occurred:

- Normal end of case
- Some type of error
- End of file reached on the input device

* GAIL1 was originally developed by R. B. Gladson of The Aerospace Corporation for the CDC 6000 computer series. It has been modified for IBM 360 and 370 computer series.

A. 1. 2 Method

All data fields are converted according to FORTRAN I/O format specifications. Real variables are converted by the F specification, whether or not the exponent (E or D) is included with the variable. Integers are converted by the I format, and alphanumeric data by the A format. This allows for alternate methods of entering real variables and integers from the FORTRAN standards. This variety of methods (Sec. A. 1. 3. 7) enables the user to enter numbers in a manner more reasonable and mathematical than did previous input routines.

A. 1. 3 Usage

A. 1. 3. 1 Data Card Format

The data card format consists of three fields, each containing three subfields; a conversion code; a location; and a value (as in the following example):

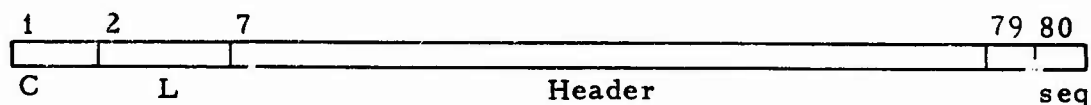
1	2	7	27	28	33	53	54	59	79	80
C ₁	L ₁	V ₁	C ₂	L ₂	V ₂	C ₃	L ₃	V ₃		seq

Subfield	Data Field 1	Data Field 2	Data Field 3
Conversion Code (C _i)	1	27	53
Location (L _i)	2-6	28-32	54-58
Value (V _i)	7-26	33-52	59-78

Columns 79 and 80 are not processed by the routine and can be used for card sequencing if the user desires. The conversion code (C_i) is one of the alphabetic characters (Sec. A. 1. 3. 7); it specifies the type of conversion to be used on the value field. The location subfield specifies the cell in which the converted value subfield is to be stored.

A. 1. 3. 2 Header Card Format

The header card format consists of a conversion code in Column 1, a sequence number in Columns 2 through 6, and any Hollerith information in Columns 7 through 78. Columns 79 and 80 are not used.



A. 1. 3. 3 Decimal Points

The use of a decimal point is valid in both integer and real variable entries; however, it is not mandatory to enter one. If the decimal point is missing from an entry, it is assumed to be at the right of the last digit punched in the value field; for example:

$$321. = 321 = 321E0$$

A. 1. 3. 4 Signs

If signs (+ or -) are used, they are placed in a column by themselves and immediately precede the value. Overpunches are not valid; e. g. :

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
		+7.1621

Valid

1	2	7
27	28	33
53	54	59
C	LOCATION	VALUE
		7.1621

Invalid

A. 1.3.5 Values (V_i Subfield)

It is not necessary for the entire subfield to be filled, since the first blank following the first nonblank denotes the end of the value. Superfluous low-order zeros should be omitted.

If alphanumeric information is entered, it is stored in core as it appears in the value subfield. Thus, for this type of data entry, leading blanks are retained. If they appear, the blanks themselves are also stored in core.

A. 1.3.6 Location (L_i Subfield)

The location is specified by either a variable, an array name, or the element subscripts in a single-dimension array or matrix.

A. 1.3.6.1 Variable, Array, or Matrix Name

If the location contains at least one nonnumeric character that is not a comma as the third character, it is interpreted as a variable, array, or matrix name. The contents of the value subfield are stored in the cell for the variable or in the first cell of the array or matrix. This location then becomes the origin of all numeric and matrix element locations that follow until another variable, array, or matrix name is encountered. Care must be taken to enter an array or matrix name before entering numeric or matrix element locations.

A.1.3.6.2 Single Numeric Entry

If a location contains a single numeric value, the entry is treated as a subscript. With its previously established origin, this subscript is used to compute the location in which the entry in the value subfield is stored. For instance, if the established origin is NAME and the value in the location subfield of the input is 6, the entry in the value subfield is stored in cell NAME(6). (Single numeric entries must be left-justified, and leading zeros are optional.) In the following example,

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
	NAME	3.716
	6	6.173

legitimate numeric entries would be shown as:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
	5	
	12	
	03	

and illegitimate numeric entries would be shown as:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
	1	
	30① 1	
	① 1	

- Not a valid subscript.
- Store as 30.
- Not recognized as a relative address; it is flagged as an error.

The symbol ① indicates 1 space between digits, and ② indicates n spaces.

A. 1.3.6.3 Matrix Element Entry

A matrix element is stored by specifying two separate two-digit numeric entries, separated by a comma, in the location subfield. For example:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
	03, 04	-3.17

-3.17 goes to element
(3,4) of the matrix

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
	15, 01	+7.38

+7.38 goes to element
(15,1) of the matrix

The elements are stored in the column major sort by using the formula

$$\text{ORIGIN}((j - 1)I + i)$$

where I is the total number of rows in the matrix and (i, j) is the element in question.

A. 1.3.6.4 Blank Location

If the location is left blank, the entry in the value subfield is stored in the cell immediately following the one in which the last value was stored. Thus, an entire array may be entered by using a name in the location subfield for the initial entry and leaving location subfields blank for the subsequent value subfield entries. The following is an example:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
	XYZ	4.0
		5.1
		6.2

4.0 stored in XYZ(1)
5.1 stored in XYZ(2)
6.2 stored in XYZ(3)

A.1.3.7 Conversion Code (C_i Subfield)

The entry in the conversion code subfield specifies the method of converting the data in the value subfield. Care should be taken to apply the proper code with each item of data; if the proper code is not applied, a premature termination will occur in a FORTRAN format statement. The eight conversion codes currently available are described in the following subsections.

A.1.3.7.1 Blank: Real Variable

The number in the value subfield is converted to and stored as a real variable. Entries can be made to the value subfield by any of four methods: Three of them are in the normal FORTRAN E, D, and F types of real variable input formats, e. g.:

1 27 53	2 28 54	7 33 59	
C	LOCATION	VALUE	
		3.615	= 3.615
		.3615E01	= 3.615
		3615E-03	= 3.615
		3615D-03	= 3.615
		.3615D01	= 3.615

The fourth method allows for the input of real variables in scientific nomenclature ($a \times 10^b$). The number is written in the value subfield and is followed by an X, then by a 10, and then by the power of ten to which the number is to be scaled (a sign must precede the exponent). Some examples follow:

- $14200 = 1.4200 \times 10^4$ is input as

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
		1.4200X10+4

or, in the normal mode, as

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
		14200

or as

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
		1.4200E4

- $.00762 = .762 \times 10^{-2}$ is input as

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
		.762X10-2

A. 1.3.7.2 I: Integer

The number in the value subfield is converted to a fixed-point integer. A decimal point is allowable; if it is used, only the integer portion is converted. Before the value is converted by the FORTRAN I format, the decimal point and any digit(s) to the right are stripped off; e. g.:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
I		71.35

is stored as 71.

A. 1.3.7.3 D: Short Header (20 Characters)

The contents of the value subfield are interpreted as 20 alphanumeric characters. They are stored in two consecutive cells in ascending order, beginning at the location specified by the location subfield. The characters are stored in the same relative positions as in the value subfield; thus, leading, trailing, and embedded blanks are legitimate. For example:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
D		ABC①DEF②GHIJ④234

is stored in two consecutive words, with ABC①DEF②G in the first word, and HIJ④234 in the second.

A. 1.3.7.4 H: Long Header (72 Characters)

A card with an H in Column 1 is considered a long header card. If the location subfield is blank, the card is ignored (treated as a comments card). If the location subfield contains a left-justified integer 1, Columns 7 through 78 of the card are stored directly in seven consecutive words in ascending core storage.

The H conversion code is the only one for which a numeric location subfield is mandatory. If the location subfield is not blank or the integer 1, the header is not stored, an error comment is printed, and the error termination procedure is invoked.

A.1.3.7.5 L: Sparse Matrix Input Definition

This input specifies only that matrix elements may be following, either on the same and/or on subsequent cards. It does not store any items of data; it only warns the subroutine that matrix elements might be stored and indicates where. The location subfield must contain the name of the matrix in which the items are to be located in core.

The value subfield must contain two-digit integers separated by a comma. The entries are the size of the matrix [I_{\max} and J_{\max}], and the comma must be the third character of the subfield. If it is not, an error comment is printed, and an error flag set.

The I_{\max} and J_{\max} values are retained to compute the successive subscripted locations of the matrix elements until they are redefined. Blank location subfields may follow this definition if successive elements of the matrix are to be loaded. It must be remembered that the matrix is stored in column major. For example:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
L	GØØD	03, 07

indicates that a 3×7 matrix GØØD is being defined and that following data values are to be stored in GØØD until another symbolic location name is encountered. Storage is to be made according to $GØØD((j - 1)I + i)$.

A.1.3.7.6 M: Full Matrix Input Definition

The use of this conversion code is identical to that of L, except that the entire matrix is preset to zero before any of the elements are loaded.

For example:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
M	GØØD	03,07

presets the 3×7 matrix GØØD to zero; it is prepared to store the matrix elements following it until another symbolic location name is encountered.

A.1.3.7.7 B: Octal

The value subfield is converted as a logical word. It is not necessary to include leading zeros, but the first octal digit must always occupy the left-most position in the subfield. If fewer than 20 digits are input, the value will be right-justified in the memory location. For example:

1 27 53	2 28 54	7 33 59
C	LOCATION	VALUE
B		123

is stored as 000000000000000000123₈ in core.

A.1.3.7.8 E: End of Case

This defines the end of case, when control is returned to the object program from which it was called. The rest of the subfield and the remaining fields on the card are ignored.

A. 2 ERROR COMMENTS

The input errors that the subroutine can recognize are listed in Table A-1. In each case, an appropriate error comment is printed, the remaining cards in the data set are scanned until an E conversion code is found, and the run is terminated. The errors are not listed in any specific order.

Table A-1. Errors Recognizable by Input Subroutine

Error Message	Type of Input Error
HEADER CARD NO. EXCEEDS MAXIMUM NO. ALLOWABLE.	If the location subfield is not blank or the integer 1, the card is not stored; it is printed as shown, and the error termination procedure takes over.
← Card Image (80 Characters) →	
ERROR ATTEMPTING TO COMPUTE NEXT STORAGE LOCATION FROM BLANK LOCATION FIELD. BASIC SYMBOLIC ORIGIN HAS NOT BEEN SET.	The first value input had a blank location subfield, and no symbolic origin had been established.
← Field in Error →	
ERROR ATTEMPTING TO COMPUTE NEXT STORAGE LOCATION FOR A MATRIX ELEMENT. BASIC SYMBOLIC ORIGIN HAS NOT BEEN SET.	A matrix element is to be stored, but no location definition of the matrix has been made by a previous M or L card.
← Field in Error →	
MATRIX SIZE UNDEFINED.	A matrix element is to be stored, but no size definition of the matrix has been made by a previous M or L card.
← Field in Error →	
ERROR ATTEMPTING TO COMPUTE NEXT STORAGE LOCATION FOR NUMERIC LOCATION FIELD. BASIC SYMBOLIC ORIGIN HAS NOT BEEN SET.	The first value input had a numeric location subfield. No symbolic origin had been established before this point.
← Field in Error →	
UNDEFINED SYMBOL USED IN LOCATION FIELD.	A symbol not previously defined was used in the location subfield.
← Field in Error →	
MISLING COMMA IN MATRIX DEFINITION.	During an attempt to define a matrix (M or L conversion code), the third character in the value subfield was not a comma.
← Field in Error →	
ILLEGAL CONVERSION CODE.	An undefined conversion code was entered.
← Field in Error →	
INVALID CHARACTER IN VALUE FIELD.	There is an invalid character in the value field.
← Field in Error →	

A.3 SAMPLE GAIL1 INPUT FORM

A sample GAIL1 input form is shown below.

6600 INPUT DATA

PROGRAMMER _____ KEYPUNCHER _____ VERIFIED _____ DATE _____ PAGE _____ OF _____

[illegible][illegible][illegible]

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APPENDIX B

TRACE DATA DECK STRUCTURE EXAMPLES

B.1 ORBIT DETERMINATION RUN (ITIN=2)

B.1.1 Single-Vehicle with OBSERVATION Card Input

The deck setup for an orbit determination run for one vehicle is shown in Fig. B-1. All observational measurements are input in the OBSERVATION block.

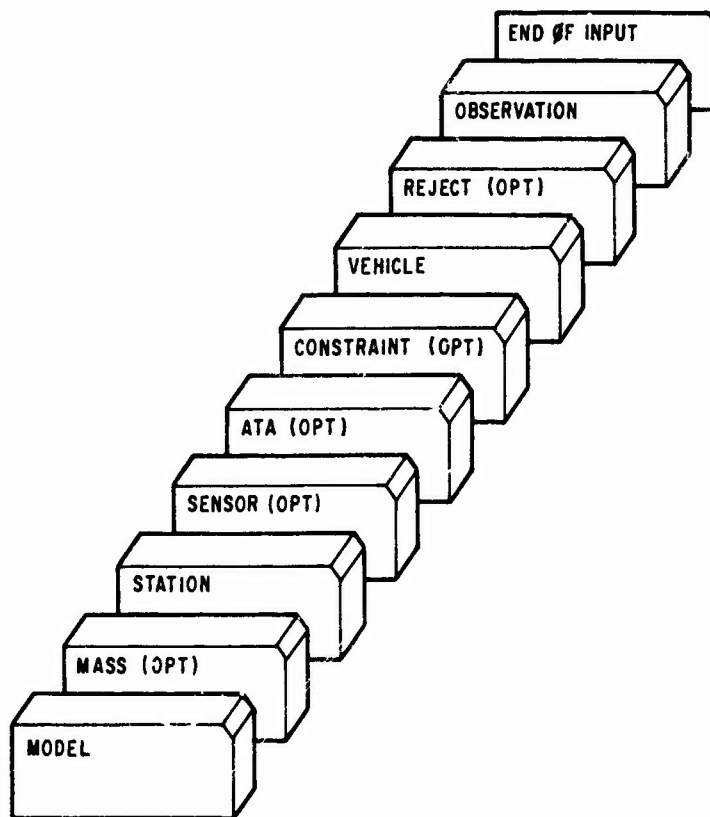


Fig. B-1. Deck Setup for a Single-Vehicle Orbit Determination Run with OBSERVATION Card Input

B.1.2 Multiple-Arc with OBSERVATION Card Input

The deck setup for an orbit determination of more than one vehicle in which measurements from the many vehicles are used (but each observation is associated with only one vehicle) is shown in Fig. B-2. In this case, only one model group (MODEL, MASS, STATION, SENSOR, ATA, and CONSTRAINT data blocks) is input; it is followed by the VEHICLE blocks for all vehicles, and then by pairs of REJECT and OBSERVATION blocks for each vehicle.

Each OBSERVATION card should have a vehicle number (Sec. 15), and VEHID and BTIME are required in each VEHICLE block. For convenience, in the VEHICLE block, the input data not overridden carries over from one vehicle to the next (characteristic of GAIL1 input).

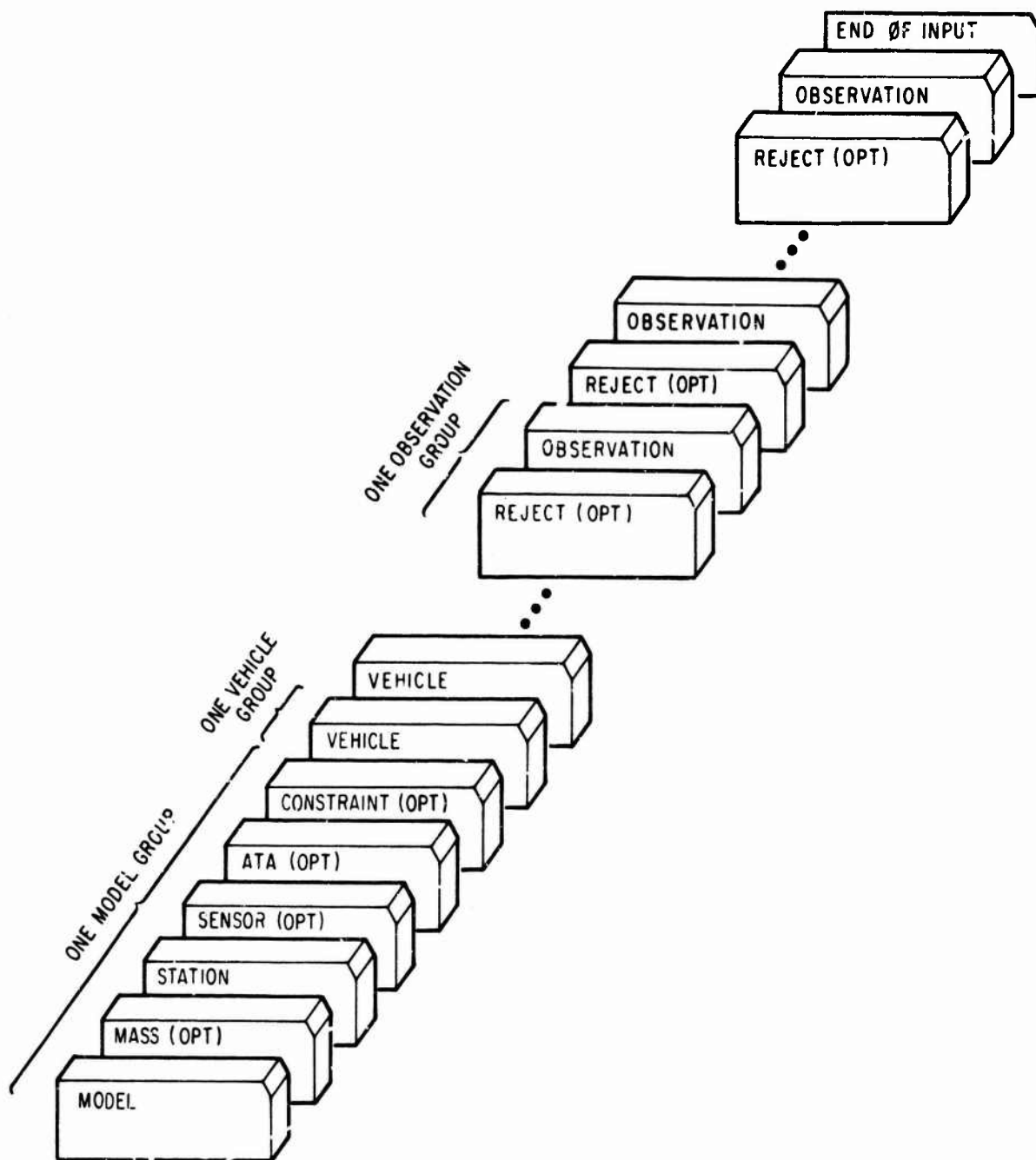


Fig. B-2. Deck Setup for a Multiple-Arc Orbit Determination Run with OBSERVATION Card Input

B.1.3 Single-Vehicle with Card Image Observation File Input

The deck setup for an orbit determination run for one vehicle, using observational measurements found on a card image observation file (TAPE4) is shown in Fig. B-3. This setup is indicated by the input item BCDIN#0 (Sec. 11.2.1) in the VEHICLE data block and the fact that the OBSERVATION card is followed by the END OF INPUT card.

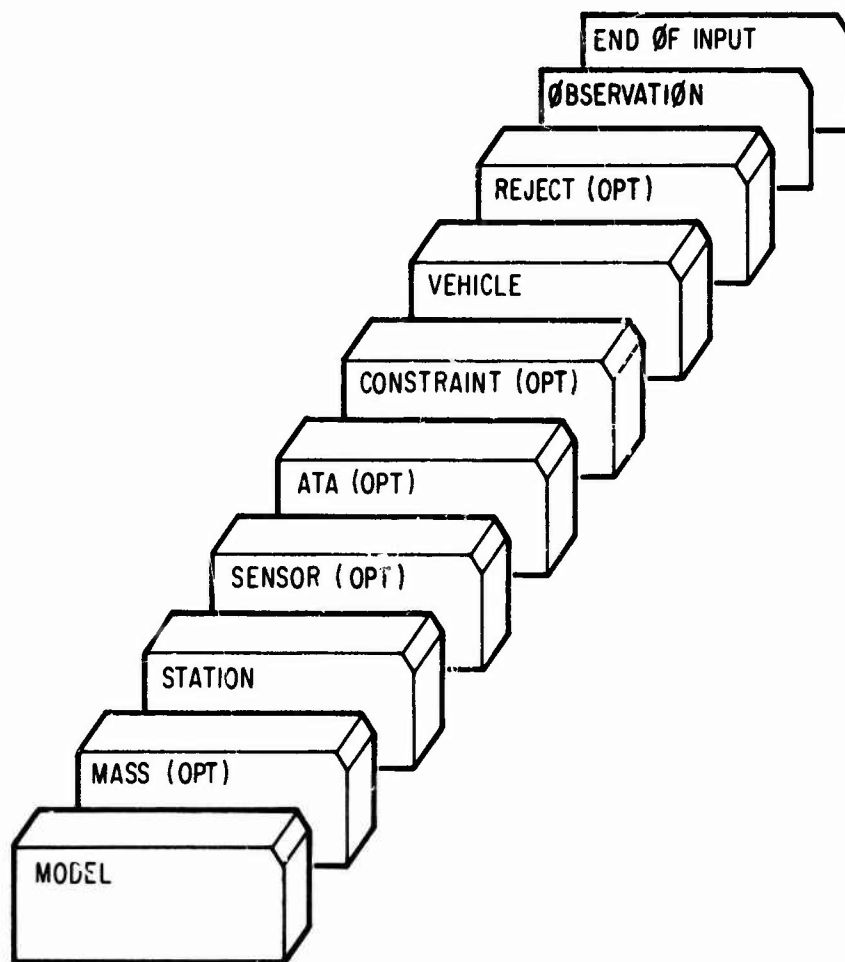


Fig. B-3. Deck Setup for a Single-Vehicle Orbit Determination Run with Card Image Observation File Input

B.1.4 Multiple-Arc with Card Image Observation File Input

In an orbit determination run with observational measurements from several vehicles (each item of data is associated with only one vehicle), the data deck requires only one set of model group data blocks (Fig. B-4). For each vehicle there must be a VEHICLE block followed by the pairs of REJECT and OBSERVATION blocks.

In the VEHICLE block, input data not overridden will carry over from one vehicle to the next. BTIME is required in each VEHICLE block to show the last integration time (more than likely, the last observation time). VEHID, which should match the vehicle number on the observation card images for that vehicle, is also required.

For this case, observations are input by the card image observation file (TAPE4). This is indicated by BCDIN \neq 0 (Sec. 11.2.1) and by a single OBSERVATION card for each vehicle.

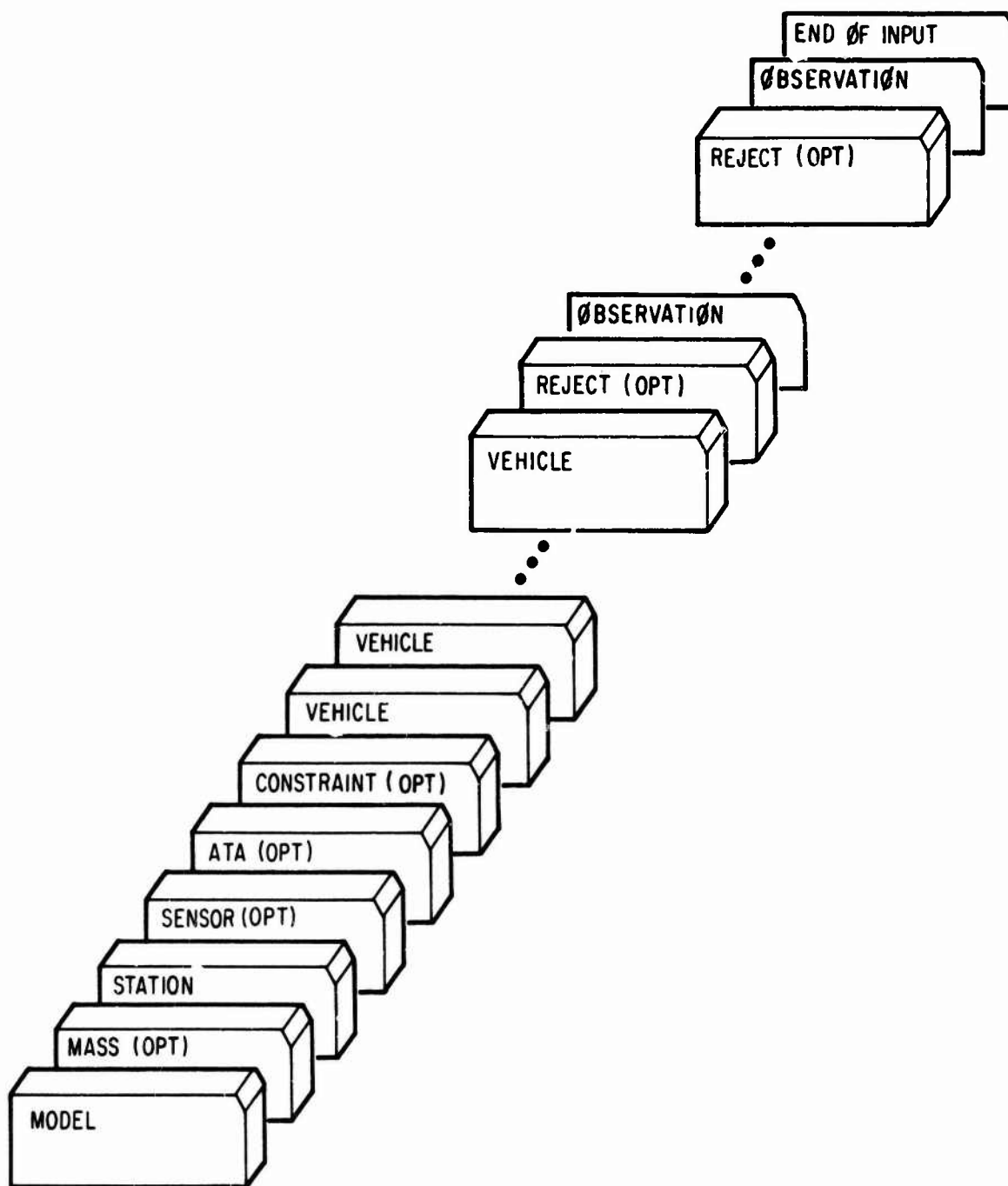


Fig. B-4. Deck Setup for a Multiple-Arc Orbit Determination Run with Card Image Observation File Input

B.1.5 Single-Vehicle Differential Correction with Binary
Observation File Input

Orbit determination for one vehicle with an input binary observation file (TAPE3) requires one model group of input data blocks and the VEHICLE block only from the vehicle group (Fig. B-5). The input item BTIME (Sec. 11.2.1) in the VEHICLE block contains the last observation time (or a later time) on the file. This time is considered in determining the final integration time. Note that no REJECT or OBSERVATION data blocks are allowed when a binary observation file is used.

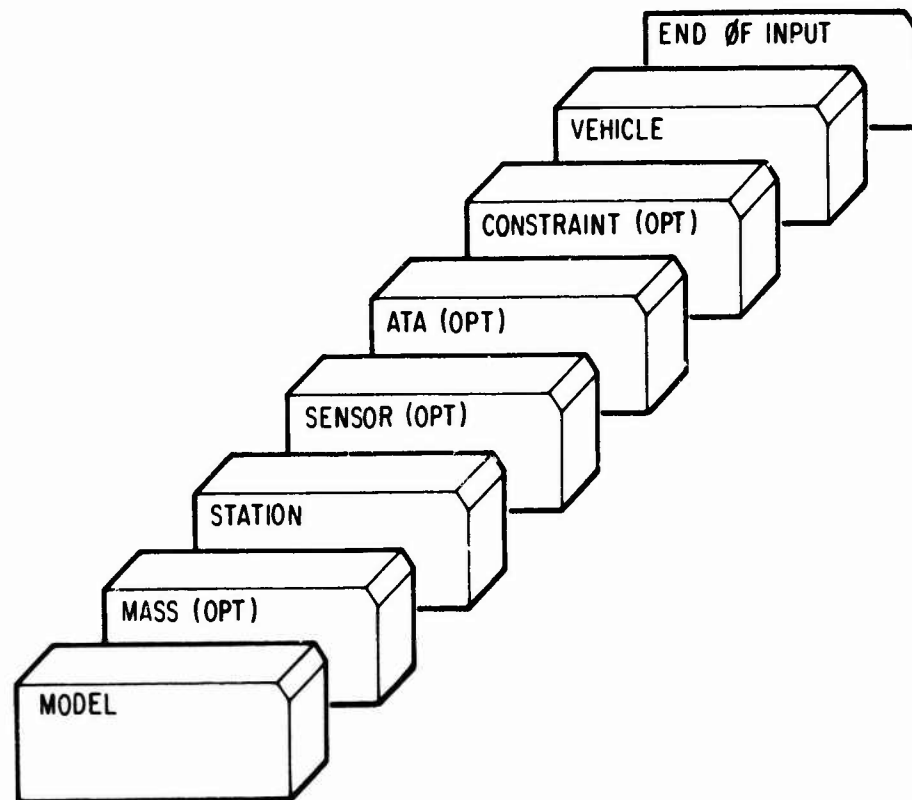


Fig. B-5. Deck Setup for a Single-Vehicle Differential Correction Run with Binary Observation File Input

B.1.6 Multiple-Arc with Binary Observation File Input

The deck setup for a multiple-arc orbit determination run with binary file observation input is shown in Fig. B-6. Observational measurements from many vehicles are used, but each item of data is associated with only one vehicle. One model group is input, and one VEHICLE block per vehicle is input. Each VEHICLE block contains the input item BTIME (Sec. 11.2.1), which indicates the last observation time (or a later time) on the binary observation file (TAPE3) for this vehicle. These times are considered in determining the final integration time for each vehicle.

Since all vehicles are assumed to be independent, a complete set of appropriate VEHICLE data should be provided for each. Input data not overridden is carried from one vehicle to the next. Again, note that no REJECT or OBSERVATION data blocks are allowed when a binary observation file is used.

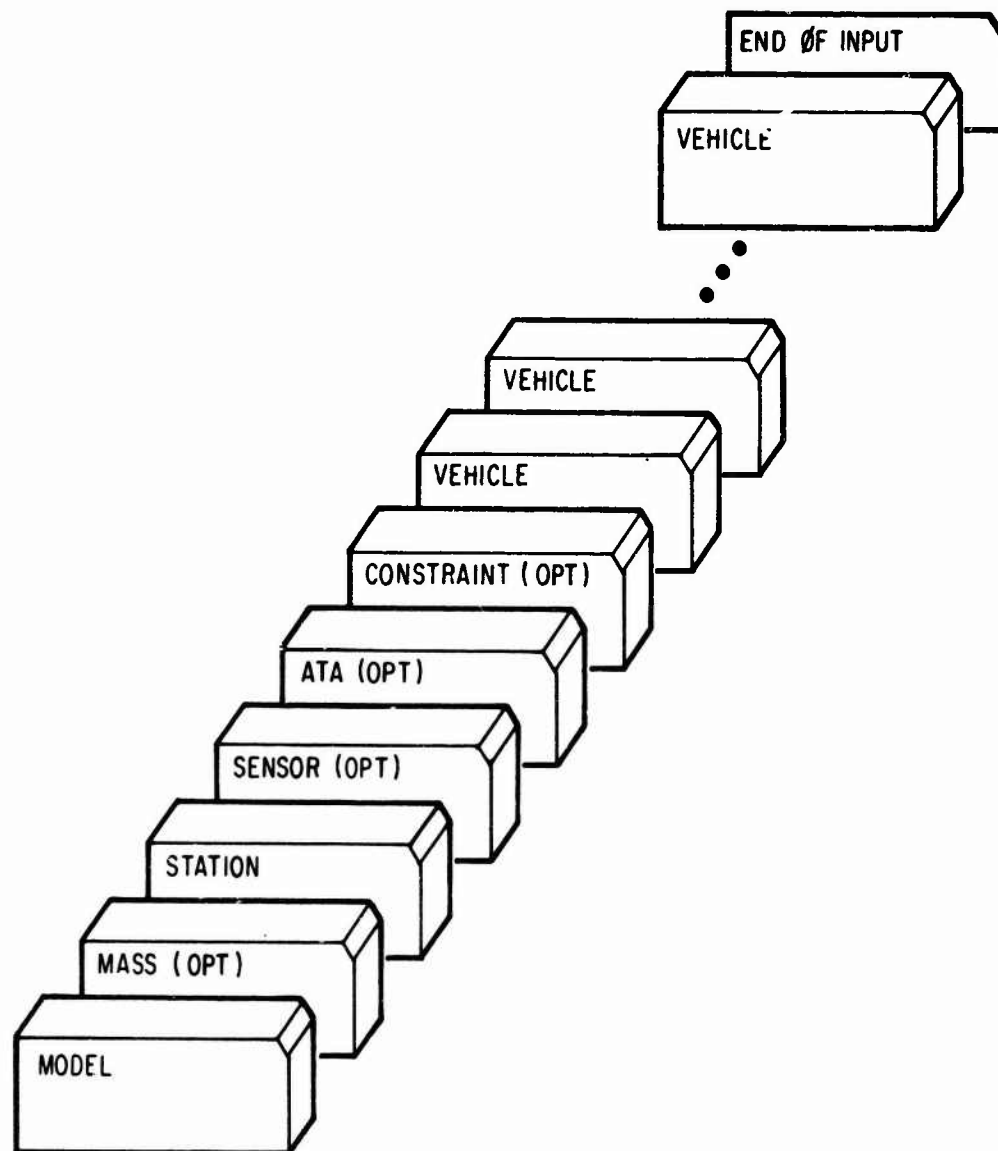


Fig. B-6. Deck Setup for a Multiple-Arc Orbit Determination Run with Binary Observation File Input

B.2 EPHEMERIS GENERATION RUN (ITIN=3)

B.2.1 Single-Vehicle

The deck setup for a single-vehicle ephemeris generation run (Fig. B-7) consists of the following: the MODEL and the (optional) MASS data blocks from the model group and the VEHICLE block. The VEHICLE block must contain the input item PTIM (Sec. 11.3.1.1), which indicates the print times and the final integration time.

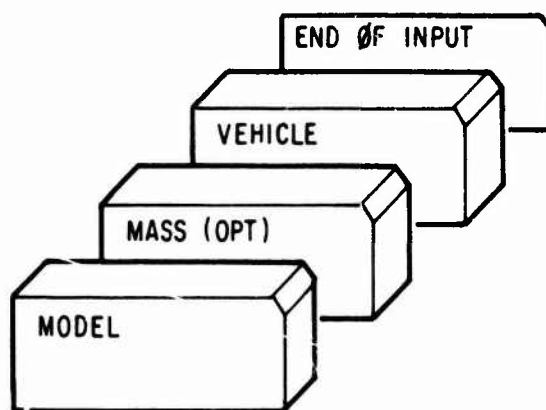


Fig. B-7. Deck Setup for a Single-Vehicle Ephemeris Generation Run

B.2.2 Multiple-Arc

The deck setup for an ephemeris generation run with several vehicles (Fig. B-8) consists of one set of MODEL and the (optional) MASS data blocks and one block of VEHICLE data per vehicle. The input item PTIM (Sec. 11.3.1.1) is specified in each VEHICLE block to indicate the print times and the final integration time for each vehicle. In the VEHICLE block, input data not overridden is carried over from one vehicle to the next.

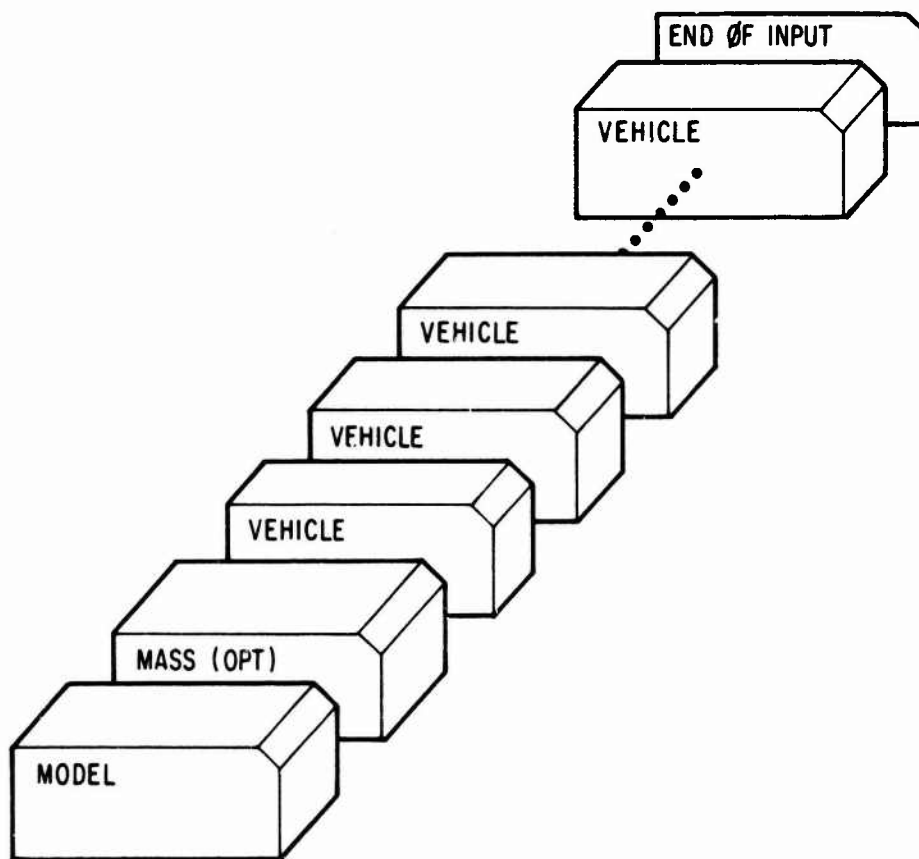


Fig. B-8. Deck Setup for a Multiple-Arc Ephemeris Generation Run

B.3 MEASUREMENT DATA GENERATION RUN (ITIN=4)

B.3.1 Single-Vehicle

The deck setup for a single-vehicle measurement data generation run (ITIN=4) requires one set each of the model and vehicle groups of input data blocks, including MODEL, STATION, VEHICLE, DATA GENERATION, and the optional MASS and SENSOR blocks (Fig. B-9).

The DATA GENERATION input block includes both DATA GENERATION I and II cards (Sec. 12) unless the VEHICLE block contains the input item JRIST=1 (Sec. 11.4.1). In this case, the DATA GENERATION II cards are omitted.

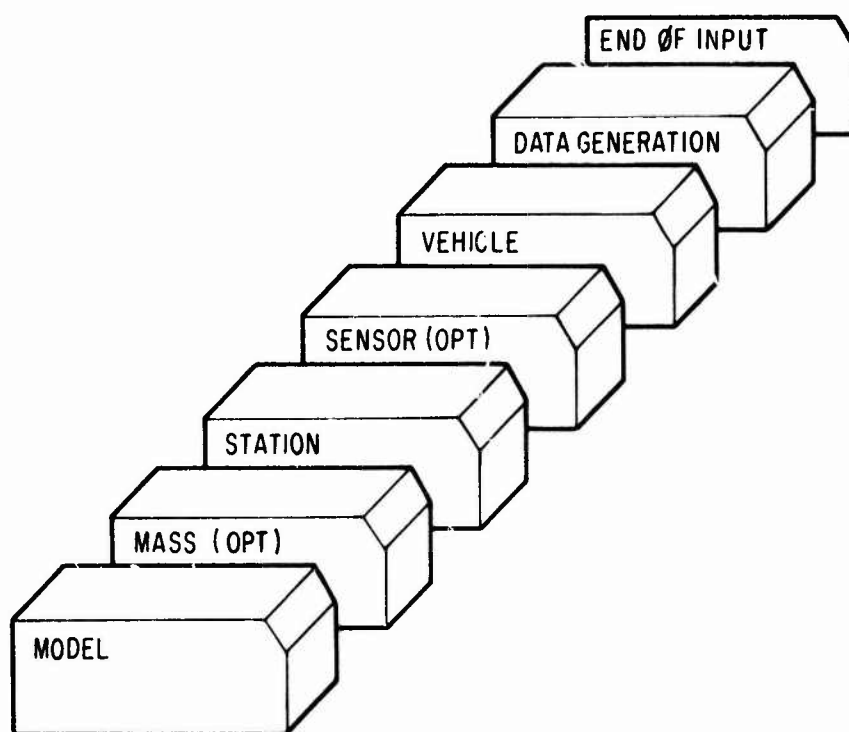


Fig. B-9. Deck Setup for a Single-Vehicle Data Generation Run

B.3.2 Multiple-Arc

The multiple-arc data generation deck (Fig. B-10) contains one set of model group data blocks and one set per vehicle of the vehicle group data blocks (VEHICLE and DATA GENERATION cards). If the VEHICLE block contains the input item JRIST=1 (Sec. 11.4.1), the DATA GENERATION II cards are omitted from the DATA GENERATION data block (Sec. 12).

Note that all vehicles are assumed to be independent; therefore, a complete set of VEHICLE and DATA GENERATION blocks should be provided for each vehicle. For convenience, in the VEHICLE block, input data not overridden is carried over from one vehicle to the next.

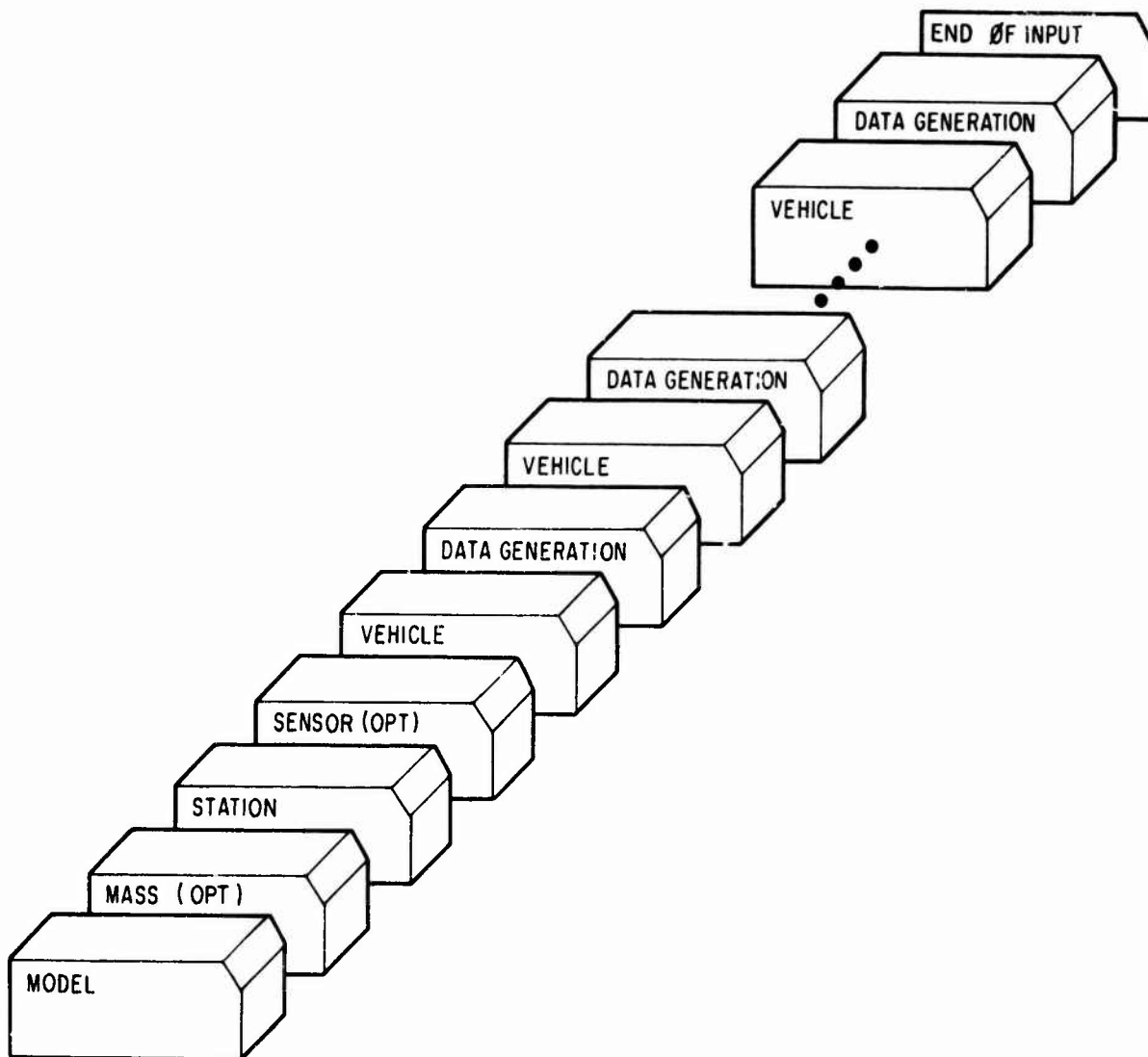


Fig. B-10. Deck Setup for a Multiple-Arc Data Generation Run

B.4 COVARIANCE ANALYSIS RUN (ITIN=5)

Deck setups for single-vehicle covariance analysis runs always contain the same basic model groups of input data blocks (MODEL, MASS, STATION, SENSOR, ATA, and COVQ), whereas the vehicle data blocks (VEHICLE and DATA GENERATION) and observation data blocks (REJECT and OBSERVATION) are variable. Various deck setups for covariance runs are shown in Figs. B-11 through B-15.

Input/output options are specified in the MODEL data block by input items $\emptyset PB\emptyset X$ and $PRC\emptyset V$ (Sec. 2.5.1). The model P/Q parameter specifications are found in the input items $\emptyset P RAM$, $MP RAM$, and $GP RAM$ (Sec. 2.1.5).

A priori input for the normal matrix $A^T A$ or the variance-covariance matrix $(A^T A)^{-1}$ is specified in the ATA data block (Sec. 6). A priori input for Q-parameters is specified via the COVQ data block (Sec. 8).

Vehicle-dependent P- and Q-parameters and the print schedule are specified by input items $VP RAM$ (Sec. 11.1.14) and $PTIM$ (Sec. 11.5.1).

Observational measurement times may be specified by:

- OBSERVATION cards
- Card image observation file (TAPE4)
- Binary observation file (TAPE3)
- DATA GENERATION data block input.

When the observational measurement times are specified by card image tape or card images, measurement times may be rejected by inputs to the REJECT data block.

In case of an update to an input $A^T A$ or $(A^T A)^{-1}$ matrix, no measurement times are required [$\emptyset PB\emptyset X(D)$ and $\emptyset PB\emptyset X(E)$, Sec. 2.5.1].

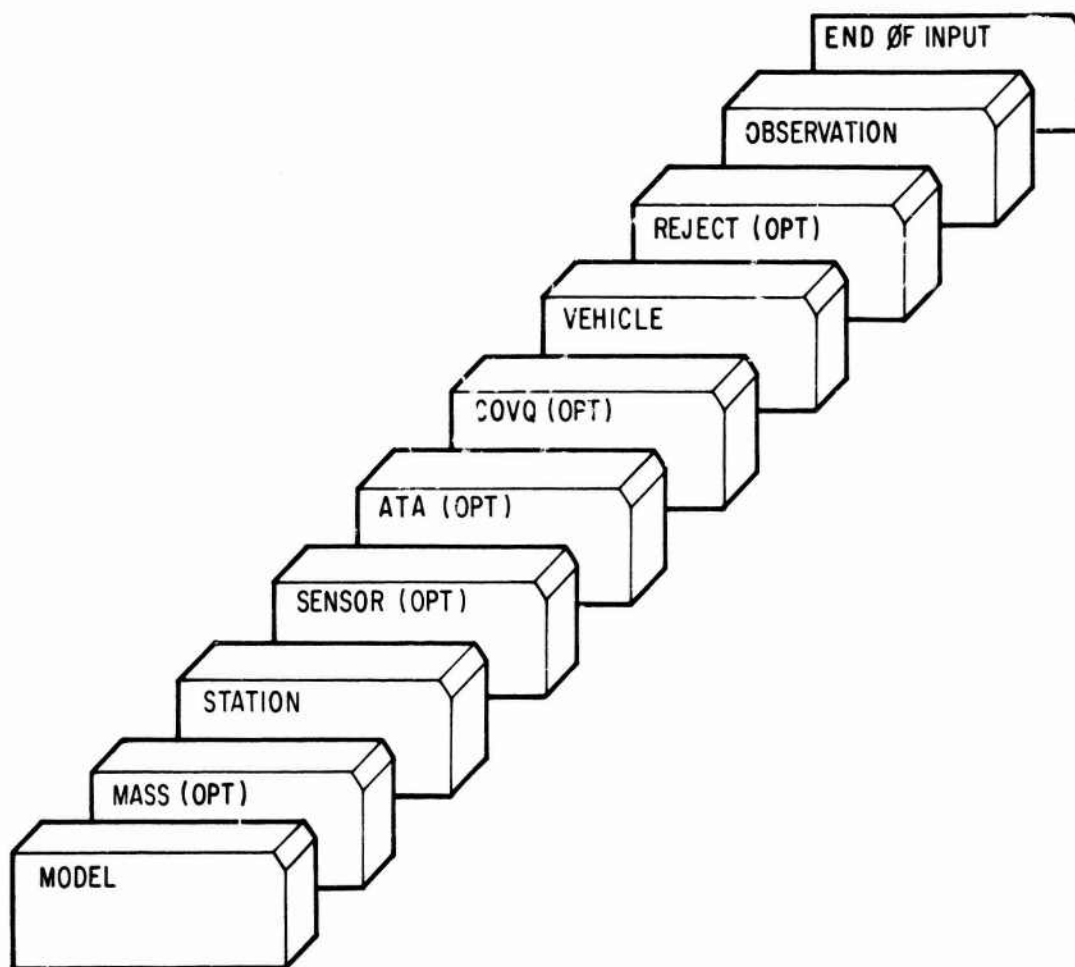


Fig. B-11. Deck Setup for a Covariance Analysis Run with OBSERVATION Card Input

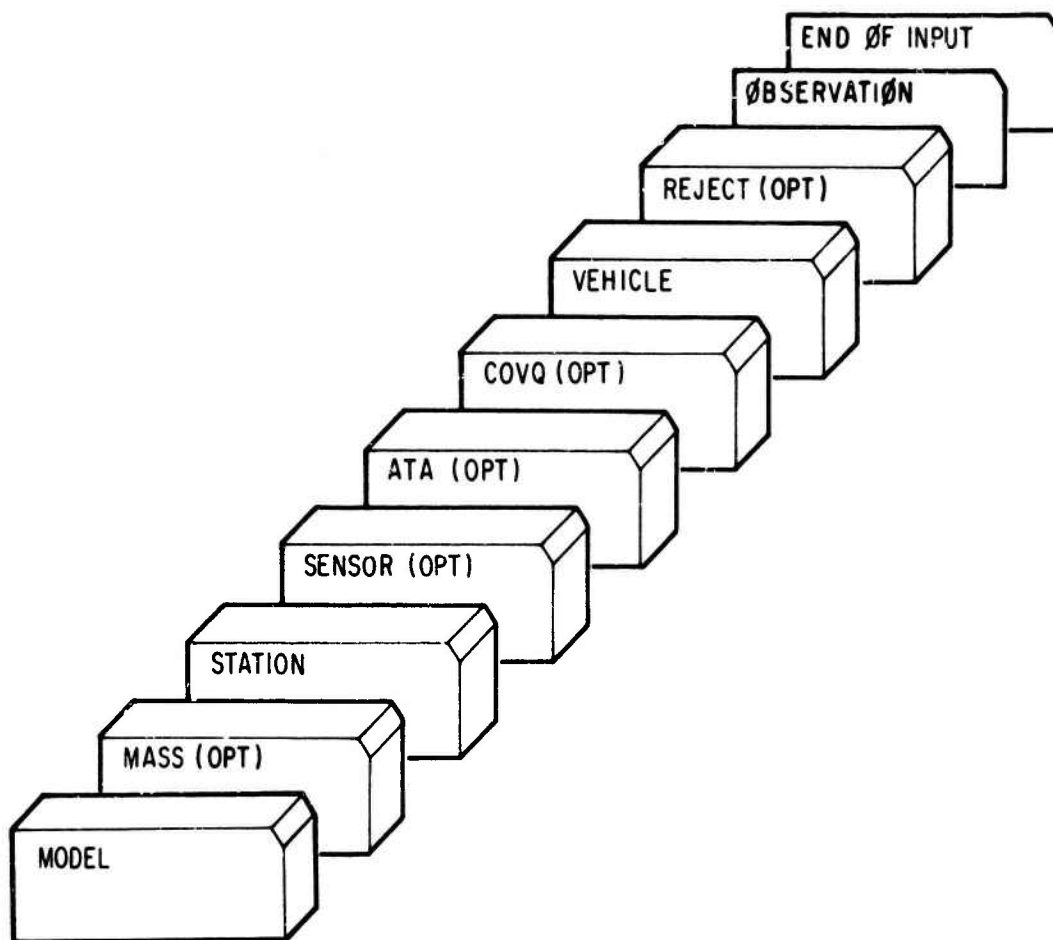


Fig. B-12. Deck Setup for a Covariance Analysis Run with Card Image Observation File Input

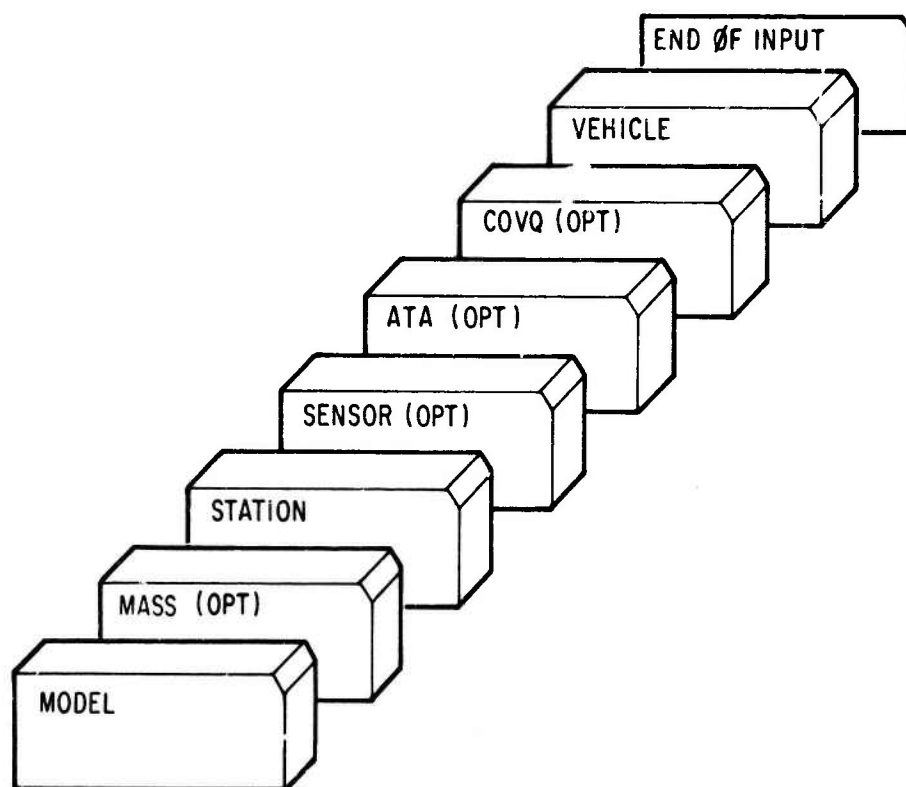


Fig. B-13. Deck Setup for a Covariance Analysis Run with Binary Observation File Input

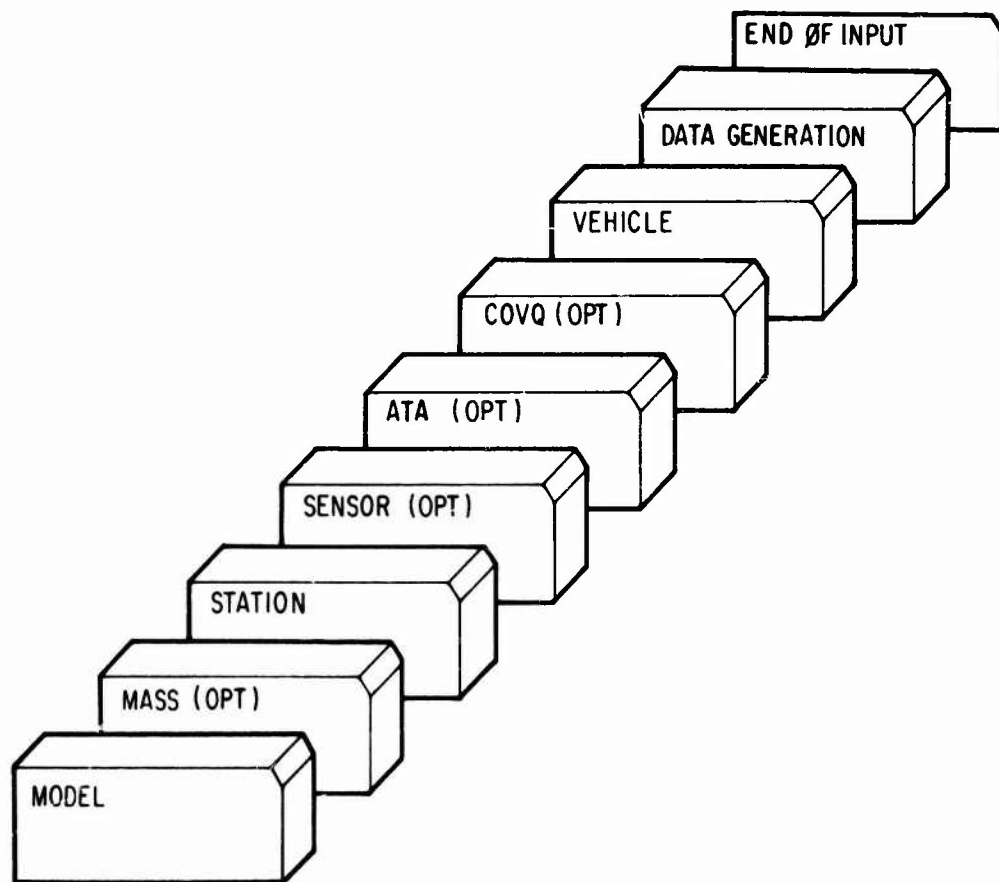


Fig. B-14. Deck Setup for a Covariance Analysis Run with Data Simulation

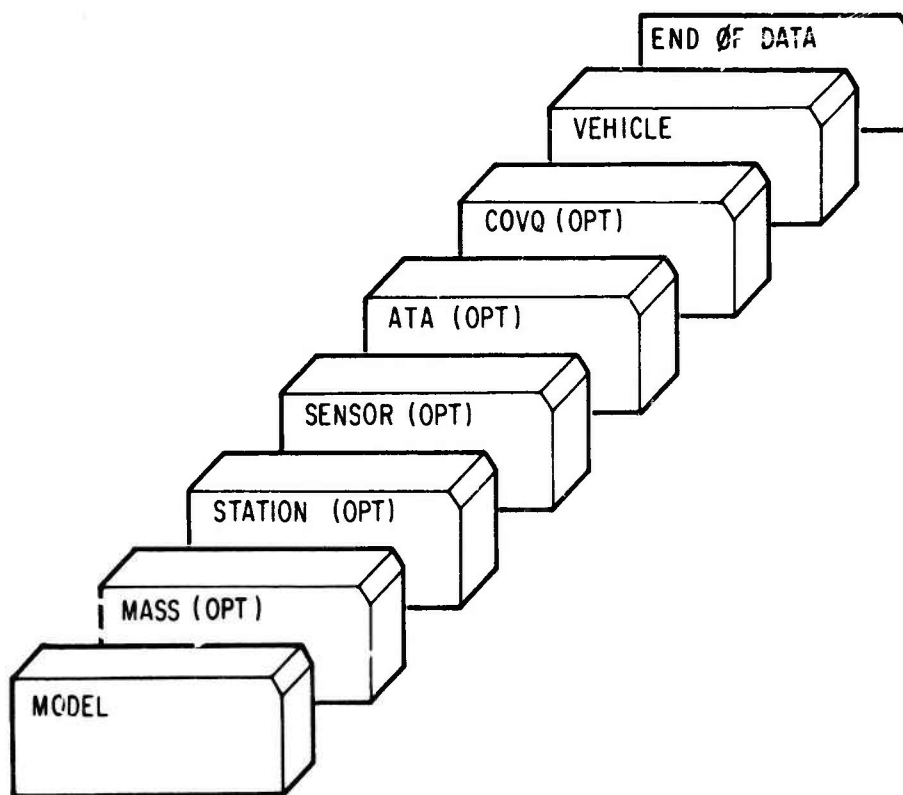


Fig. B-15. Deck Setup for a Covariance Analysis Update Only Run

B.5 MULTIPLE ITINERARY

B.5.1 Ephemeris and Data Generation (ITIN=34)

The deck setup for a case in which an ephemeris generation and a data generation are desired for the same vehicle, using the same model group blocks, is shown in Fig. B-16. Included in the MODEL and VEHICLE data blocks are all input items required for both the ephemeris generation and the data generation runs. Even though an ephemeris generation run does not require STATION, SENSOR, or DATA GENERATION input blocks, they are included in the deck setup because a data generation run does require them.

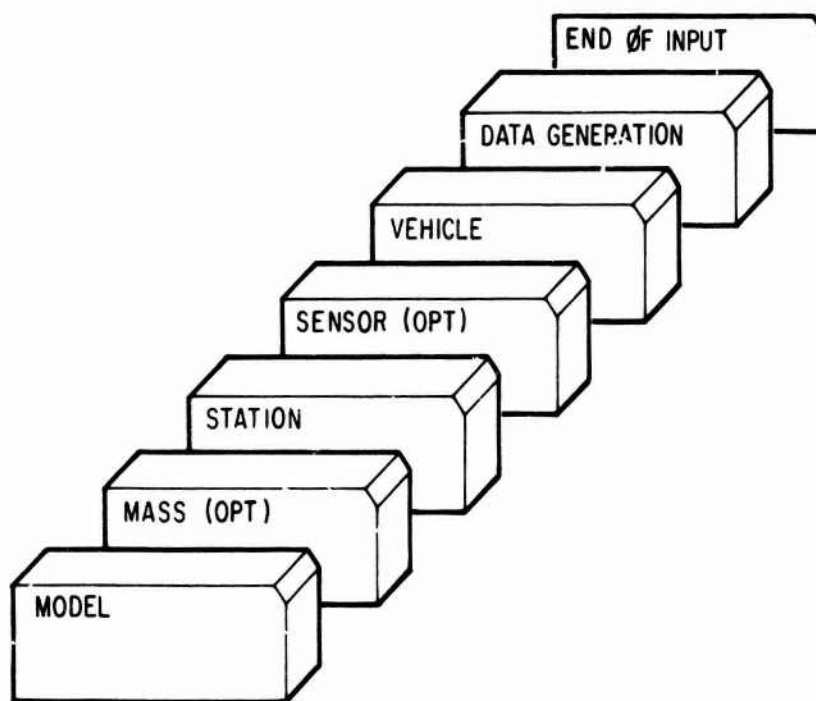


Fig. B-16. Deck Setup for a Multiple-Itinerary Run (ITIN = 34)

B.5.2 Multiple Itinerary (ITIN=3452345)

The deck setup for Example B (Sec. 1.4.1) is shown in Fig. B-17. In this case, the initial ITIN functions 3, 4, and 5 cause the generation of the nominal ephemeris, the look angles, and the covariance analysis, respectively. Reconstruction takes place starting from the nominal initial values. When the iterations terminate, the trajectory for the converged solution is used to repeat the three processing functions.

The MODEL and VEHICLE data blocks contain the necessary input items for all functions. The STATION cards are necessary for ITIN functions 2, 4, and 5. The optional ATA data block can contain $A^T A$ or $(A^T A)^{-1}$ (Sec. 6). It is used for the orbit determination and/or the covariance analysis functions. The DATA GENERATION cards are necessary to generate the look angles, and the OBSERVATION block contains the measurements used in the covariance analysis and orbit determination steps.

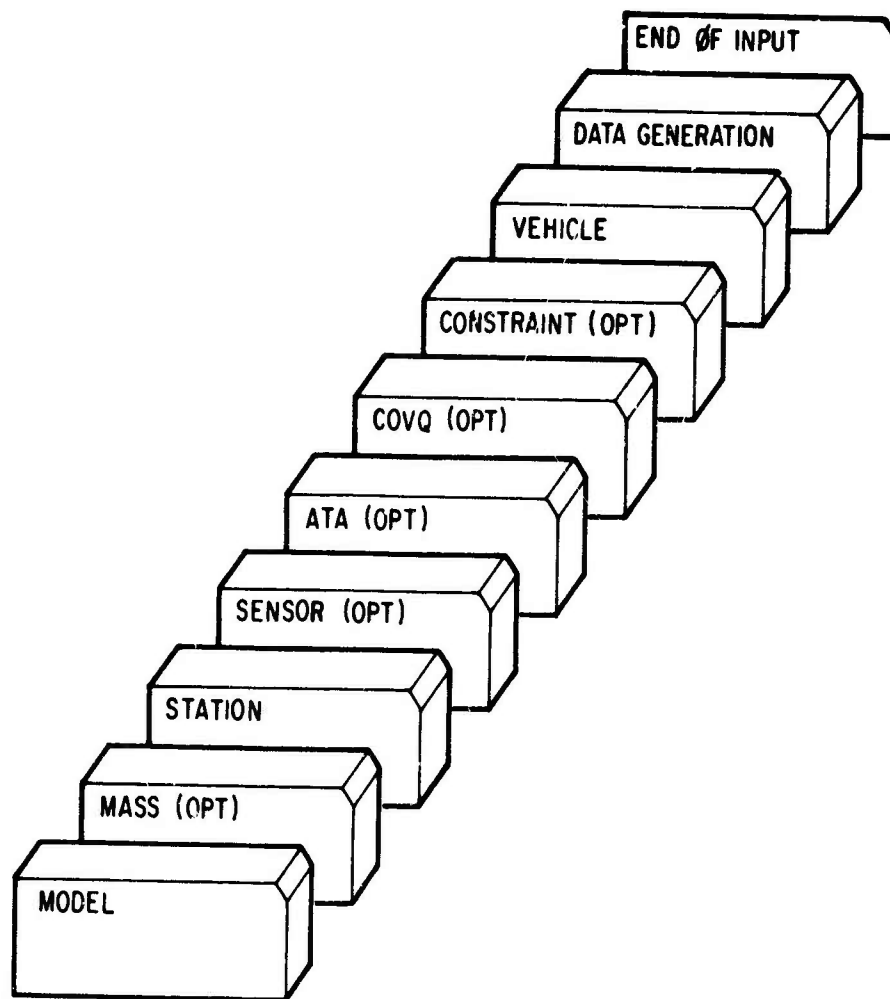


Fig. B-17. Deck Setup for a Multiple-Itinerary Run (ITIN = 3452345)

B.5.3 Multiple Itinerary (ITIN=323)

The deck setup for Example A (Sec. 1.4.1) is shown in Fig. B-18. A trajectory is generated from the input initial conditions, and an ephemeris is generated and output. Then, another trajectory is reconstructed from the observational data, and comparable ephemeris output is printed. The VEHICLE data specifies the nominal initial conditions for the trajectory, the amount of printed output, and the vehicle parameters to be differentially corrected in the reconstruction.

The observational measurements can be input by cards, card image file, or binary observation file (Sec. 11.2.1). If a card image file is used, the OBSERVATION block consists of a single card, with OBSERVATION in Columns 1 through 11. If the binary observation file is used, no REJECT or OBSERVATION data blocks are allowed.

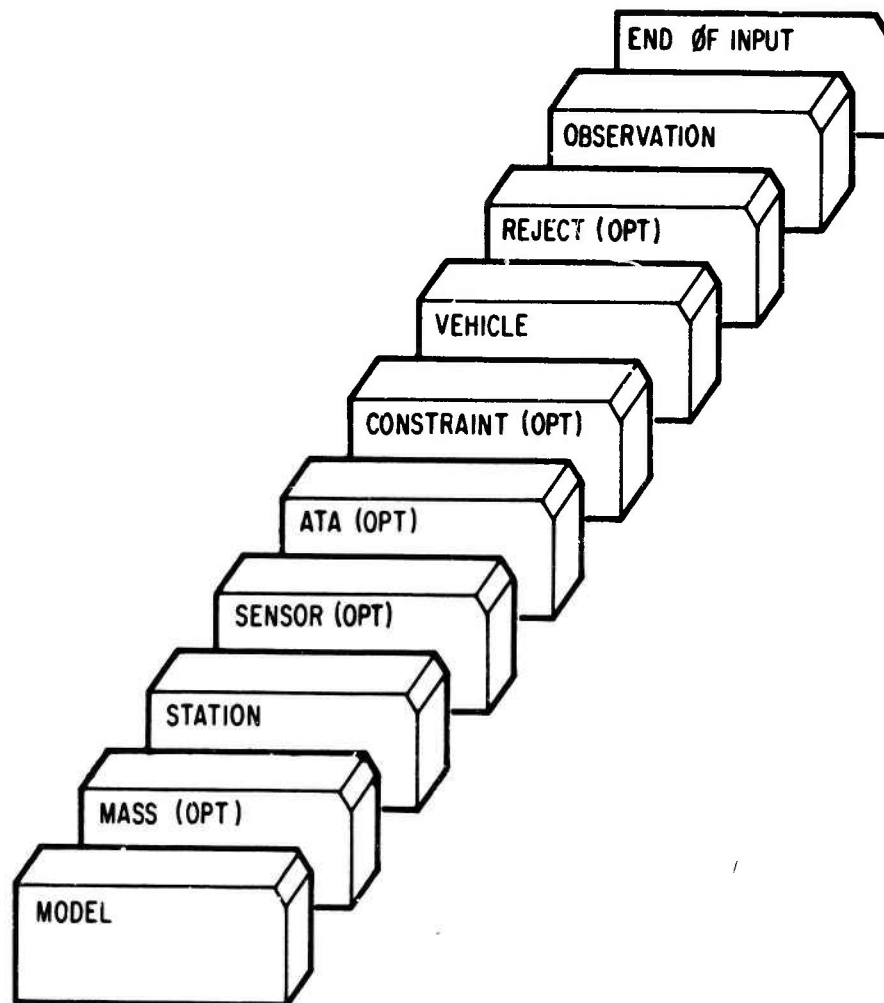


Fig. B-18. Deck Setup for a Multiple-Itinerary Run (ITIN = 323)

B.6 STACKED CASES (ITIN=34 FOLLOWED BY ITIN=2)

This data deck setup is used for Cases A and B of Appendix C (Fig. B-19). In Case A, an ephemeris is generated, and observational measurements are simulated. These measurements are written on a card image observation file (TAPE4) and are then used in the orbit determination run of Case B. Note that in the first case, from the MODEL block to the first END OF INPUT, the data block setup is as described in Secs. B.2.1 and B.3.1. The VEHICLE data also includes input item ETAPE#0 (Sec. 11.4.1), so the observations measurements are written on the card image observation file.

The ITIN=2 function is considered an entirely new case because nothing is retained from the first case; new model, vehicle, and observation group inputs are therefore included. The STATION input must be repeated, and the OBSERVATION card must be followed by the END OF INPUT card. Input item BCDIN#0 (Sec. 11.2.1), specified in the second VEHICLE block, indicates that the observations are on the card image observation file, and BTIME (Sec. 11.2.1) indicates the time of the last observation.

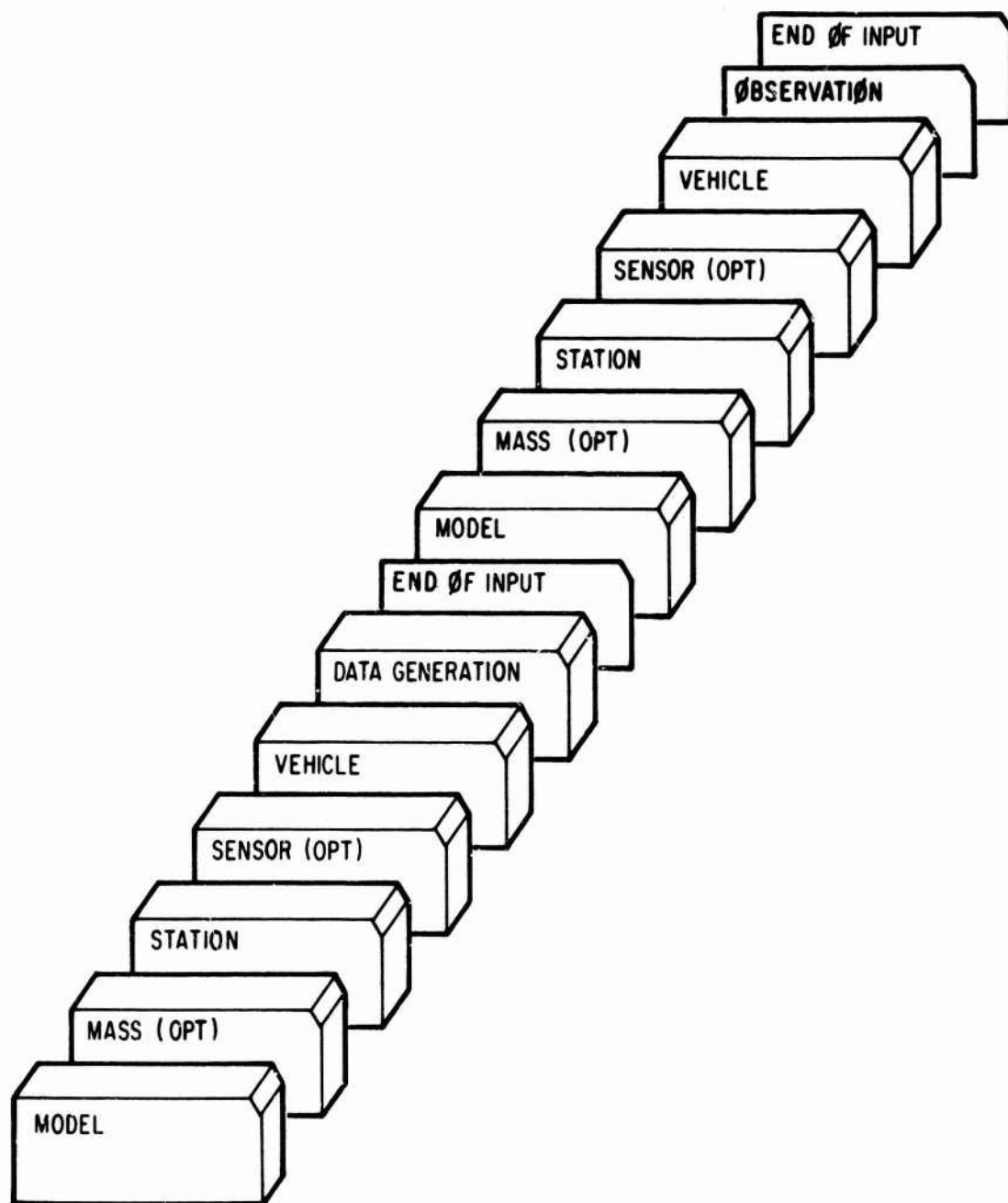


Fig. B-19. Deck Setup for Stacked Cases (ITIN = 34, ITIN = 2)

B.7 SIMULTANEOUS VEHICLES

B.7.1 Orbit Determination (ITIN=2, MULTV#0)

The deck setup is shown (Fig. B-20) for many vehicles in simultaneous orbit that have the same model. The VEHICLE data blocks are input sequentially. Each requires a VEHD (Sec. 11.1.2) and the final integration time specified by BTIME (Sec. 11.2.1), but the integration times of the first vehicle must span those of any subsequent vehicles. Since the REJECT cards are time-dependent, not vehicle-dependent, only one block is input.

Only one OBSERVATION block, containing the measurements from all vehicles, can be input. In this case, actual OBSERVATION cards are shown. If this data were input by the card image observation file (TAPE4), the block of cards would be replaced by a single OBSERVATION card. If it were input by the binary observation file (TAPE3), there would be no REJECT or OBSERVATION data blocks.

The optional ATA block may contain an $A^T A$ or $(A^T A)^{-1}$ matrix (Sec. 6). If MULTV=2 or 3, the STAGE data block (Sec. 14) is optional, and if MULTV=2, the DEWM data block (Sec. 7) is optional.

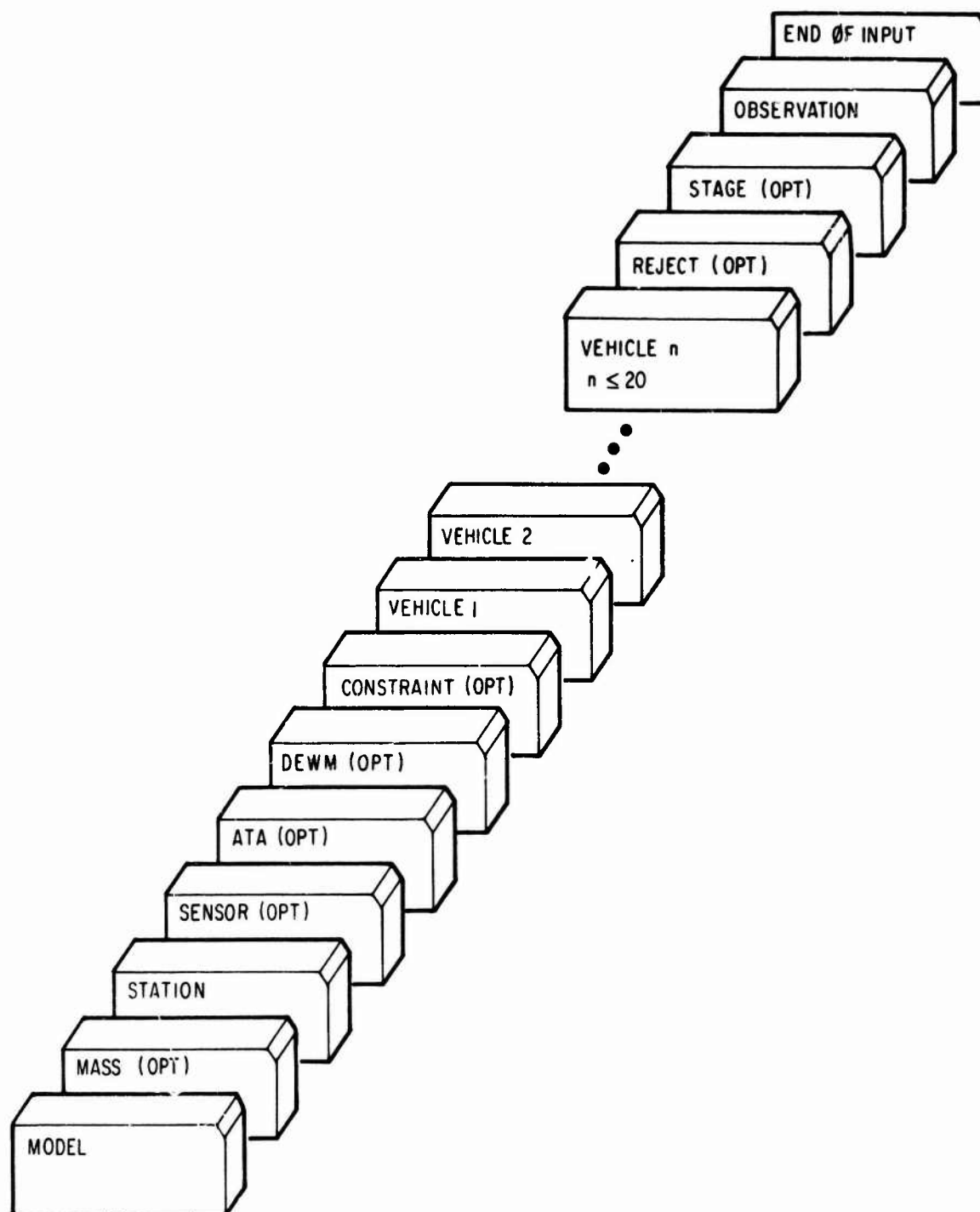


Fig. B-20. Deck Setup for a Simultaneous-Vehicle Differential Correction Run with OBSERVATION Card Input

B.7.2 Data Generation (ITIN=4, MULTV≠0)

The deck setup for generating data for vehicles simultaneously in orbit that have the same model is illustrated in Fig. B-21. Each VEHICLE data block contains a VEHIID (Sec. 11.1.2).

Only one DATA GENERATION block is input; it contains DATA GENERATION I (Sec. 12.1) and II (Sec. 12.2.2) cards.

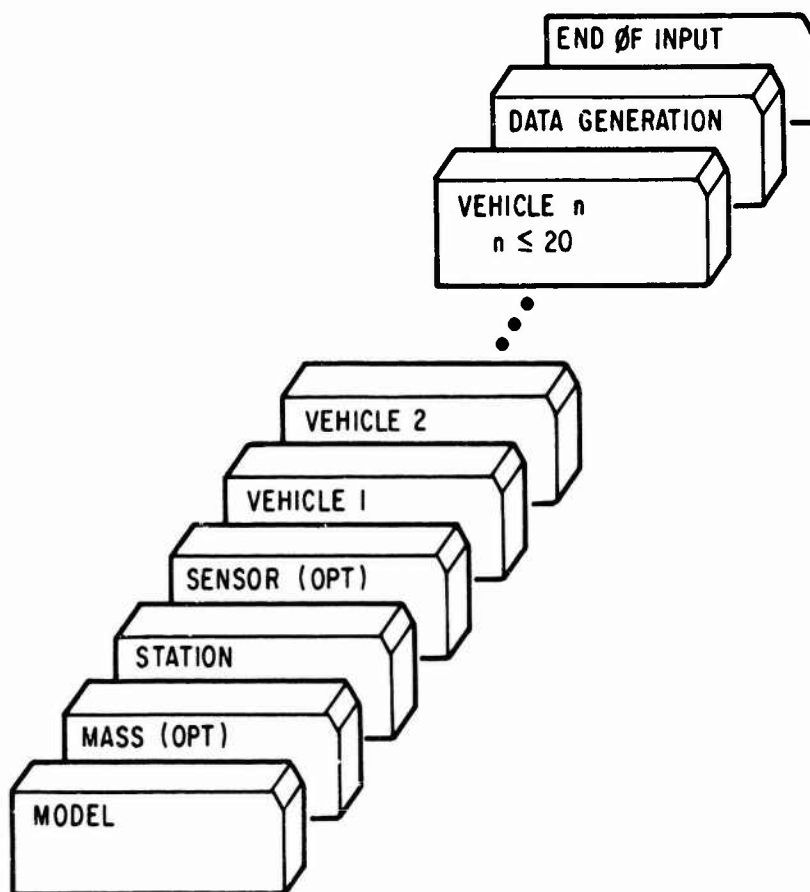


Fig. B-21. Deck Setup for a Simultaneous-Vehicle Data Generation Run

B.7.3 Covariance Analysis (ITIN=5, MULTV=1,2)

The deck setup for a simultaneous-vehicle covariance analysis run (Fig. B-22) is basically the same as that for a single vehicle (Sec. B.4). The main difference is that, since the vehicles are in simultaneous orbit, all VEHICLE data blocks are input before the DATA GENERATION, REJECT, or OBSERVATION data blocks.

Each vehicle requires a VEHD (Sec. 11.1.2), and the first requires the input of PTIM (Sec. 11.5.1). The integration times of the first vehicle must span those of any subsequent vehicles.

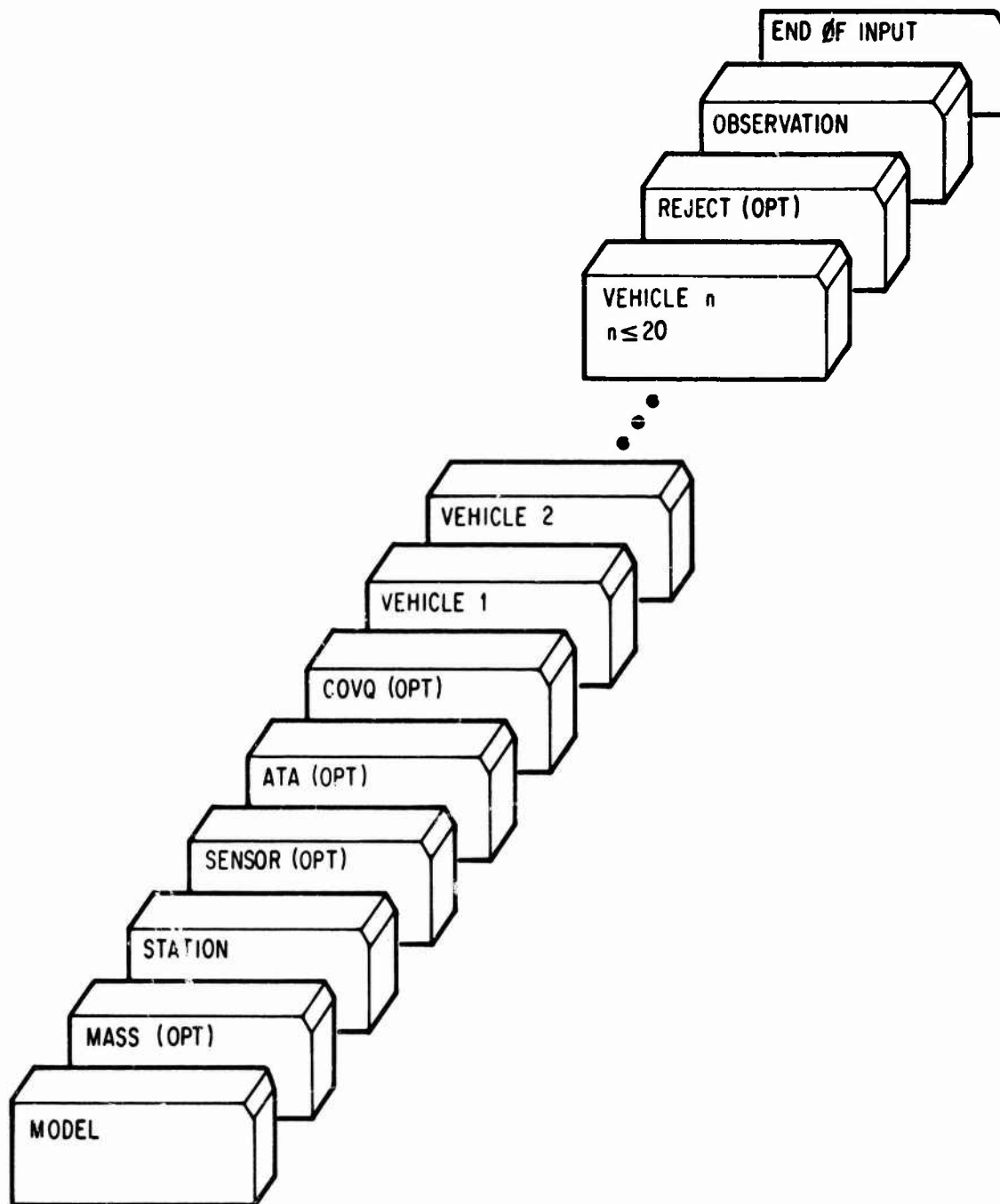


Fig. B-22. Deck Setup for a Simultaneous-Vehicle Covariance Analysis Run with OBSERVATION Card Input

C. SAMPLE OUTPUT DESCRIPTIONS

C.1	INTRODUCTION	C-1
C.2	TEST CASE A: ECI SINGLE-VEHICLE EPHEMERIS GENERATION AND SIMULATED MEASUREMENT DATA GENERATION RUN (ITIN = 34)	C-3
C.3	TEST CASE B: ECI SINGLE-VEHICLE ORBIT DETERMINATION RUN (ITIN = 2)	C-31
C.4	TEST CASE C: ECI SIMULTANEOUS-VEHICLE COVARIANCE ANALYSIS RUN (ITIN = 5)	C-63
C.5	TEST CASE D: MCI SINGLE-VEHICLE EPHEMERIS GENERATION RUN (ITIN = 3)	C-141
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TABLES

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SAMPLE OUTPUT DESCRIPTIONS

C.1 INTRODUCTION

The printed output produced by the TRACE Program is described here for typical differential correction, ephemeris generation, data generation, and covariance analysis runs. The samples that follow are of actual output listings, annotated to reference specific portions of the output data. Wherever applicable, the output items described are cross-referenced to the corresponding input definition section in this document. If an item occurs in more than one sample listing, a citation is given only for the first appearance.

The sample test cases included here are:

- Test Case A ECI single-vehicle ephemeris generation and simulated measurement data generation run (ITIN = 34)
- Test Case B ECI single-vehicle orbit determination run (ITIN = 2)
- Test Case C ECI simultaneous-vehicle covariance analysis run (ITIN = 5)
- Test Case D MCI single-vehicle ephemeris generation run (ITIN = 3)
- Test Case E ECI single-vehicle, powered flight ephemeris generation run (ITIN = 3).
- Test Case F ECI simultaneous-vehicle orbit determination run (ITIN = 2)
- Test Case G ECI simultaneous-vehicle data generation run (ITIN = 4)

The symbol , used throughout the sample output, indicates that some output has been omitted. Note that many output pages without descriptive interruption have been included only to provide continuity. Cases A through D were run on TRACE Version 6.96 and Cases E through G on Version 7.27.

TEST CASE A: ECI SINGLE-VEHICLE EPHEMERIS GENERATION AND SIMULATED MEASUREMENT DATA GENERATION RUN (ITIN = 34)

[illegible]

ITEM	DESCRIPTION	REFERENCE SECTION
1	<u>Identification number of the program version and its date</u>	
2	<u>Date on which run is made</u>	
3	<u>Program identification for accounting purposes:</u> AD104A is the Aerospace IPD (Information Processing Division) identification number	

MODEL DATA
INFORM1
N 02,00
O 03,00
O 04,00
O 02,02
NITIN 34
RSPLT5
H0 2.0
END

INTER#4
1082.76E-5
-2.693E-6
-1.56E-6
1.544E-6

MTERMS04,60

CARD 1
CARD 2
CARD 3
CARD 4
CARD 5
CARD 6
CARD 7
CARD 8
CARD 9

MMIN 2.0

MMAX 2.0

***** LUNAR GRAVITY MODEL *****
SM = 6.802326500E-05 ER**3/MIN**2 = 1.7313995407E+14 FT**3/SEC**2 = 4.902777038E+12 M**3/SEC**2
SPHERICAL MODEL

***** EART1 GRAVITY MODEL *****
SM = 5.530393500E-03 ER**3/MIN**2 = 1.4076539841E+16 FT**3/SEC**2 = 3.9860318297E+14 M**3/SEC**2
NO NORMALIZATION WITH 4 TERMS.

N	M	CNM	SNM	**	N	M	CNM	SNM
2	0	1.08276000E-03	0.	**	4	0	-1.56000000E-06	0.
3	0	-2.69300000E-06	0.	**	2	2	1.54400000E-06	-7.65000000E-07

***** PHYSICAL CONSTANTS *****
GM(EP**3/MIN**2) = 5.530393500E-03
GMKM(KM**3/MIN**2) = 0.
SGM(FD**3/MIN**2) = 6.802326500E-05
PFT(FT/EP) = 2.093573900E+07
FTKM(FT/KM) = 3.281839000E+03
SUNR0(FT/SEC**2) = 3.217400000E+01
CKFP = 1.000000000E-07
OMEGE(RAD/MIN) = 4.375269100E-03
OMEGA(RAD/MIN) = 4.375269100E-03
OMEGL(RAD/MIN) = 0.
ERKH(KM/ER) = 6.378164900E+03
FTNM(FT/NM) = 6.076115500E+03
DGREE(DEG) = 5.729577951E+01
F = 3.352329869E-03
GMLAT(DEG) = 7.830000000E+01
GMLNG(DEG) = 2.910000000E+02
AM(ER) = 2.725062770E-01
ERNH(NM/ER) = 3.443933600E+03
AE(ER) = 1.000000000E+00
SLT = 2.820176300E+03
PI = 3.141592654E+00

***** INPUT/OUTPUT CONVERSION FACTORS *****
VF(I/O-ER/MIN) = 3.48752300E+05
AF(I/O-ER/MIN**2) = 5.81270500E+03

ITEM	DESCRIPTION	REFERENCE SECTION
4	<p><u>Card images of the input MODEL data:</u></p> <p>NFØRM, NTERM, TERMS (geopotential inputs) ITIN (function indicator) RSPLT (rise/set plot indicator) HØ, HMIN, HMAX (numerical integration inputs)</p>	<p>2.1.2.2 2.1 2.4.1.1 2.1.4</p>
5	<p><u>Lunar gravity model, including the moon's gravitational constant in three unit systems.</u> In this case, the moon's gravity model is spherical</p>	<p>2.1.2 2.1.1</p>
6	<p><u>Earth's gravity model, including the earth's gravitational constant in three unit systems.</u> In this case, the gravity model is expressed by a spherical harmonic expansion with C and S coefficients, and there is no normalization</p>	<p>2.1.2 2.1.1</p>
7	<p><u>Input physical constants and OMEGL:</u></p> <p>OMEGL (lunar rotation rate)</p>	<p>2.1.1</p>
8	<p><u>Input/output conversion factors for distance, velocity, and acceleration; always using er, er/min, and er/min² internally</u></p>	<p>2.1.1</p>

***** INTERPATION INPUTS *****

IFORM = 1 ISENT = 1 NSTEP = 2
 NPCMP = 0 IR = 8 ER = 1.0000000E-10
 HMIN = 2.00000000E+00 HMAX = 2.00000000E+00 H0 = 2.00000000E+00

***** SPECIAL OPTIONS *****

TAPE2 = 0 TAPE7 = 0 TELEM = 0 PTAPE = 0 NPDOT = 0
 PRHC = 0 NONPR = 0 CLASS = 0 LEMSP = 0 PTWS = 10000

***** CRASH ALTITUDE *****

ECI CRASH ALTITUDE(FT) = 3.00000000E+05 MCI CRASH ALTITUDE(FT) = 3.00000000E+03

***** STATION LOCATIONS *****

STATION	SIG	REF	PA-REF	DATUM	TYPE	RADIUS	LATITUDE X	LONGITUDE Y	HEIGHT Z	P	Q
001	0	1	1	-0	-0	3.48000000E+01	2.39500000E+02	6.00000000E+02			
004	0	1	1	-0	-0	5.76000000E+01	2.07000000E+02	4.26000000E+02			
005	0	1	1	-0	-0	2.16000000E+01	2.01700000E+02	9.41000000E+02			
006	0	1	1	-0	-0	4.29000000E+01	2.88350000E+02	7.84000000E+02			
009	0	1	1	-0	-0	7.55000000E+01	2.91400000E+02	3.96000000E+02			

ENTER SEGMENT 01 AT 78.3 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 78.3 CP SECS., 228.4 PP SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
9	<u>Integration inputs and ICENT</u> ICENT (central force term evaluation indicator)	2.1.4
10	<u>Special options:</u> TAP2 PRH0 TAP7 N0DPR TELEM CLASS LEMSP NPDD0TEINTEG(13) (the period decay rate is printed at every integration step) PTNS=nINTEG(16) (the trajectory equations are printed every n integration steps)	2.1.4 2.1.2.4 2.1.1.3 2.1.4 2.1.4 2.2.1, 2.4.1.6, 2.5.1 2.1.4
11	<u>ECI and MCI crash altitudes at which to stop integrating</u>	2.1.4
12	<u>Printout of the station locations as input. If CLASS # 0, the actual locations are left blank</u>	4
13	<u>Program segment identification. Frequently, when different segments are entered, a remark is printed indicating the segment and its time of entry (from the beginning of the run). The amount of time taken for the segment last executed is also printed</u>	

* Information Processing Division, TRACE66 Orbit Determination Program, Vol. III: Trajectory
Generation Equations and Methods, TOR-0066(9320)-2, Vol. III, The Aerospace Corp.,
El Segundo, Calif. (25 April 1970). This report is Ref. 2 of Part A.

***** V-TITLE DATA *****

70-170
 H1
 IVEHID1
 INAY 16
 MIN 727
 IC 351.5
 4 354.475
 IIDRAG1
 IETAPF4
 DPCDEX
 PTIM 0
 4 40
 FND

IVEAR 1964
 T7NE 0
 SEC 0
 2 0
 5 21351065.
 DRAS .0116

IMNTH 8
 HR 0
 ICTYP2
 3 90
 6 25855.914

CARD 1
 CARD 2
 CARD 3
 CARD 4
 CARD 5
 CARD 6
 CARD 7
 CARD 8
 CARD 9
 CARD 10
 CARD 11
 CARD 12

DATA GENERATION I

STATION	INTERVAL (SEC.)	MIN.ELE. (DEG.)	MAX.ELE. (DEG.)	MAX.RANGE (N.MI.)	START TIME DA HR MIN	STOP TIME DA HR MIN	AZIMUTH1 (DEG.)	AZIMUTH2 (DEG.)
001	60.00	-0.00	-0.30	-0.	-0 -0 -0.0000	-0 22 -0.0000	-0.0	-0.0
004	60.00	-0.00	-0.00	-0.	-0 -0 -0.0000	-0 22 -0.0000	-0.0	-0.0
005	60.00	-0.00	-0.00	-0.	-0 -0 -0.0000	-0 22 -0.0000	-0.0	-0.0
006	60.00	-0.00	-0.00	-0.	-0 -0 -0.0000	-0 22 -0.0000	-0.0	-0.0
009	60.00	-0.00	-0.00	-0.	-0 -0 -0.0000	-0 22 -0.0000	-0.0	-0.0

DATA GENERATION II

STATION	PNG	P.D	P.D	P.D	5.D	LAT	HI-	VAR	ATT	SEO	ASN	TWO	TNT
	AZT	P.D	P.D	P.D	P.D	LN	DOP	KAP	XYZ	HRA	ADD	AXY	GCR
	ELF	0.0	0.0	0.0	0.0	SUR	LOK	ASP	TOP	J,V	EDD	LMN	SPR
001	*X X X*	*	*	*	*	*	*	*	*	*	*	*	*
004	*X X X*	*	*	*	*	*	*	*	*	*	*	*	*
005	*X X X*	*	*	*	*	*	*	*	*	*	*	*	*
006	*X X X*	*	*	*	*	*	*	*	*	*	*	*	*
009	*X X X*	*	*	*	*	*	*	*	*	*	*	*	*

70-170 (16)

EPOCH

VR/MO/DAY
 1964/ 8/16

X,Y,Z,DX,DY,DZ
 2.11221173438E+07
 -3.11902823223E+05
 0.

INITIAL CONDITIONS

A,D,B,A,R,V
 3.51600000000E+02
 0.
 9.00000000000E+01
 3.54475000000E+02
 2.13510650000E+07
 2.58559140000E+04

A,F,I,O,U,TAU
 2.16545058487E+07
 1.40128272088E-02
 9.55250000000E+01
 3.51599999932E+02
 3.61314213347E-11
 6.38058777822E+02

AF,AG,N,L,CHI,PSI
 1.38625022642E-02
 -2.04703623737E-03
 6.74602827921E-02
 3.51600000000E+02
 -1.60895386758E-01
 1.08958142631E+00

N PLANETARY PERTURBATIONS. (18)

** ATMOSPHERE MODEL ** LOOKHEAD (20)

TIME

D1 = 5.930000000E+00 D2 = -1.568000000E+01 FLUX = 0. (24)
 CDA/M 1.16000000E-02 (22) W/CDA 0.62068966E+01 (23)

ITEM	DESCRIPTION	REFERENCE SECTION
14	Card images of the input <u>VEHICLE</u> data: H1 VEHID YEAR, MNTH, DAY, TZNE, HR, MIN, SEC ICTYP, IC IDRAG DRAG ETAPE PRCDE PTIM	11.1.1.1 11.1.1.2 11.1.1.3 11.1.1.4 11.1.1.8 11.1.1.9 11.1.4.1 11.3.1.2 11.3.1.1
15	Output from the <u>DATA GENERATION I</u> and <u>II</u> cards	12
16	Printout of the <u>VEHICLE</u> input H1 header card	11.1.1
17	Epoch time	11.1.3
18	Trajectory initial conditions are printed in four coordinate frames based on BCI coordinates. The initial condition values shown are the results of transformations applied to the input values. The transformation for the input coordinate set (in this case, α , δ , β , A , r , and v) consists of the conversion from decimal to octal numbers, the conversion of units from ft, deg, and sec to er, rad, and min; and the performance of the corresponding inverse conversions for output. The three other types of element sets require coordinate system transformations, in addition to the number and unit system transformations noted above. Accuracy of the values printed is therefore subject to numerical truncation roundoff errors	11.1.4
19	Quantities in the left-hand column are position and velocity components in the basic vernal equinox coordinate system in ft and ft/sec. The second column gives the usual ADBARV spherical system coordinates (i.e., Type 2 initial conditions) in ft, ft/sec, and deg. The third column contains orbit semimajor axis, eccentricity, inclination, right ascension of ascending node, argument of perigee, and time of last perigee passage in MME. Other units are ft and deg. The right-hand column gives the vehicle coordinates in the f and g element set (valid for orbits such that $0 \leq e < 1$) (Refs. 1 and 2)	2.1.2.3
20	Names of any solar system bodies included in the computation of perturbative accelerations	11.1.8
21	Identification of the atmospheric model to be used	11.1.9
22	Time at which to initially use the C_D A/W indicated in the next column in MME	11.1.9
23	The reciprocal of the ballistic coefficient C_D A/W	11.1.9
24	Ballistic coefficient $W/C_D A$	11.1.9
24	The $D1$, $D2$, and flux expressions for the Lockheed atmospheric density model (for this case)	2.1.2.4.1

ENTER SEGMENT 10 AT 78.5 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .5 CP SECS., 3.5 PP SECS.

TRAJECTORY INTEGRATION FOR CASE 1 (25)

IVFP	0	ICENT	1	IDRAG	1	ALPHG	5.662162703E+00	COAM	1.160000000E-02
JVEP	0	JNORM	1	IR	0	ALG-DEG	3.244180258E+02	ER	1.000000000E-10
MVEP	0	MAJOR	0	ISRP	0	TJDATE	2.438623500E+06	HMIN	2.000000000E+00
KVEP	0	MASS	0	NEQS	3	TSTART	7.270000000E+02	HMAX	2.000000000E+00
LVEP	0	NT	4	RECMF	0	TSTOP	1.320000000E+03	MO	2.000000000E+00
ICENTY	1	JNORMX	0	NMASSX	0	FLIGHT	5.930000000E+02	NTX	0.
				NASA	0	SSTED	1.000000000E+02	SORD	1.500000000E+00

TIME(MME) TYPE ASSOCIATED QUANTITIES

727.0000 TZERO

1320.0000 TSTOP

*** TRAJECTORY START (26)

SEG11 ENTRY TIME IS 78.93100

T = 727.000000 Y = .250000 NSTEP = 0

2.11220178379E+07 -3.636604250258F+02 -3.049966727469E+01

-3.119028238232E+06 -2.462703577627E+03 4.503734134821E+00

0. 2.573579474117F+04 -1.368599519737E-03

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 3.093040E+01 -3.049970E+01 4.503503E+00 1.174270E-04 -3.083040E+01 1.455570E-04 2.851445E-04

ATMOSPHERIC 1.504282E-03 3.413128E-05 2.311366E-04 -1.486027E-03 1.344411E-17 -1.501618E-03 -8.948284E-05

TOTAL 3.093040E+01 -3.049967E+01 4.503734E+00 -1.368600E-03 -3.083040E+01 -1.356061E-03 1.956617E-04

(31)

REFERENCE SECTION

DESCRIPTION

ITEM

- 25 Remark indicating the relative number of the vehicle being integrated (not VEHIID)
- 26 Quantities associated with the current vehicle (Table C-1)
- 27 Event table, including times to start and stop integrating
- 28 Start of integration
- 29 Integration frame for the current vehicle (in this case, ECI)
- 30 Time T; step size H; number of integration steps from NSTEP to T; and position, velocity, and acceleration components in Columns 1, 2, and 3, respectively, for this event (epoch) print (in MME, min, ft, ft/sec, and ft/sec²)
- 31 Forces at T

Table C-1. Definitions of Initialized Integration Quantities

Symbol	Definition	Reference Section
IVEP	Number of C and S parameters (GPRAM)	2.1.5.2
JVEP	Number of other model parameters (\emptyset PRAM)	2.1.5.3
MVEP	Number of mass parameters (MPRAM)	2.1.5.1
KVEP	Number of vehicle-dependent parameters (VPRAM)	11.1.14
LVEP	Number of delayed parameters (i.e., THRUST, DRAG, etc.)	11.1.14
ICENTX	Central force flag for the moon	2.1.2.2
ICENT	Central force flag for the earth	
JNORM	Normalization for the earth gravity model	
MAJOR	Flag for the integration of the variational equations	
NMASS	Number of masses in the earth gravity model	2.1.2.2
NT	Number of terms in the earth gravity model	
JNORMX	Normalization for the lunar gravity model	11.1.8
IDRAG	Flag indicating the atmospheric model used	2.1.4
IR	Ratio of Runge-Kutta to Cowell step size (H0/IR)	
ISRP	Flag for solar radiation pressure	2.1.2.6
NEQS	Total number of equations to be integrated	2.1.4
RECMP	Flag for recomputation of perturbations	
NMASSX	Number of masses in the lunar gravity model	2.1.4
NASA	Coordinate and timekeeping transformation option flag	

Table C-1. Definitions of Initialized Integration Quantities (Continued)

Symbol	Definition	Reference Section
ALPHG	Right ascension of Greenwich (rad at midnight of epoch day)	11.1.6
ALG-DEG	Right ascension of Greenwich (deg at midnight of epoch day)	
TJDATE	Julian date of epoch day	
TSTART	Trajectory start time (MME)	
TSTOP	Trajectory stop time (MME)	
FLIGHT	Duration of flight (TSTOP - TSTART, min)	
SSTEP	Number of integration steps specified per rev when the regularized time variable is used	
CDAW	Reciprocal of the ballistic coefficient	
ER	Error control in integration ($ER = 1. \cdot S$, where S is the number of significant figures)	
HMIN	Minimum absolute step size for integration	
HMAX	Maximum absolute step size for integration	2.1.4
H0	Initial integration step size: A negative value indicates backward integration	2.1.4
NTX	Number of terms in the lunar gravity model	2.1.2.2
SORD	Power of the regularization transformation	11.1.6
CPAW	Solar radiation pressure coefficient	11.1.4
UTD	Correction that relates iteration time to ephemeris time, sec	2.1.4

* * NODF	T =	STEP	DOURLED	T =	739.250000	H =	.500000	NSSTEP =	48
NODF	T =	7.715056082307E+02	DOURLED	T =	755.250000	H =	1.000000	NSSTEP =	79
NODF	DT =	1.000000000000E+00			-2.174312233391E+07		3.220848060321E+06		9.155402131023E-02
NODF	DT =	8.160132498351E+02			3.538916113278E+02		2.392365839274E+03		-2.499914410016E+04
NODF	DT =	1.000000000000E+00			2.111878462148E+07		-3.138242581735E+06		1.057768166002E-01
NODF	DT =	9.505088844192E+02			-3.676358013866E+02		-2.462617183232E+03		2.573513801870E+04
NOCE	DT =	1.000000000000E+00			-2.173661142815E+07		3.240165570270E+06		9.162694120100E-02
NOCE	DT =	9.050141616366E+02			3.545031738123E+02		2.392907285641E+03		-2.500214730405E+04
NOCE	DT =	1.000000000000E+00			-2.111560357750E+07		-3.157478550731E+06		1.052970851538E-01
NOCE	DT =	9.495001485312E+02			-3.715253959224E+02		-2.462027934117E+03		2.573440021394E+04
NOCE	DT =	1.000000000000E+00			-2.173012707833E+07		3.259487366782E+06		9.058326290414E-02
NOCE	DT =	1.000000000000E+00			3.550446520700E+02		2.392890505067E+03		-2.500511078411E+04
NOCE	DT =	9.940033497745E+02			-2.111248671667E+07		-3.176721703786E+06		1.070233809849E-01
NOCE	DT =	1.000000000000E+00			-3.753122137674E+02		-2.460866515650E+03		2.57357343278E+04
NOCE	DT =	1.03848003411E+03			-2.172366357365E+07		3.278795075491E+06		8.716727127885E-02
NOCE	DT =	1.000000000000E+00			3.555426278197E+02		2.392411765957E+03		-2.500804218916E+04
NOCE	DT =	1.082981321138E+03			2.110940072490E+07		-3.149593565859E+06		1.048429841835E-01
NOCE	DT =	1.000000000000E+00			-3.790299919716E+02		-2.459392224658E+03		2.573269351510E+04
NOCE	DT =	1.127448861730E+03			-2.171717340806E+07		3.298071998920E+06		7.865032799414E-02
NOCE	DT =	1.000000000000E+00			3.560585150084E+02		2.391835442467E+03		-2.501098583350E+04
NOCE	DT =	1.171948128798E+03			2.110628623951E+07		-3.245162695717E+06		1.065998433399E-01
NOCE	DT =	1.000000000000E+00			-3.827440448012E+02		-2.458042725758E+03		2.573181925916E+04
NOCE	DT =	1.216406397356E+03			-2.171059451433E+07		3.317312621633E+06		6.158998121460E-02
NOCE	DT =	1.000000000000E+00			3.566534977233E+02		2.391583030237E+03		-2.501399732251E+04
NOCE	DT =	1.260903287159E+03			-2.110309216343E+07		-3.234350508507E+06		9.425052306976E-02
NOCE	DT =	1.000000000000E+00			-3.865133472910E+02		-2.457180753738E+03		2.573099833463E+04
NOCE	DT =	1.105351933197E+03			-2.170388599938E+07		3.336525691455E+06		3.443219649954E-02
NOCE	DT =	1.000000000000E+00			3.573531955035E+02		2.391889239496E+03		-2.501711161410E+04
T = 1320.250000 + = 1.000000 NSSTEP = 644									
		-1.067370314174E+07			2.175825556370E+04		1.478330439997E+01		1.478330439997E+01
		3.489513873940E+06			-2.098591769807E+03		-4.744146117512E+00		-4.744146117512E+00
		-1.859775247439E+07			-1.277447810391E+04		2.520901666549E+01		2.520901666549E+01

FORCES
GEOPOTENTIAL
ATMOSPHERIC
TOTAL

43210000 X Y 7 (EXTERNAL UNITS) RADIAL

IN-TRACK

CROSS-TRACK

2.950655E+01 1.478331E+01-4.744146E+00 2.520901E+01-2.960652E+01 3.882527E-02 7.125906E-03
5.699119E-06-4.914114E-06 2.914771E-07 2.851771E-06 6.484690E-08-5.685813E-06 1.827404E-07
2.950655E+01 1.478330E+01-4.744146E+00 2.520902E+01-2.960652E+01 3.881958E-02 7.126088E-03

REFERENCE SECTION

ITEM	DESCRIPTION
32	<u>Change in step size</u> , indicated by a remark, the time of change, the new step size, and the number of integration steps to this time
33	<u>Nodal crossing</u> showing the time (MME) and position components on the first line and the step size (min) and velocity components (ft/sec) on the second line
34	<u>Event detection print</u> (Item 30)
35	<u>Forces</u> at time T

*** TRAJECTORY TERMINATION (36)

*** THIS CASE TOOK 1.805 SECONDS TO INTEGRATE A SPAN OF 593.2500 MINUTES ***

*** FROM 727.000 TO 1320.250 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 50 AT 80.7 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 1.9 CP SECS., 9.0 PP SECS.

(37)

REFERENCE
SECTION

ITEM	DESCRIPTION
36	<u>Remark at trajectory termination</u>
37	<u>Number of seconds to integrate the time span of the current vehicle</u>

*** TRACE66 EPHEMERIS OUTPUT KEY ***

DATE,...	ME,MY,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	REMARKS
MO/DAY/YR	MIN FROM EPOCH	X (FT)	DX (FT/SEC)	LATITUDE (DEG)	ALPHA (DEG)	REV COUNT	.
HR/MIN	MIN FROM MIDNIGHT	Y (FT)	DY (FT/SEC)	LONGITUDE (DEG)	DELTA (DEG)	PERIOD	.
SEC	SEC FROM MIDNIGHT	Z (FT)	DZ (FT/SEC)	ALTITUDE (NM)	BETA (DEG)	PER-DECAY	.
	STEP SIZE (MIN)	R (FT)	V (FT/SEC)	S-VEH-LAT (DEG)	AZIMUTH (DEG)	NOD-RES	.

ECI TRAJECTORY

30

ITEM	DESCRIPTION	REFERENCE SECTION
38	<p><u>TRACE ephemeris output key.</u> Date column includes the current month, day, year, hour, minute, and second. The next column contains the times from epoch and midnight of current date and the current step size. The following columns contain the components and magnitude of the radius vector from body center to satellite (ft) and the components and magnitude of the velocity vector (ft/sec). LAT contains the latitude, longitude, altitude, and subvehicle latitude; ALPHA is self-explanatory; and REV always contains the rev count plus (at an ascending node) the period for one revolution, the period-decay rate, and the nodal regression. The remarks column is used to indicate the reason for printing (if other than the print time vector)</p>	11.3.1
39	<p><u>The integration frame for this vehicle</u></p>	11.1.6

*** CASE 140
70-170 41

*** PPOCH POINT

DATE,...	ME,MM,ST,OT	X,Y,Z,R	JK,JY,DZ,V	LAT,...	ALPHA,...	REV,...
8/16/64	0.00000	2.11220179E+07	-3.63550425E+02	0.00000000	351.59999959	.02333
12/ 7	727.00000	-3.11902824E+06	-2.46270358E+03	204.93437636	0.00000000	0.00000
0.00000	42620.00000	0.	2.57357947E+04	69.99982	90.00000000	0.00000
		2.13510650E+07	2.58559140E+04	0.00000000	354.47499959	0.00000
A =	2.16545058E+07	MEAN ANOM =	3.60000000E+02	APOGEE =	3.61381331E+03	
E =	1.40128272E-02	ECCENTRIC =	3.60000000E+02	HEIGHT =	1.69879705E+02	
I =	9.55250000E+01	TRUE ANOM =	3.60000000E+02	PERIGEE =	3.51393342E+03	
O =	3.51600000E+02	KEP PER =	8.83412222E+01	HEIGHT =	6.99998225E+01	
U =	3.61314213E-11	ANOM PER =	8.90819493E+01	O-DOT =	8.51446431E-01	
TAU =	6.38058778E+02	NOJL PER =	8.90175033E+01	U-DOT =	-4.21677378E+00	

*** REQUESTED POINTS 43

DATE,...	ME,MM,ST,OT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	ASC NODE
8/16/64	0.00000	2.11220179E+07	-3.63550425E+02	0.00000000	351.59999959	1.00000	44
12/ 7	727.00000	-3.11902824E+06	-2.46270358E+03	204.93437636	0.00000000	0.00000	
0.00000	43620.00000	0.	2.57357947E+04	69.99982	90.00000000	0.00000	
		2.13510650E+07	2.58559140E+04	0.00000000	354.47499959	0.00000	

DATE,...	ME,MM,ST,OT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...
8/16/64	73.00000	-1.54411960E+07	-1.76837291E+04	45.25874547	177.13628383	1.37406
12/40	760.00000	7.72413983E+05	4.32536701E+03	22.19807322	45.06635191	0.00000
0.00000	45600.00000	1.54363530E+07	-1.74819005E+04	164.46761	89.43019977	0.00000
	1.00000	2.18838176E+07	2.52399240E+04	45.24996466	187.82931795	0.00000

DATE,...	ME,MM,ST,OT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	DSC NODE
8/16/64	44.50561	-2.17431233E+07	3.53894348E+02	-0.0000609	171.57394639	1.50000	
12/51	771.50561	3.22084829E+06	2.39236543E+03	13.75145825	-0.0000605	0.00000	
30.33659	46290.33659	-2.32091378E+00	-2.49991441E+04	178.57223	89.99888575	0.00000	
	1.00000	2.19503029E+07	2.51158488E+04	-0.0000609	185.52555726	0.00000	

ITEM	DESCRIPTION	REFERENCE SECTION
40	<u>Number of the case on the trajectory file (TAPE2)</u>	
41	<u>Printing the input VEHICLE H1 header card</u>	11.1.1
42	<u>Epoch print (Item 38) plus three other columns. The first contains the classical elements a, e, i, Ω, ω, and τ in ft, deg, and MME. The second column contains the mean, eccentric, and true anomalies in deg and the Keplerian, anomalistic, and nodal periods in min. The last contains the radial distance and height above the oblate earth at both perigee and apogee in nmi. The nodal regression rate $\dot{\Omega}$ and the rate of advance of the line of apsides $\dot{\omega}$ are printed in deg/day</u>	11.1.4
43	<u>Output requested by PRCDE and PTIM follows</u>	11.3.1.1 11.3.1.2
44	<u>Ascending node print (Item 38)</u>	
45	<u>Print requested by PTIM (Item 38)</u>	11.3.1.1

DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	ASC MODE
8/16/64	533.90326	2.11030922E+07	-3.86509399E+02	-0.00000000	351.20640839	7.00000	
21/ 0	1260.90328	-3.23435018E+06	-2.45718136E+03	70.77953108	-0.00000902	88.95515	
54.19710	75654.19710	-3.36225350E+00	2.57309983E+04	69.73369	90.02172268	-0.01166	
	1.00000	2.13495087E+07	2.58509459E+04	-0.00000000	354.47846382	-0.05220	
DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	
8/16/64	553.00000	3.79739708E+06	-2.48359677E+04	77.70761100	325.17057615	7.21919	
21/20	1280.00000	-2.64225703E+06	3.29827419E+03	39.87645005	77.62732148	0.00000	
0.00000	76800.00000	2.10921800E+07	5.24858129E+03	120.95062	89.20585407	0.00000	
	1.00000	2.15937032E+07	2.55978010E+04	77.70489301	333.35817387	0.00000	
DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	DSC MODE
8/16/64	578.35194	-2.17038859E+07	3.57354474E+02	-0.00000287	171.26037154	7.50000	
21/45	1305.35194	3.33652580E+06	2.39188904E+03	239.61090008	-0.00000285	0.00000	
21.11633	78321.11633	-1.09188644E+00	-2.50171116E+04	170.02827	89.97667859	0.00000	
	1.00000	2.19588494E+07	2.51337365E+04	-0.00000287	189.52164962	0.00000	
DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	
8/16/64	593.00000	-1.11943977E+07	2.15332700E+04	-57.64199647	162.54791699	7.66081	
22/ 0	1320.00000	3.52054757E+06	-2.02713773E+03	227.22841232	-57.46778205	0.00000	
0.00000	79200.00000	-1.84833097E+07	-1.31305126E+04	156.73157	90.64933992	0.00000	
	1.00000	2.18234258E+07	2.53125855E+04	-57.63441492	190.29659789	8.00000	
DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	PST-EVNT
8/16/64	593.25000	-1.08737031E+07	2.17582556E+04	-58.61936726	162.20745342	7.66358	
22/ 0	1320.25000	3.48950387E+06	-2.09859177E+03	226.82327764	-58.44804353	0.00000	
15.00000	79215.00000	-1.85977524E+07	-1.27744781E+04	156.24817	90.65737993	0.00000	
	1.00000	2.18240956E+07	2.53182358E+04	-58.61193680	190.58496505	0.00000	
A =	2.16900275E+07	MEAN ANOM =	2.42343660E+02	APOGEE =	3.61624033E+03		
E =	1.30320787E-02	ECCENTRIC =	2.41586307E+02	HEIGHT =	1.72322910E+02		
I =	9.55158745E+01	TRUE ANOM =	2.41038959E+02	PERIGEE =	3.52319860E+03		
O =	3.51255664E+02	KEPL PER =	8.91301580E+01	HEIGHT =	7.928611798E+01		
U =	3.57853864E+02	ANOM PER =	8.90942174E+01	D-DOT =	8.45137210E-01		
TAU =	1.26022945E+03	NOCL PER =	8.89399172E+01	U-DOT =	-4.19310098E+00		

*** END OF TRAJECTORY *** (47)

ENTER SEGMENT 60 AT 82.0 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS 1.2 CP SECS., 5.7 PP SECS.

REFERENCE SECTION

ITEM	DESCRIPTION
46	<u>Post-event prints.</u> In this case, the event was termination. The output contains the items described in the ephemeris output key (Item 38) and the three additional columns in Item 42
47	<u>A remark indicating the end of the trajectory ephemeris</u>

◆ ◆ ◆ DATA GENERATION FOR VEHICLE

AUG. 16, 1964

0005	RISE	AT 12	4R	9	MIN	25.84	SEC	ELEVATION =	0.00	DEGREES,	AZIMUTH =	171.88	DEGREES	80
005	12	HR	9	MIN	60.00	SEC	5.5794568E+02(RN3)	1.7220949E+02(AZI)	2.7696341E+00(ELE)					81
005	12	HR	10	MIN	60.00	SEC	3.0839567E+02(RN3)	1.7349238E+02(AZI)	1.1207660E+01(ELE)					
005	12	HR	11	MIN	60.00	SEC	8.0448078E+01(RN3)	1.8787277E+02(AZI)	5.7359071E+01(ELE)					
0005	MAX EL	AT 12	4R	12	MIN	10.67	SEC	ELEVATION =	79.53	DEGREES,	AZIMUTH =	261.09	DEGREES	82
005	12	HR	12	MIN	60.00	SEC	2.2308304E+02(RN3)	3.4479546E+02(AZI)	1.8427180E+01(ELE)					
005	12	HR	13	MIN	60.00	SEC	4.6962138E+02(RN3)	3.4496770E+02(AZI)	5.8783741E+00(ELE)					
005	12	HR	14	MIN	60.00	SEC	7.2045819E+02(RN3)	3.5019130E+02(AZI)	5.8590576E-01(ELE)					
0005	SFT	AT 12	4R	15	MIN	8.65	SEC	ELEVATION =	0.00	DEGREES,	AZIMUTH =	350.26	DEGREES	83
0005	TOTAL VISIBILITY OF PASS =	5.71	MIN.	OF	STAT. =	5.71	MIN.	OF	VEH. =	5.71	MIN.	PASS =	1	84
0004	RISE	AT 12	4R	18	MIN	13.00	SEC	ELEVATION =	0.00	DEGREES,	AZIMUTH =	217.13	DEGREES	
004	12	HR	18	MIN	60.00	SEC	5.6327235E+02(RN3)	2.2792592E+02(AZI)	2.8602274E+00(ELE)					
004	12	HR	19	MIN	60.00	SEC	5.3398100E+02(RN3)	2.4905712E+02(AZI)	6.3954642E+00(ELE)					
0004	MAX EL	AT 12	4R	20	MIN	52.02	SEC	ELEVATION =	7.79	DEGREES,	AZIMUTH =	273.67	DEGREES	
004	12	HR	20	MIN	60.00	SEC	5.0416915E+02(RN3)	2.7755269E+02(AZI)	7.7513304E+00(ELE)					
004	12	HR	21	MIN	60.00	SEC	5.8891714E+02(RN3)	3.0319002E+02(AZI)	5.7174502E+00(ELE)					
004	12	HR	22	MIN	60.00	SEC	7.4975958E+02(RN3)	3.2004020E+02(AZI)	2.4155542E+00(ELE)					
0004	SFT	AT 12	4R	23	MIN	44.72	SEC	ELEVATION =	0.00	DEGREES,	AZIMUTH =	320.24	DEGREES	
0004	TOTAL VISIBILITY OF PASS =	5.53	MIN.	OF	STAT. =	5.53	MIN.	OF	VEH. =	11.24	MIN.	PASS =	1	
0009	RISE	AT 15	4R	27	MIN	48.62	SEC	ELEVATION =	0.00	DEGREES,	AZIMUTH =	25.05	DEGREES	
009	15	HR	27	MIN	60.00	SEC	3.6357395E+02(RN3)	2.2765197E+01(AZI)	3.25563539E-01(ELE)					
009	15	HR	28	MIN	60.00	SEC	3.0680157E+02(RN3)	4.2787894E+01(AZI)	1.53968014E+00(ELE)					
0009	MAX EL	AT 15	4R	29	MIN	36.13	SEC	ELEVATION =	1.75	DEGREES,	AZIMUTH =	52.44	DEGREES	
009	15	HR	29	MIN	60.00	SEC	3.1169530E+02(RN3)	5.8771469E+01(AZI)	1.6615190E+00(ELE)					
009	15	HR	30	MIN	60.00	SEC	9.7715671E+02(RN3)	7.3590588E+01(AZI)	6.8709926E-01(ELE)					
0009	SFT	AT 15	4R	31	MIN	26.30	SEC	ELEVATION =	0.00	DEGREES,	AZIMUTH =	79.35	DEGREES	

ITEM	DESCRIPTION	REFERENCE SECTION
48	Identification of the vehicle (Item 40) for which the program is <u>simulating measurements</u> (and its VEHD)	11.1.2
49	<u>Date</u> on which the data to follow applies	
50	<u>Rise message</u> . The time at which the vehicle becomes visible from a particular location is obtained by interpolation and is printed in hr, min, and sec (the elevation and local azimuth angles are printed in deg)	4 12
51	<u>Simulated data</u> showing the station; the time of day in hr, min, and sec; and the measurements generated, as indicated by the DATA GENERATION II card (Item 15). The time results from incrementing the START by Δt ; both are found on the DATA GENERATION I card	12
52	<u>Maximum elevation point</u> . The time of the maximum elevation angle is obtained by interpolation and is printed, with the corresponding elevation and azimuth angles, in deg	
53	<u>Set message</u> . When the vehicle is no longer visible from a station, the time of invisibility is obtained by interpolation and is printed, with the corresponding elevation and azimuth angles, in deg	12
54	<u>Duration message</u> . After each pass, a message is printed giving the elapsed time of visibility for the pass in min and the current totals for station and vehicle. The number of the pass for the station is also printed	

***** VISIBILITY SUMMARY *****

STA- TION	NO. OF PASSES	TOTAL VISIBILITY TIME OF STATION	STA- TION	NO. OF PASSES	TOTAL VISIBILITY TIME OF STATION	STA- TION	NO. OF PASSES	TOTAL VISIBILITY TIME OF STATION
001	1	3.34	004	1	5.53	005	1	5.71
006	2	13.09	009	5	33.35			
TOTAL NUMBER OF PASSES WERE		10.	TOTAL VISIBILITY TIME FOR THE VEHICLE WAS		67.03 MIN.			

ITEM	DESCRIPTION	REFERENCE SECTION
55	<p>Visibility Summary. After the data for the spans indicated by the <u>DATA GENERATION</u> I cards has been generated, a summary is printed. It includes the number of passes and the total visibility time for each station and vehicle</p>	12

CONT'D
NEXT
COLUMN!

001	004	005	006	009	x
15	15	25			
15	15	30			
15	15	35			
15	15	40			
15	15	45			
16	15	50			
15	15	55			
16	16	0			
16	16	5			
16	16	10			
15	16	15			
16	16	20			
16	16	25			
16	16	30			
16	16	35			
16	16	40			
16	16	45			
16	16	50			
16	16	55			
16	17	0			
16	17	5			
16	17	10			
16	17	15			
16	17	20			
16	17	25			
16	17	30			
15	17	35			
16	17	40			
16	17	45			
16	17	50			
16	17	55			
15	18	0			
16	18	5			
16	18	10			
16	18	15			
16	18	20			
16	18	25			
16	18	30			
16	18	35			
16	18	40			

ITEM	DESCRIPTION	REFERENCE SECTION
56	<p>Rise-set printer plot. When RSPLT is input $\neq 0$, the passes are given in a printer plot, using RSPLT as the scale. On the page shown, R means rise, S means set, X stands for rise and set in the same interval, and a + indicates continued visibility</p>	2.4.1.1


```

MODEL DATA
DITIN 2
JCSIG 1
SIGMA100
INFOPM1
0 02,00
0 03,00
0 04,00
0 02,02
H0 2.0
IMAXIT2
GPLOT6.
END

```

```

I2 2
2 .1
INTERM4
1082.78E-5
-2.693E-6
-1.56E-6
1.544E-6
HMIN 2.0
HMAX 2.0
15.

```

```

CARD 1
CARD 2
CARD 3
CARD 4
CARD 5
CARD 6
CARD 7
CARD 8
CARD 9
CARD 10
CARD 11
CARD 12

```

```

***** LUNAR GRAVITY MODEL *****
GM = 6.802326500E-05 ER**3/MIN**2 = 1.7313995407E+14 FT**3/SEC**2 = 4.9027777038E+12 M**3/SEC**2
**SPHERICAL MODEL**

```

```

***** EARTH GRAVITY MODEL *****
GM = 5.530393500E-03 ER**3/MIN**2 = 1.4076539841E+16 FT**3/SEC**2 = 3.9860318297E+14 M**3/SEC**2
NO NORMALIZATION WITH 4 TERMS.

```

N	M	CNM	SNM	**	N	M	CNM	SNM
2	0	1.08276010E-03	0.	**	4	0	-1.56000000E-06	0.
3	0	-2.69300010E-06	0.	**	2	2	1.54400000E-06	-7.65000000E-07

```

***** PHYSICAL CONSTANTS *****
GM(ER**3/MIN**2) = 5.530393500E-03
SM(KM**3/MIN**2) = 0.
SGM(ER**3/MIN**2) = 6.802326500E-05
ERFT(FT/ER) = 1.092573900E+07
ETKM(F./KM) = 3.280339900E+03
SSUR0(FT/SFC**2) = 3.217403000E+01
CKEP = 1.011003000E-07
OMEGA(RAD/MIN) = 4.375269100E-03
OMEGA(RAD/MIN) = 4.375269100E-03
OMESL(RAD/MIN) = 0.
SRKM(KM/ER) = 6.378164900E+03
FTNM(FT/NM) = 6.076115500E+03
DGREE(DEG) = 5.729577951E+01
F = 3.352329869E-03
GMLAT(DEG) = 7.830000000E+01
GMLNG(DEG) = 2.910000000E+02
AM(ER) = 2.725062770E-01
ERNM(NM/ER) = 3.443933600E+03
AE(ER) = 1.000000000E+00
SLT = 2.820176300E+03
PI = 3.141592654E+00

```


ITEM	DESCRIPTION	REFERENCE SECTION
1	<p>Card images of the input <u>MODEL</u> data. Those emphasized here are associated with a differential correction run, the others having been discussed earlier:</p> <p>ITIN MAXIT GPLOT KSIG, SIGMA</p>	<p>2.1 2.2.2 2.2.1 2.2.6</p>


```

***** INPUT/OUTPUT CONVERSION FACTORS *****
DF(I/O-ER) = 2.09257300E+07 VF(I/O-ER/MIN) = 3.40762300E+05 AF(I/O-ER/MIN**2) = 5.61270500E+03

***** INTEGRATION INPUTS *****
IFORM = 1 ISENT = 1 NSTEP = 2
NPCMP = 0 IR = 0 ER = 1.00000000E-10
HMIN = 2.00000000E+00 HMAX = 2.00000000E+00 H0 = 2.00000000E+00

***** SPECIAL OPTIONS *****
TAPE2 = 0 TAPE7 = 0 TELEM = 0 PTAPE = 0 NPOOT = 0
PRHO = 0 NOOPR = 0 CLASS = 0 LEMSP = 0 PTNS = 10000

***** CRASH ALTITUDE *****
ECI CRASH ALTITUDE(FT) = 3.00000000E+05 MCI CRASH ALTITUDE(FT) = 3.00000000E+03

***** STATION LOCATIONS *****
STATION SIG REF RA-REF DATUM TYPE LATITUDE LONGITUDE HEIGHT P Q
RADIUS LATITUDE LONGITUDE
001 0 1 1 -0 -0 3.48000000E+01 2.39500000E+02 6.00000000E+02
004 0 1 1 -0 -0 5.75000000E+01 2.07800000E+02 4.26000000E+02
005 0 1 1 -0 -0 2.15000000E+01 2.01700000E+02 9.41000000E+02
006 0 1 1 -0 -0 4.29000000E+01 2.08350000E+02 7.04000000E+02
009 0 1 1 -0 -0 7.65000000E+01 2.91400000E+02 3.96000000E+02

ENTER SEGMENT 01 AT 07.3 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 87.3 CP SECS., 256.0 PP SECS.

***** VEHICLE DATA *****
IVEHID1 IYEAR 1964 IMNTH 8
JDAY 16 T7NF 0 HR 0
MIN 727 SEC 0 IICTYP2
IC 351.5 2 0 3 90.005
4 354.5 5 21351000 6 25056.
5 21360000
IIDRAG1 DRAG .011
OPAG .01
MVPPAM04,60
D ALPHA
D DELTA
D BETA
D A7
D P
D V
D OPAG
TBDOIN4
END

```

2

CARD	1
CARD	2
CARD	3
CARD	4
CARD	5
CARD	6
CARD	7
CARD	8
CARD	9
CARD	10
CARD	11
CARD	12
CARD	13
CARD	14
CARD	15
CARD	16
CARD	17
CARD	18

ITEM	DESCRIPTION	REFERENCE SECTION
2	<p data-bbox="397 514 503 1627">Card images of the input <u>VEHICLE</u> data. The data emphasized here are those for a differential correction run, the others having been discussed earlier:</p> <p data-bbox="527 1491 592 1627">VPRAM BCDIN</p>	<p data-bbox="535 199 568 336">11.1.14</p> <p data-bbox="568 220 600 336">11.2.1</p>

***** OBSERVATIONS *****

STAPASS	VR	MO	DY	HR	MIN	SEC	JD	Y	C	FIELD 1	FIELD 2	FIELD 3	MJD	ST	VEHID	MESSAGE
0050001	64	8	16	12	10	0.0100	1	0	3.39014234E+06	1.72209494E+02	2.76963411E+00	38623	43868.000	1		
0050001	64	8	16	12	11	0.0100	1	0	1.87384769E+06	1.73492974E+02	1.12076600E+01	38623	43860.000	1		
0050001	64	8	16	12	12	0.0100	1	0	5.37420728E+05	1.87872771E+02	5.73590711E+01	38623	43920.000	1		
0050001	64	8	16	12	13	0.0100	1	0	1.35547828E+05	3.47295855E+02	1.84271805E+01	38623	43980.000	1		
0050001	64	8	16	12	14	0.0100	1	0	2.85347371E+05	3.49467701E+02	5.87837413E+00	38623	44040.000	1		
0050001	64	8	16	12	15	0.0100	1	0	4.37758711E+05	3.50191395E+02	5.85905759E-01	38623	44100.000	1		
0040001	64	8	16	12	16	0.0100	1	0	4.03011936E+05	2.27925924E+02	2.86022743E+00	38623	44340.000	1		
0040001	64	8	16	12	20	0.0100	1	0	3.24453020E+06	2.49067115E+02	6.39566421E+00	38623	44400.000	1		
0040001	64	8	16	12	21	0.0100	1	0	3.36338996E+06	2.77562594E+02	7.75133841E+00	38623	44460.000	1		
0040001	64	8	16	12	22	0.0100	1	0	3.57832848E+06	3.03190025E+02	5.71745024E+00	38623	44520.000	1		
0040001	64	8	16	12	23	0.0100	1	0	4.55562572E+05	3.20040201E+02	2.41555425E+00	38623	44580.000	1		
0090001	64	8	16	15	28	0.0100	1	0	5.85478650E+06	2.76761965E+01	1.53988145E+00	38623	55740.000	1		
0090001	64	8	16	15	29	0.0100	1	0	5.30983100E+06	4.27878335E+01	1.53988145E+00	38623	55680.000	1		
0090001	64	8	16	15	30	0.0100	1	0	5.53956587E+06	5.87714689E+01	1.66151901E+00	38623	55800.000	1		
0090001	64	8	16	15	31	0.0100	1	0	5.33731692E+06	7.35905880E+01	6.87099257E-01	38623	55860.000	1		
0090002	64	8	16	15	57	0.0100	1	0	4.8832835E+06	3.17928740E+01	3.24075259E+00	38623	61020.000	1		
0090002	64	8	16	15	58	0.0100	1	0	4.13176431E+06	4.86814040E+01	6.40911377E+00	38623	61080.000	1		
0090002	64	8	16	15	59	0.0100	1	0	3.52064868E+05	7.06168218E+01	8.13172504E+00	38623	61140.000	1		
0090002	64	8	16	17	0	0.0100	1	0	4.06008072E+05	9.29956332E+01	7.28281979E+00	38623	61200.000	1		
0090002	64	8	16	17	1	0.0100	1	0	4.76570170E+05	1.10695971E+02	4.62626881E+00	38623	61260.000	1		
0090002	64	8	16	17	2	0.0100	1	0	5.76533468E+05	1.23037331E+02	1.49506641E+00	38623	61320.000	1		
0090003	64	8	16	18	25	0.0100	1	0	5.17267297E+05	2.36501787E+01	2.04242981E+00	38623	66300.000	1		
0090003	64	8	16	18	26	0.0100	1	0	3.84061613E+05	3.20603692E+01	7.36520897E+00	38623	66360.000	1		
0090003	64	8	16	19	27	0.0100	1	0	2.67830231E+06	4.87761602E+01	1.50081673E+01	38623	66420.000	1		
0090003	64	8	16	19	28	0.0100	1	0	2.01580569E+05	8.45829217E+01	2.30015375E+01	38623	66480.000	1		

ITEM	DESCRIPTION	REFERENCE SECTION
3	<p><u>Observations.</u> Each line represents one OBSERVATION card (or card image) containing the station pass identification, the last two digits of the year; the month, day, hour, minute, and second; the data set type; the covariance code; three measurements; the system time in seconds from midnight; the vehicle identification (which should be the same as the input VEHID); and any pertinent message</p> <p>If the observations are input by binary tape, nothing is printed at this point</p>	<p>11.2.1 15 11.1.2</p>


```

EPOCH
YR/MO/DAY      X,Y,Z,X,Y,DZ      A,B,A,R,V      A,F,I,O,U,IAU      AF,AG,N,L,CMT,PSI
1964/ 8/16     2.11253789414E+07  3.5150000000E+02  2.16730437072E+07  1.42983433809E-02
0.             -3.15721902173E+05  0.             1.44441834610E-02  -2.04739161253E-03
0.             -3.68511052086E+02  9.00050000000E+01  9.55000000000E+01  6.73737489112E-02
0.             -2.45051350318E+03  3.54500000000E+02  3.51149999993E+02  3.51510035590E+02
7.2700000000E+02  2.57351640070E+04  2.13600000000E+07  3.51162206121E-01  -1.62725471159E-01
n.             2.58560000000E+04  2.58560000000E+04  6.38028929616E+02  1.00082155146E+00
NO PLANETARY PERTURBATIONS.
** ATMOSPHERE MODEL ** LOCKHEED
TIME COM/W M/COA
7.27000000E+02  1.00000000E-02  1.00000000E+02
D1 = 5.93000000E+00  D2 = -1.56840000E+01  FLUX = 0.

```

THESE ARE THE 7 PARAMETERS IN THE PARAM MATRIX. 7 ARE P PARAMETERS AND 0 ARE 3 PARAMETERS

NAME	P/O	CURRENT VALUE	BOUND	SIGMA	CONVERSION
0001 ALPHA	P	3.51500000E+02	1.00000000E+00	0.	5.72957795E+01
0001 DELTA	P	0.	1.00000000E+00	0.	5.72957795E+01
0001 PETA	P	9.10050000E+01	1.00000000E+00	0.	5.72957795E+01
0001 A7	P	3.54500000E+02	1.00000000E+00	0.	5.72957795E+01
0001 P	P	2.13600000E+07	1.00000000E+05	0.	2.09257300E+07
0001 V	P	2.58560000E+04	1.00000000E+01	0.	3.48762300E+05
0001 PPAG	P	1.00000000E-02	1.00000000E-02	0.	1.00000000E+00

ENTER SEGMENT 10 AT 88.2 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .9 CP SECS., 3.7 PP SECS.

TRAJECTORY INTEGRATION FOR CASE 1

IVFP	JVEP	MVEP	KVEP	LVEP	ICENTY	ICENT	JNORM	MAJOR	NMASS	NT	JNCPMX	IRAG	IR	ISRP	NEQS	RECMP	NVASSX	NASA	ALPHG	ALG-DEG	TJDATE	TSTART	TSTOP	FLIGHT	SSTEP	CDAW	ER	HMIN	HMAX	H0	NTX	SORD
0	0	0	0	0	1	1	1	1	0	0	0	1	1	1	24	0	0	0	5.662162703E+00	3.244180258E+02	2.438623500E+06	7.270000000E+02	1.303000000E+03	5.760000000E+02	1.000000000E+02	1.000000000E-10	2.000000000E+00	2.000000000E+00	2.000000000E+00	2.000000000E+00	1.500000000E+00	

ITEM	DESCRIPTION	REFERENCE SECTION
4	Parameter list indicating the quantities to be differentially corrected. Shown in tabular form are the name, P- or Q- parameter indicator, current value, input bound and sigma, and input/output conversion factor for each	2.1.5 5 11.1.14

TIME(MME) TYPE ASSOCIATED QUANTITIES * PREDETERMINED EVENT TABLE *

727.0000 TZF30
1303.0000 TSTOP

*** TRAJECTORY START

***** ECI *****
SEG11 ENTRY TIME IS 80.39200

	T =	727.000000	H =	.250000	NSTEP =	0
ALPHA		2.112537894141E+07	-3.685310520857E+02		-3.046630747846E+01	
		-3.157239021720E+06	-2.450633503183E+03		4.55308330712E+00	
		0.	2.573696400698E+04		-9.269647818762E-04	
		1.508738303287E-01	7.026658280390E-03		-7.831510004013E-04	
		1.009540444471E+00	-1.056682594666E-03		-5.241378230337E-03	
		0.	0.		-1.097983001491F-19	
DELTA		-0.	-7.298456764874E-02		7.796797467675E-08	
		-0.	1.090761671814E-02		-1.1652339188860E-08	
		1.020732529732E+00	-6.469626029979E-06		-5.282946063561E-03	
BETA		0.	-7.332203652761E-02		1.784801233243E-07	
		0.	1.095867075294E-02		-2.667557346189E-08	
		0.	-5.439841155098E-06		1.576490526150E-11	
A7		0.	1.090761671814E-02		-2.679811016287E-08	
		0.	7.298456764874E-02		-1.793040486660F-07	
		0.	7.105664137797E-03		-6.686192638061E-09	
P		5.890138633619E-01	0.		1.025158804091E-02	
		-1.478034111296E-01	0.		-1.545030064381E-03	
		0.	0.		8.273446422207E-05	
V		0.	-1.425321210109E-02		9.054266773255E-08	
		0.	-9.478007051295E-02		6.029741570225E-07	
		0.	9.953961945770E-01		-4.823534210103E-06	
DRAC		0.	0.		4.179048465007E-07	
		0.	0.		2.785612136380E-06	
		0.	0.		-1.796317601821E-05	

REFERENCE
SECTION

ITEM

DESCRIPTION

- 5 Variational equations $\partial \underline{r} / \partial p$, $\partial \underline{i} / \partial p$, and $\partial \underline{\ddot{i}} / \partial p$ at epoch in internal units (er, min, rad). They are also printed at trajectory termination

FD=CFS
 GEOPOTENTIAL
 ATMOSPHERIC
 TOTAL

	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	3.080465E+01	-3.046633E+01	4.552923E+00	1.171816E-04	3.080465E+01	1.451160E-04	2.844807E-04	
ATMOSPHERIC	1.056906E-03	2.129158E-05	1.619134E-04	-1.044146E-03	9.154040E-08	-1.055032E-03	-6.290061E-05	
TOTAL	3.020465E+01	-3.046633E+01	4.553005E+00	-9.269648E-04	-3.080465E+01	-9.099163E-04	2.215801E-04	

	STEP	DOUBLED	T	H	NSTEP
NODE	7.715583520117E+02	-2.176582988905E+07	3.262980322285E+06	3.262980322285E+06	45
DT	1.000000000000E+00	3.537911412926E+02	2.373231048850E+03	2.373231048850E+03	77
NODE	9.161292664234E+02	2.112218520803E+07	-3.175314737377E+06	-3.175314737377E+06	
DT	1.000000000000E+00	-3.725292228421E+02	-2.450571977882E+03	-2.450571977882E+03	
NODE	8.505792101379E+02	-2.176031672252E+07	3.281341969531E+06	3.281341969531E+06	
DT	1.000000000000E+00	3.543221992190E+02	2.373711998480E+03	2.373711998480E+03	
NODE	9.052495437519E+02	2.111904558180E+07	-3.19144148025E+06	-3.19144148025E+06	
DT	1.000000000000E+00	-3.764451039999E+02	-2.450006458669E+03	-2.450006458669E+03	
NODE	9.497914183555E+02	-2.175484343843E+07	3.301710320733E+06	3.301710320733E+06	
DT	1.000000000000E+00	3.547775373964E+02	2.379635130283E+03	2.379635130283E+03	
NODE	9.943614921564E+02	2.11159715074E+07	-3.214574854071E+06	-3.214574854071E+06	
DT	1.000000000000E+00	-3.802618536119E+02	-2.448869768818E+03	-2.448869768818E+03	
NODE	1.038895652446E+03	-2.174940212352E+07	3.321068564613E+06	3.321068564613E+06	
DT	1.000000000000E+00	3.551846330693E+02	2.379099125130E+03	2.379099125130E+03	
NODE	1.083465655387E+03	2.111292961254E+07	-3.233696657703E+06	-3.233696657703E+06	
DT	1.000000000000E+00	-3.840137775150E+02	-2.447423489211E+03	-2.447423489211E+03	
NODE	1.127992265585E+03	-2.174394390575E+07	3.340398114736E+06	3.340398114736E+06	
DT	1.000000000000E+00	3.556059319688E+02	2.378469786029E+03	2.378469786029E+03	
NODE	1.172562116777E+03	2.110985991176E+07	-3.252795144273E+06	-3.252795144273E+06	
DT	1.000000000000E+00	-3.877669615493E+02	-2.446106012514E+03	-2.446106012514E+03	
NODE	1.217081055379E+03	-2.173840712948E+07	3.359694427764E+06	3.359694427764E+06	
DT	1.000000000000E+00	3.561029504792E+02	2.378167572974E+03	2.378167572974E+03	
NODE	1.261050421331E+03	2.110671163950E+07	-3.271871947250E+06	-3.271871947250E+06	
DT	1.000000000000E+00	-3.915807895113E+02	-2.445278185376E+03	-2.445278185376E+03	

T	H	NSTEP
-2.128523953293E+07	-5.050055711570E+03	2.816695826715E+01
2.851378919969E+06	3.152604898545E+03	-3.773118593270E+00
4.702934850006E+06	-2.440058016364E+04	-6.204912227728E+08

ALPHA	-1.3623+2841631E-01	-9.088436656835E-03	6.484328686607E-04
	-1.017212811139E+00	-1.469786187184E-02	4.845908917901E-03
	3.071118860762E-04	7.194849530475E-06	-1.329310329866E-06
DELTA	-2.223629979567E-01	6.923775580704E-02	1.090259254607E-03
	3.486708901093E-02	-1.07600899338E-02	-1.648846072365E-04
	-1.029532701896E+00	-1.573248918873E-02	4.892409574229E-03
BETA	-5.950846829238E-01	2.127862353480E-01	8.238380127628E-03
	4.991170083584E-01	-2.670819115936E-02	-2.831687981173E-03
	-4.166991554943E+00	-6.517231652939E-02	1.904434799678E-02
A7	2.073376609690E-02	-9.399691661485E-03	-9.550779774932E-05
	1.633997159981E-01	-7.026605970557E-02	-7.787934028991E-04
	-6.352352055773E-03	-7.178167747321E-03	2.945430374282E-05
R	2.257114554561E+01	-8.641203558093E+00	-1.469266634679E-01
	-1.577246371543E+01	1.141847806475E+00	8.041463864869E-02
	1.256600101207E+02	2.064367198044E+00	-5.882053793044E-01
V	2.921975565344E+02	-1.160413882949E+02	-2.075062236619E+00
	-2.162592031205E+02	1.524962195283E+01	1.093134073450E+00
	1.689179548620E+03	2.854457430755E+01	-7.873182542686E+00
ORAG	-1.788350615598E-01	8.611654347690E-02	1.902624164764E-03
	1.512410902734E-01	-1.119862927215E-02	-8.612346895912E-04
	-1.262497928033E+00	-2.316321440878E-02	5.765712037801E-03

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOCENTRICAL	2.908905E+01	2.915696E+01	-3.773118E+00	-6.204916E+00	-2.908805E+01	-1.798890E-02	-1.910441E-03	
ATMOSPHERIC	3.519705E-06	6.741910E-07	-6.553724E-07	3.391798E-06	-1.217397E-08	3.513011E-06	2.166337E-07	
TOTAL	2.908905E+01	2.916696E+01	-3.773119E+00	-6.204912E+00	-2.908805E+01	-1.799241E-02	-1.910224E-03	

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 6.931 SECONDS TO INTEGRATE A SPAN OF 576.0000 MINUTES ***


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*** FROM 777.000 TO 1303.000 MINUTES FROM MIDNIGHT OF EPOCH ***
ENTER SEGMENT 20 AT 95.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 7.1 CD SECS., 11.2 PD SECS.

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COSEPARATION RESIDUALS

STABSS	YEAR	MO	DAY	HR	MIN	SEC	RNG	AZ	EL	MJD	ST	
00050001	1964	8	15	12	10	1.0300	7.2193E+02	RNG	-5.7748E-01	-1.5353E-01	38623	43800.000
00050001	1964	8	15	12	11	1.0070	-1.3801E+00	RNG	-1.0051E+00	-2.6631E-01	38623	43860.000
00050001	1964	8	15	12	11	1.0070	-1.2039E+04	RNG	-3.1996E+00	2.7212E-01	38623	43920.000
00050001	1964	8	15	12	13	1.0070	-6.1736E+03	RNG	1.2433E+00	-2.9075E-01	38623	43980.000
00050001	1964	8	15	12	14	1.0000	-3.8206E+03	RNG	5.5980E-01	-1.7079E-01	38623	44040.000
00050001	1964	8	15	12	15	1.0070	-2.8554E+03	RNG	7.4050E-01	-1.1805E-01	38623	44100.000
00040001	1964	8	15	12	19	1.0070	-1.7570E+04	RNG	-1.1783E-01	-9.4941E-02	38623	44340.000
00040001	1964	8	15	12	20	1.0070	-1.7816E+04	RNG	-8.6713E-03	-1.1780E-01	38623	44400.000
00040001	1964	8	15	12	21	1.0070	-1.7983E+04	RNG	1.4065E-01	-1.4985E-01	38623	44460.000
00040001	1964	8	15	12	22	1.0070	-7.2055E+03	RNG	1.7872E-01	-1.6847E-01	38623	44520.003
00040001	1964	8	15	12	23	1.0070	-1.4351E+03	RNG	1.7872E-01	-1.6847E-01	38623	44520.003
00040001	1964	8	15	12	23	1.0070	-1.4351E+03	RNG	1.7872E-01	-1.6847E-01	38623	44520.003
00040001	1964	8	15	15	25	1.0070	-1.2982E+05	RNG	3.4447E+00	2.2904E-01	38623	44580.000
00090001	1964	8	15	15	29	1.0000	-4.0564E+04	RNG	3.9272E+00	-2.7734E-02	38623	55740.000
00090001	1964	8	15	15	30	1.0070	5.8452E+04	RNG	7.9207E+00	-3.4042E-01	38623	55800.000
00090001	1964	8	15	15	31	1.0070	1.4832E+05	RNG	3.4197E+00	-5.9195E-01	38623	55860.000
00090002	1964	8	15	16	57	1.0000	-3.5218E+05	RNG	4.9318E+00	1.0259E+00	38623	61020.000
00090002	1964	8	15	16	58	1.0000	-2.2774E+05	RNG	7.0022E+00	7.8108E-01	38623	61080.000
00090002	1964	8	15	16	59	1.0070	-3.7413E+04	RNG	8.5014E+00	-2.1927E-02	38623	61140.000
00090002	1964	8	15	17	0	1.0070	1.7160E+05	RNG	7.7989E+00	-1.0276E+00	38623	61200.000
00090002	1964	8	15	17	1	1.0070	3.2728E+05	RNG	5.5789E+00	-1.4818E+00	38623	61260.000
00090002	1964	8	15	17	2	1.0070	4.1849E+05	RNG	3.7989E+00	-1.4921E+00	38623	61320.000
00090003	1964	8	15	18	25	1.0070	-6.8546E+05	RNG	2.8032E+00	1.9257E+00	38623	66300.000
00090003	1964	8	15	18	26	1.0070	-6.4581E+05	RNG	4.3128E+00	2.5937E+00	38623	66360.000
00090003	1964	8	15	18	27	1.0070	-5.2705E+05	RNG	9.9434E+00	3.7369E+00	38623	66420.000
00090003	1964	8	15	18	29	1.0070	-2.2054E+05	RNG	1.9821E+01	2.6701E+00	38623	66480.000
00090003	1964	8	15	18	23	1.0070	2.2744E+05	RNG	1.7870E+01	-4.3395E+00	38623	66540.000
00090003	1964	8	15	18	31	1.0070	5.8760E+05	RNG	3.3667E+00	-4.4874E+00	38623	66600.000
00090003	1964	8	15	18	32	1.0070	7.1764E+05	RNG	2.1718E+00	-2.3600E+00	38623	66720.000
00060001	1964	8	15	18	33	1.0070	-7.1169E+05	RNG	1.8713E+00	1.9399E+00	38623	66780.000
00060001	1964	8	15	18	34	1.0070	-7.0566E+05	RNG	3.0210E+00	2.6756E+00	38623	66840.000
00060001	1964	8	15	18	35	1.0070	-5.8270E+05	RNG	5.8862E+00	4.4637E+00	38623	66900.003
00060001	1964	8	15	18	36	1.0070	-4.3394E+05	RNG	1.5855E+01	8.5635E+00	38623	66960.000
00060001	1964	8	15	18	37	1.0070	9.2051E+04	RNG	2.9397E+01	-4.7912E+00	38623	67020.000
00060001	1964	8	15	18	38	1.0070	5.8605E+05	RNG	9.2309E+01	-1.0165E+01	38623	67080.000

REFERENCE SECTION

DESCRIPTION

ITEM

6 Observation residuals. Each line corresponds to one input observation set or card and contains the station-pass identification in year, month, day, hour, minute, and second; three pairs of measurement residuals and identification; the modified Julian date; and the system time in seconds from midnight

The residuals are the unnormalized differences between the input measurements (modified by bias and/or refraction corrections) and the corresponding values for the same measurement types computed from the integrated trajectory position at the observation time. The observation names are abbreviated as follows:

RNG	Range	CM3	Three-way cumulative doppler
AZ	Azimuth	DOP	Doppler
EL	Elevation	TWD	Two-way doppler
TRA	Topocentric right ascension	SRR	SGLS range rate
TD	Topocentric declination	AX	X-antenna
THA	Topocentric hour angle	AY	Y-antenna
GRA	Geocentric right ascension	CC3	JPL two- or three-way doppler
GD	Geocentric declination	TNT	Tranet doppler
U	u	GCR	Geociever range difference
V	v	V2	Vehicle-vehicle range
H	Height	V2D	Vehicle-vehicle range rate
X	\hat{x}	S2	Station-vehicle-vehicle range
Y	\hat{y}	S2D	Station-vehicle-vehicle range rate
Z	\hat{z}	S3	Station-vehicle-vehicle-vehicle range
P	P		
Q	Q	S3D	Station-vehicle-vehicle-vehicle range rate
RD	Range rate	V3	Vehicle-vehicle-vehicle range
PD	P rate	TDA	Time difference of arrival
QD	Q rate	TDA	Time of arrival
ACC	Accelerometer	N	Time-of-arrival counter
CM1	One-way cumulative doppler		

STA	N TYP	PMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
0060001	1964	8 15 18 39	3.0000	7.0206E+05	RNG	2.9163E+00	AZ	38623 67140.000
0060001	1964	8 15 18 40	3.0000	7.3429E+05	RNG	1.1680E+00	AZ	38623 67200.000
0060001	1964	8 15 18 41	3.0000	7.4494E+05	RNG	5.2410E-01	AZ	38623 67260.000
0090004	1964	8 15 19 54	3.0000	-9.2242E+05	RNG	3.9277E-02	AZ	38623 71640.000
0090004	1964	8 15 19 55	3.0000	-9.1014E+05	RNG	-5.0427E-02	AZ	38623 71700.000
0090004	1964	8 15 19 56	3.0000	-8.4236E+05	RNG	-8.0807E-01	AZ	38623 71700.000
0090004	1964	8 15 19 57	3.0000	-8.2121E+05	RNG	-9.8093E-01	AZ	38623 71800.000
0090004	1964	8 15 19 58	3.0000	7.5414E+05	RNG	-3.4655E+00	AZ	38623 71800.000
0090004	1964	8 15 19 59	3.0000	8.836E+05	RNG	-1.2950E+00	AZ	38623 71940.000
0090004	1964	8 15 20 0	3.0000	9.1358E+05	RNG	-7.5093E-01	AZ	38623 72000.000
0090004	1964	8 15 20 1	3.0000	9.2012E+05	RNG	-5.3110E-01	AZ	38623 72060.000
0060002	1964	8 15 20 2	3.0000	-6.5857E+05	RNG	-6.0141E+00	AZ	38623 72120.000
0060002	1964	8 15 20 3	3.0000	-5.1788E+05	RNG	-8.1363E+00	AZ	38623 72120.000
0060002	1964	8 15 20 4	3.0000	-3.0667E+05	RNG	-1.0234E+01	AZ	38623 72120.000
0060002	1964	8 15 20 5	3.0000	-4.0119E+04	RNG	-1.1161E+01	AZ	38623 72300.000
0060002	1964	8 15 20 6	3.0000	2.2402E+05	RNG	-1.0203E+01	AZ	38623 72360.000
0060002	1964	8 15 20 7	3.0000	4.3282E+05	RNG	-8.3794E+00	AZ	38623 72420.000
0090005	1964	8 15 21 22	3.0000	-1.0705E+06	RNG	-3.6137E+00	AZ	38623 76920.000
0090005	1964	8 15 21 23	3.0000	-1.0197E+06	RNG	-6.6744E+00	AZ	38623 76980.000
0090005	1964	8 15 21 24	3.0000	-3.6017E+05	RNG	-3.2194E+01	AZ	38623 77100.000
0090005	1964	8 15 21 25	3.0000	4.6302E+05	RNG	-2.7804E+01	AZ	38623 77160.000
0090005	1964	8 15 21 26	3.0000	8.7611E+05	RNG	-1.2828E+01	AZ	38623 77220.000
0090005	1964	8 15 21 27	3.0000	1.0081E+06	RNG	-6.4230E+00	AZ	38623 77280.000
0090005	1964	8 15 21 33	3.0000	-1.0512E+06	RNG	3.8996E+00	AZ	38623 77580.000
0090005	1964	8 15 21 34	3.0000	-1.0094E+06	RNG	6.0810E+00	AZ	38623 77640.000
0090005	1964	8 15 21 35	3.0000	-9.3781E+05	RNG	1.0721E+01	AZ	38623 77780.000
0090005	1964	8 15 21 36	3.0000	-6.3781E+05	RNG	2.1169E+01	AZ	38623 77780.000
0090005	1964	8 15 21 37	3.0000	-1.9800E+03	RNG	3.1735E+01	AZ	38623 77820.000
0090005	1964	8 15 21 38	3.0000	6.7253E+05	RNG	2.0250E+01	AZ	38623 77880.000
0090005	1964	8 15 21 39	3.0000	9.6476E+05	RNG	9.2024E+00	AZ	38623 77940.000
0090005	1964	8 15 21 40	3.0000	1.0652E+06	RNG	4.5307E+00	AZ	38623 78000.000

TOTAL FOOT SUMMARY

STA	N TYP	PMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
001	8 RNG	8.6E+03	-1.1E+05	8 AZ	1.6E+01	1.6E+02	1.3E+01	8 EL 5.2E+00 5.2E+01 -4.6E-01
004	5 PNG	1.3E+04	-1.2E+04	5 AZ	1.3E-01	1.3E+01	6.5E-02	5 EL 1.4E-01 1.4E+00 -1.4E-01
005	6 PNG	6.0E+03	-4.3E+03	6 AZ	1.5E+00	1.5E+01	-4.4E-01	6 EL 2.2E-01 2.2E+00 -1.2E-01
006	15 PNG	5.6E+03	-4.0E+04	15 AZ	1.1E+01	1.1E+02	1.0E+00	15 EL 4.3E+00 4.3E+01 -4.8E-01
009	33 PNG	6.4E+05	3.4E+03	33 AZ	2.0E+01	2.0E+02	-2.6E+00	33 EL 6.9E+00 6.9E+01 1.1E-01

ENTER SEGMENT 30 AT 97.1 SECONDS. EXECUTION TIME FOR SEGMENT 20 WAS 1.8 CP SECS., 9.8 PP SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
7	<p data-bbox="395 569 635 1673"><u>Edit summary.</u> The RMS of the residuals for each measurement type from each station is computed by the residuals editor. Included in the printout are the station identification, the number of residuals included in the RMS (i.e., the total number for that station and type minus the number deleted by the editor on this iteration), the RMS, the RMS divided by the input weighting sigma, and the mean value of the residuals. The measurement type indicators are the same as those used for residuals (Item 6)</p> <p data-bbox="667 569 756 1673">Because of storage constraints, the residuals editor accumulates residuals and makes editing checks only for the first 6 measurement types for the first 30 stations</p>	2.2.4

ITERATION NUMBER 1

201 OBSERVATIONS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS BEST SO FAR
CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	ROUND	NEW VALUE	SIGMA
0001 ALPHA	3.51499999999999996E+02	3.29208724E-01	1.00000000E+00	3.51829208723932E+02	1.25190034E-04
0001 DELTA	0.	1.13160500E-01	1.00000000E+00	1.131604999953416E-01	2.10518024E-04
0001 BETA	9.00049999999999999E+01	-2.26835100E-01	1.00000000E+00	8.97781648996747E+01	9.19896857E-05
0101 AZ	3.54499999999999996E+02	6.64006620E-02	1.00000000E+00	3.54566400661983E+02	7.31252969E-05
0001 R	2.13599999999999998E+07	-1.23030329E+04	1.00000000E+05	2.13476969170890E+07	5.73271117E+01
0001 V	2.58559999999999999E+04	-5.17544231E-01	1.00000000E+08	2.58554824557692E+04	7.08926739E-02
0001 DRAG	1.00000000000000000E-02	-8.77565717E-03	1.00000000E-02	1.22434282701928E-03	8.45819835E-06

CORRECTIONS HITTING ROUNDS. 5 ITERATIONS USED IN FINDING Z

RMS FOR THIS SOLUTION =

3.4716713914E+03

PREDICTED RMS FOR NEXT SOLUTION =

4.8322106976E+02

 $XT((ATA)X) = 2.37501378E+09$
 $XT(ATB) = 2.37561893E+09$
 $RATIO = 9.99745266E-01$

CORRELATION MATRIX DETERMINANT = 7.26217525E-07

0001 ALPHA	0001 DELTA	0001 BETA	0001 AZ	0001 R	0001 V	0001 DRAG
1.000000000	1.000000000	1.000000000	1.000000000	1.000000000	1.000000000	1.000000000
.177635916	1.000000000	1.000000000	1.000000000	1.000000000	1.000000000	1.000000000
-.122165667	-.533863245	1.000000000	1.000000000	1.000000000	1.000000000	1.000000000
.460579679	.205133632	-.234238491	1.000000000	1.000000000	1.000000000	1.000000000
.169899883	.850313741	-.615787104	1.000000000	1.000000000	1.000000000	1.000000000
-.167862861	-.845366506	.632669139	-.162982940	-.999457483	1.000000000	1.000000000
.165362253	.443753863	.054309304	.072642556	.406561987	-.378328785	1.000000000

ENTER SEGMENT 40 AT 97.3 SECONDS. EXECUTION TIME FOR SEGMENT 30 WAS .2 CP SECS., 2.6 PP SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
8	Iteration number. TRACE makes the differential correction, or orbit determination, by computing a series of differential corrections of the parameters selected by the user. The iteration number is advanced each time a set is recomputed and indicates the number of times the orbit determination algorithm has been performed	2.2.2
9	Observation count. The number of individual measurements included in the current (best) least squares computation is indicated	
10	Convergence indicator. If the weighted RMS for all residuals is less than that for any previous iteration, the correction process is converging, and the message shown is printed. If the current RMS is greater than the smallest RMS obtained on previous iterations, the message CURRENT ITERATION IS NOT GOOD (SOS X.XXXXXXXXE+XX) is printed at this point.	2.2.2
11	The current solution is shown, one parameter per line, starting with the name (Item 4). If the iteration has been successful (i.e., if the overall RMS has been lowered), the current value is the parameter value used in the integration, partial derivatives, and residuals computations just completed. For the first iteration, it is the input value of the parameter. If an iteration is had, the value produced for the lowest RMS is recovered from memory and is printed as the current value The correction, the solution of the system of normal equations associated with the current (best) iteration, is also shown on the line, as is the bound, the current value of the number used to limit the correction size. In general, these bounds are automatically increased on a good iteration and decreased on a bad one. The last two columns contain the new value (correct value plus correction) to be used for the next iteration and the a priori sigma for the parameter	2.2.3
12	Indications that the correction sizes have been controlled by solving the system so that the constraint of the bounds is satisfied. The number of iterations to determine the Lagrange multiplier λ is also shown. If the normal equations were solved without applying the bounds, nothing would be printed at this point	
13	RMS. The quantity to be minimized in the differential correction process is the RMS of the normalized residuals for the current iteration	
14	Predicted RMS. If the fitting process is converging in a completely linear manner, this will be the RMS on the next iteration; it may be compared with the current RMS (Item 13) to measure the degree to which the process has already converged	
15	The equation being solved is $A^T W \Delta P = A^T W B$; therefore, the solution should also satisfy $\Delta P^T A^T W \Delta P = \Delta P^T A^T W B$. By comparing the ratio of the two sides of the preceding equation to 1, an estimation of the quality of the matrix inversion may be obtained and, implicitly, of the normal matrix conditioning. This comparison is valid only when bounds are not hit	
16	Determinant of the correlation matrix	
17	Correlation matrix, the correlation coefficients for the parameter set. These values are computed directly from the covariance matrix (i.e., the inverse normal matrix). Row sequence is the same as column sequence	

TRAJECTORY INTEGRATION FOR CASE 1

★ PREDETERMINED EVENT TABLE ★

727.0000 TZFR0
1303.0000 TSTOP

TRAJECTORY START

T	=	727.00000	I	=	.25000	NSTEP	=
2.11302512784E+07			-2.991917404612E+02			-3.052702432160E+01	
-3.0334021339711E+06			-2.430441368898E+03			4.362852174980E+00	
4.216217155988E+04			2.573925818813E+04			-5.077158946111E-02	

REFERENCE
SECTION

ITEM

DESCRIPTION

- 18 Initial conditions and characteristics for the next iteration are fully explained in the epoch print (Item 42) of the previous case

Preceding page blank

ALPHA	1.449839349170E-01 1.009315734373E+00 0.	6.968761729401E-03 -8.578672077264E-04 0.	-7.538634032513E-04 -5.251821922072E-03 5.072796977429E-10
DELTA	-1.994334437437E-03 2.863518731332E-04 1.020152593830E+00	-7.305254656714E-02 1.04890208885E-02 1.41271615228E-04	1.013851645742E-05 -1.455639639366E-06 -5.288997732691E-03
BETA	0. 0. 0.	-7.338613986721E-02 1.050946047628E-02 1.393241626287E-04	2.910517841894E-08 -4.167985675079E-09 -5.589291141101E-11
AZ	0. 0. 0.	1.047523697341E-02 7.305409839516E-02 7.019930643232E-03	-4.189457598863E-09 -2.924014878256E-08 -1.055755549733E-09
R	9.898458823081E-01 -1.421740615554E-01 1.975022023389E-03	0. 0. 0.	1.027953859891E-02 -1.478110678485E-03 3.530004569560E-05
V	0. 0. 0.	-1.157169435817E-02 -9.400100628776E-02 9.955048501673E-01	1.249910573710E-08 9.763856698058E-08 -7.860128671986E-07
DRAG	0. 0. 0.	0. 0. 0.	4.833824156621E-07 3.688586245117E-06 -2.390669173616E-05
POPCFS		(EXTERNAL UNITS)	IN-TRACK CROSS-TRACK
POTENTIAL	3.084011E+01-3.052703E+01 1.721854E-04 3.440109E-06 3.084011E+01-3.052702E+01	4.382825E+00-6.050145E-02 2.625072E-05-1.701378E-04 4.382852E+00-6.077159E-02	3.353302E+01 3.353302E-04 -1.718791E-04-1.024360E-05 1.634510E+01 2.578042E-04
ATMOSPHERIC			
TOTAL			
STEP	DOUBLED	T = 737.000000	H = .500000
STEP	COUPLED	T = 752.500000	H = 1.000000
NOFF	T = 7.716776901297E+02	-2.174592635526E+07	3.128044651412E+06
NOFF	DT = 1.00000000000E+00	4.363066596235E+02	2.341032215047E+03
NOFF	DT = 8.159439381329E+02	2.11280778157E+07	-3.048921452957E+06
NOFF	DT = 1.00000000000E+00	-2.531640793088E+02	-2.437807435119E+03
			NSSTEP = 39
			NSSTEP = 69
			8.185382931127E-02
			-2.501100242896E+04
			-8.866507996913E-03
			2.573986349851E+04

MODE	T =	8.608439784349E+02	-2.174307672354E+07	3.147574109853E+06	6.346018681070E-02
DT	=	1.00000000000E+00	4.367489585501E+02	2.341259412302E+03	-2.501018063800E+04
MODE	T =	9.049131125587E+02	2.112480922144E+07	-3.067826874256E+06	-3.145012691736E-02
DT	=	1.00000000000E+00	-2.570751312713E+02	-2.437496916786E+03	2.574014521037E+04
MODE	T =	9.496085345421E+02	-2.174027955617E+07	3.167115480898E+06	4.271287274222E-02
DT	=	1.00000000000E+00	4.371065454945E+02	2.340923513896E+03	-2.501069558271E+04
MODE	T =	9.934809223146E+02	-2.112160903266E+07	-3.086737009815E+06	-5.239012997875E-02
DT	=	1.00000000000E+00	-2.609021288274E+02	-2.436611139646E+03	2.574174086916E+04
MODE	T =	1.038572072318E+03	-2.173752250007E+07	3.186650039577E+06	2.199108108714E-02
DT	=	1.00000000000E+00	4.374054250921E+02	2.340136156310E+03	-2.501146135307E+04
MODE	T =	1.082847949403E+03	2.111844585457E+07	-3.105634339711E+06	-6.394101090157E-02
DT	=	1.00000000000E+00	-2.646769896776E+02	-2.435406138572E+03	2.574108312266E+04
MODE	T =	1.127534984272E+03	-2.173475444553E+07	3.206160942905E+06	6.063245481935E-03
DT	=	1.00000000000E+00	4.377056630312E+02	2.339242337792E+03	-2.501022625244E+04
MODE	T =	1.171814315422E+03	2.111526079807E+07	-3.124507502435E+06	-8.281080897144E-02
DT	=	1.00000000000E+00	-2.684624881963E+02	-2.434319116268E+03	2.571143064371E+04
MODE	T =	1.216497109383E+03	-2.173191504376E+07	3.225642388976E+06	1.371241885715E-06
DT	=	1.00000000000E+00	4.380669398760E+02	2.338670267869E+03	-2.501004494494E+04
MODE	T =	1.260779610736E+03	2.111200155498E+07	-3.143357829477E+06	-9.027222714296E-02
DT	=	1.00000000000E+00	-2.723159956769E+02	-2.433715458936E+03	2.574183413167E+04

	T =	1303.500000	1 =	1.000000	NSTEP =	620
ALPHA		-2.158139373011E+07		-2.936560141066E+03	2.857982166037E+01	
		2.941512320333E+06		2.820751815171E+03	-3.895256128281E+00	
		2.928945390395E+06		-2.478242573033E+04	-3.867091391020E+00	
		-1.405703253351E-01		-8.112355054985E-03	6.694580358838E-04	
		-1.031332567536E+00		-8.414333182920E-03	4.916945383847E-03	
		3.631775022101E-04		5.226738822887E-06	-1.632595318533E-06	
DELTA		-1.387830212820E-01		7.05656936537E-02	6.574981670973E-04	
		2.129733688308E-02		-1.054634674355E-02	-1.009641314532E-04	
		-1.047049174250E+00		-9.559078210560E-03	4.977361441106E-03	
BETA		-3.140554057470E-01		1.967200090466E-01	3.662521752306E-03	
		4.237426207680E-01		-2.575880859943E-02	-2.315171961345E-03	
		-3.917007913912E+00		-3.740467308669E-02	1.832581816705E-02	
AZ		9.128512328766E-03		-8.972395236228E-03	-3.906947413612E-05	
		8.055012853788E-02		-7.104564900142E-02	-3.846045274812E-04	
		-1.608918734680E-02		-7.046327340826E-03	7.587327516339E-05	

R 1.144856139165E+01 -1.009066847643E-01
 -1.359557914992E+01 7.112715583158E-02
 1.233937145524E+02 -5.802036060332E-01

V 1.452234490322E+02 -1.520343930412E+00
 -1.862350275205E+02 1.000672309522E+00
 1.708311085917E+03 -8.008410938828E+00

DRAG -9.78352270257E-02 2.136118776008E-03
 1.920342549582E-01 -1.149855285102E-03
 -1.842454554114E+00 8.525382604848E-03

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 2.910213E+01 2.857983E+01 -3.895257E+00 -3.867092E+00 -2.910213E+01 -1.142734E-02 -1.238510E-03
 ATMOSPHERIC 4.495445E-07 4.833679E-08 -7.803580E-08 4.400730E-07 7.376945E-10 -4.486663E-07 2.807590E-08
 TOTAL 2.910213E+01 2.857983E+01 -3.895257E+00 -3.867092E+00 -2.910213E+01 -1.142734E-02 -1.238482E-03

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 6.885 SECONDS TO INTEGRATE A SPAN OF 576.500 MINUTES ***
 *** FROM 727.000 TO 1303.500 MINUTES FROM MIDNIGHT OF EPOCH ***
 ENTER SEGMENT 20 AT 104.5 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 7.0 CP SECS., 11.3 PP SECS.

OBSERVATION RESIDUALS

STAPASS	YEAR	MO	DAY	HR	MIN	SEC	RNG	1.6215E+00	AZ	-3.3328E-01	EL	MJD	ST
0050001	1964	8	16	12	10	0.0000	RNG	1.6215E+00	AZ	-3.3328E-01	EL	38623	43800.000
0050001	1964	8	16	12	11	0.0000	RNG	2.9479E+00	AZ	-8.0831E-01	EL	38623	43860.000
0050001	1964	8	16	12	12	0.0000	RNG	9.3419E+00	AZ	-4.2212E+00	EL	38623	43920.000
0050001	1964	8	16	12	13	0.0000	RNG	-4.0375E+00	AZ	-1.0205E+00	EL	38623	43980.000
0050001	1964	8	16	12	14	0.0000	RNG	-1.9082E+00	AZ	-6.6809E-01	EL	38623	44040.000
0050001	1964	8	16	12	15	0.0000	RNG	-1.2258E+00	AZ	-5.1925E-01	EL	38623	44100.000
0040001	1964	8	15	12	19	0.0000	RNG	1.0505E+00	AZ	-9.6596E-01	EL	38623	44340.000
0040001	1964	8	15	12	20	0.0000	RNG	1.0582E+00	AZ	-1.3543E+00	EL	38623	44400.000
0040001	1964	8	16	12	21	0.0000	RNG	6.1915E-01	AZ	-1.6029E+00	EL	38623	44460.000

0940001	1964	8 15 12 22	0.0000	6.5667E+04	RNG	9.8096E-02	AZ	-1.4357E+03	EL	38623	44520.000
0040001	1964	8 15 12 23	0.0000	6.8526E+04	RNG	-1.0075E-01	AZ	-1.1507E+00	EL	38623	44580.000
0090001	1964	8 16 15 28	0.0000	-6.1104E+03	RNG	3.0765E-01	AZ	-8.0133E-01	EL	38623	55600.000
0090001	1964	8 16 15 29	0.0000	-6.8573E+03	RNG	3.8295E-01	AZ	-8.4310E-01	EL	38623	55740.000
0090001	1964	8 16 15 30	0.0000	-2.7751E+03	RNG	4.4800E-01	AZ	-8.4095E-01	EL	38623	55800.000
0090001	1964	8 16 15 31	0.0000	5.2159E+03	RNG	4.8157E-01	AZ	-7.9429E-01	EL	38623	55860.000
0090002	1964	8 15 16 57	0.0000	1.5211E+03	RNG	1.1618E-01	AZ	-1.0140E+00	EL	38623	61020.000
0090002	1964	8 16 16 58	0.0000	-8.4322E+03	RNG	1.4544E-01	AZ	-1.1552E+00	EL	38623	61080.000
0090002	1964	8 16 16 59	0.0000	-1.3588E+04	RNG	2.1944E-01	AZ	-1.2119E+00	EL	38623	61140.000
0090002	1964	8 15 17 1	0.0000	-1.0744E+04	RNG	3.0655E-01	AZ	-1.1336E+00	EL	38623	61200.000
0090002	1964	8 15 17 1	0.0000	-2.2753E+03	RNG	3.5173E-01	AZ	-9.7400E-01	EL	38623	61260.000
0090002	1964	8 15 17 2	0.0000	7.3316E+03	RNG	3.6114E-01	AZ	-8.1401E-01	EL	38623	61320.000
0090003	1964	8 16 18 25	0.0000	2.0690E+04	RNG	1.9155E-01	AZ	-1.0434E+00	EL	38623	66300.000
0090003	1964	8 15 18 26	0.0000	6.5799E+03	RNG	1.6134E-01	AZ	-1.3569E+00	EL	38623	66360.000
0090003	1964	8 15 18 27	0.0000	-1.1036E+04	RNG	9.5496E-02	AZ	-1.0453E+00	EL	38623	66420.000
0090003	1964	8 15 18 28	0.0000	-2.8822E+04	RNG	2.1144E-02	AZ	-2.2312E+00	EL	38623	66480.000
0090003	1964	8 15 18 29	0.0000	-2.6325E+04	RNG	1.2254E-01	AZ	-1.9183E+00	EL	38623	66540.000
0090003	1964	8 15 18 30	0.0000	-1.1609E+04	RNG	2.1121E-01	AZ	-1.3912E+00	EL	38623	66600.000
0090003	1964	8 15 18 31	0.0000	1.8438E+03	RNG	2.4020E-01	AZ	-1.0271E+00	EL	38623	66660.000
0090003	1964	8 15 18 32	0.0000	1.3232E+04	RNG	2.5305E-01	AZ	-7.9933E-01	EL	38623	66720.000
0060001	1964	8 16 18 33	0.0000	-7.6649E+04	RNG	-7.9060E-02	AZ	-5.3474E-01	EL	38623	66780.000
0060001	1964	8 15 18 34	0.0000	-8.8371E+04	RNG	-9.8217E-02	AZ	-5.9098E-01	EL	38623	66840.000
0050001	1964	8 16 18 35	0.0000	-1.0111E+05	RNG	1.1402E-02	AZ	-5.5867E-01	EL	38623	66900.000
0060001	1964	8 15 18 36	0.0000	-1.0593E+05	RNG	1.1116E+00	AZ	-4.8510E-04	EL	38623	66960.000
0060001	1964	8 15 18 37	0.0000	-4.1937E+04	RNG	3.7652E+00	AZ	-1.5807E+00	EL	38623	67020.000
0060001	1964	8 15 18 38	0.0000	3.2485E+04	RNG	2.1183E+00	AZ	-1.8628E+00	EL	38623	67080.000
0060001	1964	8 15 18 39	0.0000	6.4311E+04	RNG	1.2775E+00	AZ	-1.2035E+00	EL	38623	67140.000
0060001	1964	8 16 18 40	0.0000	8.1036E+04	RNG	9.1514E-01	AZ	-8.3730E-01	EL	38623	67200.000
0060001	1964	8 15 18 41	0.0000	9.2000E+04	RNG	7.2426E-01	AZ	-6.2982E-01	EL	38623	67260.000
0090004	1964	8 15 19 54	0.0000	3.9279E+03	RNG	4.3546E-01	AZ	-1.2301E+00	EL	38623	71640.000
0090004	1964	8 16 19 55	0.0000	-8.4590E+03	RNG	5.2603E-01	AZ	-1.7714E+00	EL	38623	71700.000
0090004	1964	8 15 19 56	0.0000	-4.2444E+04	RNG	7.3920E-01	AZ	-2.8249E+00	EL	38623	71760.000
0090004	1964	8 15 19 57	0.0000	-3.2978E+04	RNG	-1.8495E-01	AZ	-1.1511E+00	EL	38623	71820.000
0090004	1964	8 15 19 58	0.0000	-3.2978E+04	RNG	-1.8495E-01	AZ	-2.2512E+00	EL	38623	71880.000
0090004	1964	8 15 19 59	0.0000	-7.7099E+03	RNG	3.8521E-03	AZ	-1.4418E+00	EL	38623	71940.000
0090004	1964	8 16 20 0	0.0000	7.3660E+03	RNG	8.2113E-02	AZ	-1.0324E+00	EL	38623	72000.000
0090004	1964	8 15 20 1	0.0000	2.0179E+04	RNG	1.2390E-01	AZ	-8.0225E-01	EL	38623	72060.000
0060002	1964	8 15 20 2	0.0000	-4.1328E+04	RNG	-5.1514E-01	AZ	-6.0920E-01	EL	38623	72120.000
0060002	1964	8 15 20 3	0.0000	-2.7986E+04	RNG	-7.4698E-01	AZ	-7.0650E-01	EL	38623	72180.000
0060002	1964	8 15 20 4	0.0000	-4.9266E+03	RNG	-9.2915E-01	AZ	-8.1586E-01	EL	38623	72240.000
0060002	1964	8 15 20 5	0.0000	2.5070E+04	RNG	-9.3451E-01	AZ	-8.9165E-01	EL	38623	72300.000
0060002	1964	8 15 20 6	0.0000	5.4716E+04	RNG	-7.5593E-01	AZ	-8.8289E-01	EL	38623	72360.000
0060002	1964	8 15 20 7	0.0000	7.8674E+04	RNG	-5.1917E-01	AZ	-8.0346E-01	EL	38623	72420.000

0090005	1964	8 15 21 22	1.0000	-6.6495E+03	RNG	5.5421E-01	A7	-1.0323E+00	EL	38623	76920.000
0090005	1964	8 15 21 23	1.0000	-2.4423E+04	RNG	5.1460E-01	AZ	-1.3509E+00	EL	38623	76980.000
0090005	1964	8 15 21 24	1.0000	-4.7316E+04	RNG	5.6663E-01	AZ	-1.7762E+00	EL	38623	77040.000
0090005	1964	8 15 21 25	1.0000	-6.0912E+04	RNG	-9.2395E-02	A7	-2.0151E+00	EL	38623	77100.000
0090005	1964	8 15 21 26	1.0000	-3.5964E+04	RNG	-4.7476E-01	A7	-1.9004E+00	EL	38623	77160.000
0090005	1964	8 15 21 27	1.0000	-8.7365E+03	RNG	-2.9727E-01	AZ	-1.4333E+00	EL	38623	77220.000
0090005	1964	8 15 21 28	1.0000	1.0382E+04	RNG	-1.4865E-01	A7	-1.0838E+00	EL	38623	77280.000
0010001	1964	8 15 21 33	1.0000	-1.1744E+05	RNG	2.5720E-02	A7	-3.7427E-01	EL	38623	77580.000
0010001	1964	8 15 21 34	1.0000	-1.2718E+05	RNG	1.5447E-01	A7	-3.6870E-01	EL	38623	77640.000
0010001	1964	8 15 21 35	1.0000	-1.3317E+05	RNG	5.8531E-01	AZ	-2.7821E-01	EL	38623	77700.000
0010001	1964	8 15 21 36	1.0000	-1.1933E+05	RNG	1.9884E+00	A7	-1.2593E-01	EL	38623	77760.000
0010001	1964	8 15 21 37	1.0000	-5.0370E+04	RNG	3.8556E+00	AZ	-9.2945E-01	EL	38623	77820.000
0010001	1964	8 15 21 38	1.0000	2.3855E+04	RNG	2.4054E+00	A7	-1.4173E+00	EL	38623	77880.000
0010001	1964	8 15 21 39	1.0000	7.4482E+04	RNG	1.8260E+00	AZ	-1.1119E+00	EL	38623	77940.000
0010001	1964	8 15 21 40	1.0000	9.8614E+04	RNG	1.2881E+00	AZ	-8.7896E-01	EL	38623	78000.000

TOTAL EDIT SUMMARY

STA	N TYP	PMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
001	8	RNG	1.0E+03	-4.3E+04	8	AZ	7.0E+00	1.5E+00	8	EL	8.0E-01	-6.8E-01
004	5	RNG	5.5E+04	5.3E+04	5	AZ	7.2E-01	5.4E-01	5	EL	1.3E+00	1.3E+00
005	6	RNG	1.7E+04	-3.0E+03	6	AZ	4.5E+00	4.5E+01	6	EL	1.8E+00	1.8E+01
006	15	RNG	6.8E+04	-4.0E+03	15	AZ	1.3E+00	1.3E+01	15	EL	9.4E-01	9.4E+00
009	33	RNG	2.6E+04	-1.2E+04	33	AZ	3.6E-01	3.6E+00	33	EL	1.4E+00	1.4E+01

ENTER SEGMENT 30 AT 106.3 SECONDS. EXECUTION TIME FOR SEGMENT 20 WAS 1.7 CP SECS., 10.0 PP SECS.

ITERATION NUMBER 2
 201 OBSERVATIONS WERE USED IN THIS SOLUTION
 CURRENT SOLUTION IS BEST SO FAR
 CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	BOUND	NEW VALUE	SIGMA
0001	3.51829203723992E+02	-2.26699431E-01	1.50000000E+00	3.51602509263401E+02	1.20826357E-04
0001	1.13160493953416E-01	-1.05599386E-01	1.50000000E+00	7.56111375938326E-03	2.02968458E-04
0001	8.9778164396747E+01	2.15475537E-01	1.50000000E+00	8.99836404363975E+01	8.98199728E-05
0001	1.54566401661983E+02	-9.16232540E-02	1.50000000E+00	3.54474777407950E+02	7.36258673E-05
0001	2.13476963170890E+07	5.46936314E+03	1.50000000E+05	2.13531662862318E+07	5.47662656E+01
0001	2.58554824597692E+04	-2.40599258E+00	1.50000000E+01	2.58530764631926E+04	6.77420654E-02
0001	1.22434282701928E-03	8.29721686E-03	1.50000000E-02	9.521555968620821E-03	6.02311948E-06

RMS FOR THIS SOLUTION = 3.0655522444E+02

PREDICTED RMS FOR NEXT SOLUTION = 9.7959735872E+00

XT((ATA)X) = 1.68699091E+07 XT(ATB) = 1.89699091E+07 RATIO = 1.00000000E+00

CORRELATION MATRIX DETERMINANT = 8.39750581E-07

	0001	0001	0001	0001	0001	0001	0001
	ALPHA	DELTA	BETA	AZ	R	V	DRAG
1.000000000							
.126707585							
-.095784306							
.469347141							
.105068389							
-.103952302							
.009335237							
	1.000000000						
	-.524526749	1.000000000					
	.172114292	-.201620817	1.000000000				
	.937164667	-.604628379	.113595954	1.000000000			
	-.931937276	.621176562	-.115757975	-.999467638	1.000000000		
	-.3295568072	.594698927	-.090391574	-.511015911	.536027303	1.000000000	

ENTER SEGMENT 40 AT 106.4 SECONDS. EXECUTION TIME FOR SEGMENT 30 WAS .2 CP SECS., 2.7 PP SECS.
 *** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 3. ***

YEAR/MO/DY	X	Y	Z	ALPHA	DELTA	BETA	AZIMUTH	RADIUS	VELOCITY	TAU	AF	AG	N	L	CHI	SI	MEAN ANOMOLY	ECCENTRIC ANOM	TRUE ANOMOLY	KEPLERIAN PER	ANOMALY PER	NODAL PERIOD	APOGEE RADIUS	APOGEE HEIGHT	PERIGEE RADIUS	PERIGEE HEIGHT	O-DOT	U-DOT
1964/ 8/16	21124233.035	351.602508852	21653940.572	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016	.0137249932016
12/ 7	-3118410.042	.007561114	.01369049192	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792	-.0021378323792
0.0000000	2817.893	99.993640436	35.92222544	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904	.0674629243904
.0076121	-364.0479416	354.474776997	351.603240608	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400	351.598074400
204.9368856	-2462.4712545	21353156.286	359.543396168	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689	-.16083438689
70.3456	25732.9607125	25853.0764632	726.8884727	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675	1.08959477675

END OF LEAST SQUARES PROCESS - MAXIMUM ITERATIONS (2) REACHED. (10)

REFERENCE
SECTION

DESCRIPTION

ITEM

2.2.2

19 Indication of the reason for ending the least-squares process. In this case, it was because the maximum number of iterations had been reached. Other reasons for ending the process could be convergence or the lack of additional computer running time

R -3.04E+05	1	0	0	0	3.04E+05
A -5.92E+00					5.92E+00
F -2.43E+00					2.43E+00
77590+					0010001
77595.					
77610.					
77625.					
77640.	R				0010001
77655.					
77670.					
77685.					
77700.	R				0010001
77715.					
77730.					
77745.					
77760.					
77775.	R				0010001
77790.					
77805.					
77820.					
77835.					
77850.					
77865.					
77880.					
77895.					
77910.					
77925.					
77940.					
77955.					
77970.					
77985.					
78000.					
78015.					
78030.					
78045.					
78060.					
78075.					
78090.					
78105.					
78120.					
78135+					

REFERENCE
SECTION

DESCRIPTION

ITEM

2.2.1
11.1.2
15

20 An example of the printer plot of the measurement residuals for the last iteration if GPLOT is input $\neq 0$. Its order is by station input, then by measurement encounter

Each page contains a maximum of six different measurements for a station. The first six, or fewer, lines contain the measurement type identifiers and the ranges of the residuals (the maximum negative value, a zero, and the maximum positive value) for the measurement types encountered first. The first line also has the VEHID printed between the maximum negative value and the zero. The identifiers and corresponding measurements are shown as follows (note that since only one character can be used as an identifier, some are repeated):

R	A	E	1	2	3	4	5	U	V	H	X	Y	Z	R	P	Q	D	7	8	9	1
Range	Azimuth	Elevation	Topocentric right ascension	Topocentric declination	Topocentric hour angle	Geocentric right ascension	Geocentric declination	u	v	Height	x	y	z	Range	P	Q	Range rate	P rate	Q rate	Accelerometer	One-way cumulative doppler
3	*	*	*	*	S	+	-	J	T	G	V	+	2	-	3)	(D	O		
Three-way cumulative doppler	Range rate	Doppler	Two-way doppler	SGLS range rate	X-antenna	Y-antenna	JPL two- or three-way doppler	Tranet doppler	Geociever range difference	Vehicle-vehicle range	Vehicle-vehicle range rate	Station-vehicle-vehicle range	Station-vehicle-vehicle range rate	Station-vehicle-vehicle range	Station-vehicle-vehicle range rate	Station-vehicle-vehicle range rate	Vehicle-vehicle range	Time difference of arrival	Time of arrival		

The left-hand column contains the system time in sec, incremented by GPLOT(2); the measurement identifiers are used to show the placement of the residual. In the far right-hand margin, the station-pass identification is shown.

ITEM	DESCRIPTION	REFERENCE SECTION
1	<p>Card images of the input MODEL data. The inputs used during a covariance analysis run are emphasized here. The input item MULTV indicates that simultaneous vehicles are used:</p> <p>MULTV ØPBOX, PRCØV, PANDR ITIN ØPRAM GPRAM KIG, SIGMA</p>	<p>2.1.6 2.5.1 2.1 2.1.5.3 2.1.5.2 2.5.3</p>

***** LUNAR GRAVITY MODEL *****

GM = 6.802326500E-05 ER**3/MIN**2 = 1.7314003854E+14 FT**3/SFC**2 = 4.9027777038E+12 M**3/SEC**2
 SPHERICAL MODEL

***** EARTH GRAVITY MODEL *****

GM = 5.5303936200E-03 ER**3/MIN**2 = 1.4076545201E+16 FT**3/SEC**2 = 3.9860319162E+14 M**3/SEC**2
 NO NORMALIZATION WITH 24 TERMS.

N	M	GM	SNM	**	N	M	GM	SNM
2	0	-1.04263710E-03	0.	**	5	2	1.21376037E-07	-2.75119005E-08
3	0	2.56637910E-06	0.	**	6	2	3.73837758E-09	-4.73526613E-08
4	0	1.62000910E-06	0.	**	3	3	7.66938326E-08	0.
5	0	1.32665010E-07	0.	**	4	3	5.31876720E-08	4.18329853E-09
6	0	-5.49000910E-07	0.	**	5	3	-2.01509731E-08	4.95514785E-09
3	1	2.09543373E-06	1.62018557E-07	**	6	3	2.48806140E-09	7.25686409E-09
4	1	-5.75696539E-07	-4.64855128E-07	**	4	4	-6.53285565E-09	2.37178570E-09
5	1	-4.24174235E-08	2.56904982E-08	**	5	4	0.	0.
6	1	-1.4144851E-07	9.42988666E-08	**	6	4	4.92117588E-10	-1.89273502E-09
2	2	1.56852217E-06	-8.97210795E-07	**	5	5	0.	0.
3	2	2.4592694E-07	-2.66420655E-07	**	6	5	-8.87768432E-11	-2.98614379E-10
4	2	7.37902536E-08	1.58760806E-07	**	6	6	0.	0.

***** PHYSICAL CONSTANTS *****

GM/ER**3/MIN**2)	=	5.531393520F-03	OMEGA(RAD/MIN)	=	4.375269500E-03	GMLAT(DEG)	=	7.830000000E+01
GM/KM**3/MIN**2)	=	0.	OMEGA(RAD/MIN)	=	4.375269500E-03	GMLNG(DEG)	=	2.910000000E+02
SGM/ER**3/MIN**2)	=	6.802326500F-05	OMEGL(RAD/MIN)	=	0.	AM(ER)	=	2.725062770E-01
ERFT(FT/ER)	=	2.092574100E+07	ERKM(<M/ER)	=	6.378164900E+03	ERNM(NM/ER)	=	3.443933600E+03
FTKM(FT/KM)	=	3.281839300E+03	FTNM(FT/NM)	=	6.076115500E+03	AE(ER)	=	1.000000000E+00
SSURD(FT/SEC**2)	=	3.217409000E+01	DGREE(DEG)	=	5.729577951E+01	SLT	=	2.820176300E+03
CKEP	=	1.001000000E-07	F	=	3.352329869E-03	PI	=	3.141592654E+00

***** INPUT/OUTPUT CONVERSION FACTORS *****

DF(I/O-ER) = 2.09257410E+07 VF(I/O-ER/MIN) = 3.48762308E+05 AF(I/O-ER/MIN**2) = 5.81278588E+03

***** INTEGRATION INPUTS *****

IFORM = 1 ICENT = 1 NSTEP = 2
 NPCMP = 0 IR = 8 ER = 1.00000000E-10
 HMIN = 1.56250000E-02 HMAX = 6.40000000E+01 MO = 1.00000000E+00

***** SPECIAL OPTIONS *****

TAPF2 = 0 TAPE7 = 0 TELEM = 0 PTAPE = 0 NPOUT = 0
 PRMO = 0 NODPR = 0 CLASS = 0 LEMSP = 0 PTNS = 10000

***** CRASH ALTITUDE *****

ECI CRASH ALTITUDE(FT) = 3.00000000E+05 MCI CRASH ALTITUDE(FT) = 3.00000000E+03

***** STATION LOCATIONS *****

STATION	SIG	REF	RA-REF	DATUM	TYPE	LATITUDE X	LONGITUDE Y	HEIGHT Z	P	Q
1	-0	-0	-0	0	0	4.30000000E+01	-9.30000000E+01	5.00000000E+02		
2	-0	-0	-0	0	0	4.30000000E+01	-9.30000000E+01	5.00000000E+02		
3	-0	-0	-0	0	0	4.30000000E+01	-9.30000000E+01	5.00000000E+02		

***** SENSOR PARAMETERS *****

STAPASS	PARAMETER	P-Q	INITIAL	VALUE	BOJND	SIGMA
1	LAT	Q	-0.	-0.	3.60000000E+02	1.37000000E-04
1	LONG	Q	-0.	-0.	3.60000000E+02	1.87000000E-04
1	ALT	Q	-0.	-0.	1.00000000E+10	5.00000000E+01
1	RBIA	Q	-0.	-0.	1.00000000E+10	1.00000000E+02
1	ABIA	Q	-0.	-0.	3.60000000E+02	2.00000000E-01
1	EBIA	Q	-0.	-0.	3.60000000E+02	2.00000000E-01
2	LAT	Q	-0.	-0.	3.60000000E+02	1.37000000E-04
2	LONG	Q	-0.	-0.	3.60000000E+02	1.87000000E-04
2	ALT	Q	-0.	-0.	1.00000000E+10	5.00000000E+01
2	RBIA	Q	-0.	-0.	1.00000000E+10	1.00000000E+02
3	LAT	Q	-0.	-0.	3.60000000E+02	1.37000000E-04
3	LONG	Q	-0.	-0.	3.60000000E+02	1.87000000E-04
3	ALT	Q	-0.	-0.	1.00000000E+10	5.00000000E+01
3	RBIA	Q	-0.	-0.	1.00000000E+10	1.00000000E+02

ITEM	DESCRIPTION	REFERENCE SECTION
2	<u>Sensor parameter information.</u> Each line contains the station and pass identification, parameter name, P- or Q-parameter indicator, initial value, bound, and sigma	5

ENTER SEGMENT 01 AT 110.7 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 110.7 CP SECS., 337.7 PP SECS.

***** VEHICLE DATA *****

YEAR	1969	IMNT4	0	IDAY	22	CARD
TZNE	0	HR	0	FIN	0	CARD 2
SEC	0	TICTYP3		IVCHID1		CARD 3
IC	1.3834434E8				10.	CARD 4
	-140.				-7.18E2	CARD 5
MVPRAM04,60						CARD 6
0	X					CARD 7
0	Y					CARD 8
0	Z					CARD 9
0	DX					CARD 10
0	DY					CARD 11
0	DZ					CARD 12
PT	0					CARD 13
	15					CARD 14
DRAG	0					CARD 15
FND						CARD 16

***** INITIAL CONDITIONS *****

EPOCH	YR/MO/DAY	TZNE,HR,MIN,SEC	X,Y,Z,X,Y,Z	A,D,B,A,R,V	A,E,I,O,U,TAU	AF,AG,N,L,CHI,PSI
1969/ 8/22			-1.14512224488E+08	2.19975207933E+02	1.36344340000E+08	6.14005836449E-02
0.			-9.60061635294E+07	-4.19511075994E-03	8.01529000000E-02	5.15212916005E-02
0.			-1.09412622380E+04	8.99978948803E+01	1.00000000000E+01	4.17761658205E-03
0.			5.88925582835E+03	8.00000000710E+01	-1.40000000000E+02	2.19971722355E+02
0.			-7.02517998470E+03	1.49433030692E+08	1.80800000000E+02	-5.62366289025E-02
0.			1.61641425299E+03	9.30855966659E+03	-7.18000000000E+02	-6.70202045299E-02

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

ITEM	DESCRIPTION	REFERENCE SECTION
3	Card images of the input <u>VEHICLE</u> data. The items used by a <u>simultaneous-vehicle or covariance analysis</u> run are emphasized	
	VEHID	11.1.2
	VPRAM	11.1.14
	PTIM	11.5.1

***** VEHICLE DATA *****

```

IVEHID3
IIC1YP3
IC 1.38334198E8
75
END

```

```

CARD 1
CARD 2
CARD 3
CARD 4
CARD 5

```

```

0
180
-7.71343693E2

```

```

EPOCH
YR/MO/DAY
YZNE,HP,MIN,SEC
1969/ 8/22
0.
0.
0.
0.
X,Y,Z,JX,JY,DZ
4.06703434460E+05
1.38245315589E+08
2.78671742142E+05
-1.00471057857E+04
2.78333870503E+02
8.55373878177E+02
A,D,B,A,R,V
8.83143155734E+01
1.15423120500E+00
9.00000000000E+01
8.51347337324E+01
1.38334198000E+08
1.00874919013E+04
INITIAL CONDITIONS
A,E,I,C,U,TAU
1.38334198000E+08
0.
5.00000000000E+00
7.50000000000E+01
1.80000000000E+02
-7.71343693000E+02
AF,AG,N,L,CHI,PSI
-8.27566114034E-15
-1.06388505267E-13
4.17807601469E-03
8.83639549683E+01
4.21732323555E-02
1.130028355519E-02

```

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

***** VEHICLE DATA *****

```

IVEHID3
IIC1YP3
IC 1.38334198E8
75.5
END

```

```

CARD 1
CARD 2
CARD 3
CARD 4
CARD 5

```

```

0
180
-7.18E2

```

```

EPOCH
YR/MO/DAY
YZNE,HP,MIN,SEC
1969/ 8/22
0.
0.
0.
0.
X,Y,Z,JX,JY,DZ
3.46553508933E+07
1.33922786431E+08
0.
-9.76580732694E+03
2.52715256980E+03
0.
A,D,B,A,R,V
7.54915147128E+01
0.
9.00000000000E+01
8.99999996107E+01
1.38334198000E+08
1.00874919013E+04
INITIAL CONDITIONS
A,E,I,C,U,TAU
1.38334198000E+08
0.
0.
7.55000000000E+01
1.80000000000E+02
-7.18000000000E+02
AF,AG,N,L,CHI,PSI
-2.24851579148E-14
-8.22551413022E-14
4.17807601469E-03
7.54915147128E+01
0.
-0.

```


ITEM	DESCRIPTION	REFERENCE SECTION
4	<p>Card images of the input <u>VEHICLE</u> data for the second vehicle and the printout of the initial conditions, perturbation remark, and atmospheric model (repeated for each vehicle used in the simultaneous-vehicle run). Note that inputs not overridden carry over from vehicle to vehicle. In this example, the VPRAM matrix carries over</p>	<p>Case A: Items 17, 18, 19, and 20</p>

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

THESE ARE THE 34 PARAMETERS IN THE PARAM MATRIX. 18 ARE P PARAMETERS AND 16 ARE Q PARAMETERS

	NAME	P/Q	CURRENT VALUE	BOUND	SIGMA	CONVERSION
0001	X	P	-1.14512224E+08	1.00000000E+10	1.00000000E+07	2.09257410E+07
0001	Y	P	-9.50031535E+07	1.00000000E+10	1.00000000E+07	2.09257410E+07
0001	Z	P	-1.09412622E+04	1.00000000E+10	1.00000000E+07	2.09257410E+07
0001	DX	P	5.38925583E+03	1.00000000E+10	1.00000000E+03	3.48762300E+05
0001	DY	P	-7.02517998E+03	1.00000000E+10	1.00000000E+03	3.48762300E+05
0001	DZ	P	1.51641425E+03	1.00000000E+10	1.00000000E+03	3.48762300E+05
0002	X	P	4.06701434E+06	1.00000000E+10	1.00000000E+07	2.09257410E+07
0002	Y	P	1.38245316E+08	1.00000000E+10	1.00000000E+07	2.09257410E+07
0002	Z	P	2.78671742E+06	1.00000000E+10	1.00000000E+07	2.09257410E+07
0002	DX	P	-1.00473058E+04	1.00000000E+10	1.00000000E+03	3.48762300E+05
0002	DY	P	2.78335871E+02	1.00000000E+10	1.00000000E+03	3.48762300E+05
0002	DZ	P	8.55375878E+02	1.00000000E+10	1.00000000E+03	3.48762300E+05
0003	X	P	3.46539509E+07	1.00000000E+10	1.00000000E+07	2.09257410E+07
0003	Y	P	1.33922796E+08	1.00000000E+10	1.00000000E+07	2.09257410E+07
0003	Z	P	0.	1.00000000E+10	1.00000000E+07	2.09257410E+07
0003	DX	P	-9.76580733E+03	1.00000000E+10	1.00000000E+03	3.48762300E+05
0003	DY	P	2.2715257E+03	1.00000000E+10	1.00000000E+03	3.48762300E+05
0003	DZ	P	0.	1.00000000E+10	1.00000000E+03	3.48762300E+05
3	RBIA	Q	-0.	1.00000000E+10	1.00000000E+02	2.09257410E+07
3	ALT	Q	5.30000000E+02	1.00000000E+10	5.00000000E+01	2.09257410E+07
3	LONG	Q	-9.30000000E+01	3.50000000E+02	1.87000000E-04	5.72957795E+01
3	LAT	Q	4.30000000E+01	3.50000000E+02	1.37000000E-04	5.72957795E+01
2	RBIA	Q	-0.	1.00000000E+10	1.00000000E+02	2.09257410E+07
2	ALT	Q	5.30000000E+02	1.00000000E+10	5.00000000E+01	2.09257410E+07
2	LONG	Q	-9.30000000E+01	3.50000000E+02	1.87000000E-04	5.72957795E+01
2	LAT	Q	4.30000000E+01	3.50000000E+02	1.37000000E-04	5.72957795E+01
1	EBIA	Q	-0.	3.50000000E+02	2.00000000E-01	5.72957795E+01
1	ABIA	Q	-0.	3.50000000E+02	2.00000000E-01	5.72957795E+01
1	RBIA	Q	-0.	1.00000000E+10	1.00000000E+02	2.09257410E+07
1	ALT	Q	5.30000000E+02	1.00000000E+10	5.00000000E+01	2.09257410E+07

1 LONG Q -9.30000000E+01 3.50000000E+02 1.07000000E-04 5.72957795E+01
 1 LAT Q 4.30000000E+01 3.60000000E+02 1.37000000E-04 5.72957795E+01
 GM Q 5.33039362E-03 0. 1.09667700E-08 1.00000000E+00
 02,00 C Q -1.38263700E-03 0. 2.23600000E-08 1.00000000E+00

ENTER SEGMENT 10 AT 111.6 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .8 CP SECS., 4.5 PP SECS.

TRAJECTORY INTEGRATION FOR CASE 1

IVEP	ICENT	1	IDRAG	0	ALPHG	5.761750222E+00	CDAM	0.
JVEP	JNORM	1	IR	9	ALG-DFG	3.301239703E+02	ER	1.000000000E-10
MVEP	MAJOR	1	ISRP	0	TJDATE	2.440455500E+06	HMIN	1.562500000E-02
KVEP	NMASS	0	NEQS	27	TSTART	0.	HMAX	5.400000000E+01
LVEP	VT	24	RECHP	0	TSTOP	3.000000000E+01	H0	1.000000000E+00
ICENTX	JNORMX	0	NVASSX	0	FLIGHT	3.000000000E+01	NTX	0.
			NASA	0	SSTEP	1.000000000E+02	SORD	1.500000000E+00

TIME(MME) TYPE ASSOCIATED QUANTITIES
 0.0000 TZERO
 30.0000 TSTOP

*** TRAJECTORY START

*** ENTRY TIME IS 111.70100

T	=	0.000000	4	=	.125000	NSTEP	=	0
-1.145122244079E+08					5.089255828347E+03	4.	830829047242E-01	
-9.600616352941E+07					-7.025179984701E+03	4.	050130141915E-01	
-1.094126223805E+04					1.616414252905E+03	4.	614415693159E-05	
02,00 C					0.	-2.	44496288923E-06	
					0.	-2.	34946786235F-06	
					0.	-7.	002904861358E-10	
GM					0.	1.	502752199719E-02	
					0.	1.	259895871980F-02	
					0.	1.	435431228069E-06	
X					1.0000100000000E+00	1.	156849534924E-05	

	0.	0.	2.243161066230E-05
	0.	0.	2.55524807094E-09
Y	0.	0.	2.243161066230E-05
	1.000030000000E+00	0.	3.619483449938E-06
	0.	0.	2.142254137494E-09
Z	0.	0.	2.55524807094E-09
	0.	0.	2.142254137494E-09
	1.000030000000E+00	0.	-1.518797879918E-05
DX	0.	1.000000000000E+00	0.
	0.	0.	0.
	0.	0.	0.
DY	0.	0.	0.
	0.	1.000000000000E+00	0.
	0.	0.	0.
DZ	0.	0.	0.
	0.	0.	0.
	0.	1.000000000000E+00	0.

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	6.304004E-01	4.830829E-01	4.050130E-01	4.614416E-05	-6.304004E-01	-3.420336E-08	-6.976752E-09	
TOTAL	6.304004E-01	4.830829E-01	4.050130E-01	4.614416E-05	-6.304004E-01	-3.420336E-08	-6.976752E-09	

MODE	Y =	1.12814106350E-01	-1.14472343940E+08	-9.605370662137E+07	-1.227973594797E-10
OY =	1.2500000000700E-01	5.892525173075E+03	-7.022437834961E+03	1.616414409103E+03	
*	STEP DOUBLED	T =	3.250000	M =	.250000 NSTEP = 25
*	STEP DOUBLED	T =	7.500000	M =	.500000 NSTEP = 41
*	STEP DOUBLED	T =	15.000000	M =	1.000000 NSTEP = 57

Y =	30.300000	T =	1.000000	NSTEP =	71
-1.031517926203E+08	6.717059485659E+03	4.350762082148E-01			
-1.079671375801E+08	-6.249427521532E+03	4.562150451684E-01			
2.892032284940E+06	1.605453243475E+03	-1.222115672862E-02			

02, JO C	-1.067305128407E-03	-7.009771297779F-05	-2.232865286960E-06
	-9.64115372844E-04	-6.572210958654F-05	-2.339382147550E-06
	2.767112854346E-05	2.780059370108E-06	1.864451829015E-07
GM	6.562092628373E+00	4.310746463120F-01	1.373717558371E-02
	5.927637541327E+00	4.0413466684247E-01	1.439248707537E-02
	-5.693159818645E-02	-5.734773176488E-03	-3.870978531235E-04
X	1.004477955644E+00	2.747888019029E-04	6.820129799268E-06
	1.019931600779E-02	6.827010123838F-04	2.297611316839E-05
	-9.630510433524E-05	-9.522323254205F-06	-6.182057231257E-07
Y	1.019512349771E-02	6.821857296951E-04	2.290744045517E-05
	1.00233935225E+00	1.860943686471E-04	8.890457780075E-06
	-9.024715473606E-05	-9.252425235328E-06	-6.452862051509E-07
Z	-9.588913321212E-05	-9.452713086250E-06	-6.089286477563E-07
	-8.989650147419E-05	-9.194015111649F-06	-6.375017710560E-07
	9.931728272075E-01	-4.546772525530E-04	-1.509178751809E-05
DX	3.004034250283E+01	1.003725452967E+00	1.993488181183E-04
	1.022439151825E-01	1.025315636076E-02	6.853948449331E-04
	-1.432034419944E-03	-1.86376774393E-04	-1.838115336730E-05
DY	1.02273425880E-01	1.025006160901E-02	6.848790387747E-04
	3.002754670061E+01	1.003149681995F+00	2.616909180022E-04
	-1.372021153866E-03	-1.865284733097E-04	-1.922631782016E-05
DZ	-1.429954095661E-03	-1.879587038032E-04	-1.831147254788E-05
	-1.370257148254E-03	-1.861776660532E-04	-1.916784830180E-05
	2.993159056583E+01	9.931714844961E-01	-4.548297409590E-04

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
SEOPOTENTIAL	6.310860E-01	4.358762E-01	4.562150E-01	1.222116E-02	-6.310860E-01	-1.739166E-07	-7.744879E-07	
TOTAL	6.310860E-01	4.358762E-01	4.562150E-01	1.222116E-02	-6.310860E-01	-1.739166E-07	-7.744879E-07	

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 1.129 SECONDS TO INTEGRATE A SPAN OF 30.000 MINUTES ***

*** FROM 0.000 TO 30.000 MINUTES FROM MIDNIGHT OF EPOCH ***

TRAJECTORY INTEGRATION FOR CASE 2

IVER	ICENT	1	IRAG	0	ALPMG	5.761750222E+00	COAM	0.
JVEP	JNORM	1	IR	9	ALG-DES	3.301239703E+02	ER	1.000000000E-10
MVEP	MAJOP	1	ISRP	0	TJDATE	2.440455500E+06	HMIN	1.562500000E-02
KVEP	VMASS	0	NFQS	27	TSTART	0.	HMAX	6.400000000E+01
LVEP	VT	24	RFCMP	2	TSTOP	3.000000000E+01	M0	1.000000000E+00
IDENTY	JNORMX	0	NMASSX	3	FLIGHT	3.000000000E+01	NTX	0.
			NASA	4	SSTEP	1.000000000E+02	SORD	1.500000000E+00

* PREDETERMINED EVENT TABLE *

ASSOCIATED QUANTITIES

TIME(MME) TYPE
0.0000 T7F50
30.0000 TSTOP

*** TRAJECTORY START

SEG1 ENTRY TIME IS 112.85300

T	=	0.000000	4	=	.125000	NSTEP	=	0
02,00 C		4.067034344501E+06	-1.004730578571E+04		-2.162744150928E-02			
		1.382453155891E+08	2.783368705028E+02		-7.351517941123E-01			
		2.786717421420E+06	8.553758781768E+02		-1.482002055073E-02			
		0.	0.		1.274437767438E-07			
		0.	0.		4.332058961582E-06			
		0.	0.		2.623271566750E-07			
GM		0.	0.		-6.727765114606E-04			
		0.	0.		-2.286876416886E-02			
		0.	0.		-4.610143886837E-04			
X		1.000010000000E+00	0.		-1.909406277137E-05			
		0.	0.		1.687467803763E-06			
		0.	0.		3.401905643118E-08			

	-1.031835027654E+01	-6.892533705414E-01	-2.314441681329E-02
	-2.461874755292E-01	-1.772837401649E-02	-7.246866026364E-04
X	9.914272990064E-01	-5.680081449113E-04	-1.839421018251E-05
	-3.635617942318E-04	-6.145012900747E-05	-5.744386322036E-06
	-1.073532393402E-05	-1.785119061049E-06	-1.795199097829E-07
Y	-3.6937311264649E-04	-6.241723129230E-05	-5.873111043707E-06
	1.017214659442E+00	1.149388370508E-03	3.829710369053E-05
	6.163371735316E-04	4.427394692864E-05	1.793490631172E-06
Z	-1.086745890223E-05	-1.807419928568E-06	-1.824349837512E-07
	6.158432534138E-04	4.41221749907E-05	1.782610832439E-06
	9.914119190898E-01	-5.715525417284E-04	-1.892465283486E-05
DX	2.991448216747E+01	9.915082636154E-01	-5.550210678596E-04
	-9.267732775470E-03	-1.485972548969E-03	-1.732620244910E-04
	-2.567657963390E-04	-4.299783690502E-05	-5.414942578455E-06
DY	-9.29683232778E-03	-1.491780883369E-03	-1.742291272889E-04
	3.017196880907E+01	1.017148866298E+00	1.135887758193E-03
	6.627238215817E-03	7.092581074666E-04	5.341831321044E-05
DZ	-2.574248749686E-04	-4.312937141402E-05	-5.436843357366E-06
	6.624732105526E-03	7.087671875916E-04	5.333657382664E-05
	2.991499297218E+01	9.914167476987E-01	-5.710390014654E-04

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	7.356196E-01	7.445408E-02	-7.314850E-01	-2.285719E-02	-7.356196E-01	5.249624E-08	-1.712987E-06	
TOTAL	7.356196E-01	7.445408E-02	-7.314850E-01	-2.285719E-02	-7.356196E-01	5.249624E-08	-1.712987E-06	

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 1.132 SECONDS TO INTEGRATE A SPAN OF 30.000 MINUTES ***

*** FROM 0.000 TO 30.000 MINUTES FROM MIDNIGHT OF EPOCH ***

TRAJECTORY INTEGRATION FOR CASE 3

TIME(H:MM)	TYPE	ASSOCIATED QJANTITIES	* PREDETERMINED EVENT TABLE *
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*** TRAJECTORY START

SFG1: ENTRY TIME IS 114.00500 ECI

	Y	=	0.000000	X	=	.125000	NSTEP	=	0
02,00 C	3.465535082333E+07			-9.765807326943E+03			-1.842899424245E-01		
	1.339227954313E+08			2.527152569800E+03			-7.121605279939E-01		
	0.			0.			-1.006964949376E-08		
	0.			0.			1.088179954344E-06		
	0.			0.			4.205110486071E-06		
	0.			0.			0.		
GM	0.			0.			-5.732806837653E-03		
	0.			0.			-2.215356242819E-02		
	0.			0.			-3.132420288982E-10		
X	1.000010001000E+00			0.			-1.553511309570E-05		
	0.			0.			1.392937542766E-05		
	0.			0.			-4.344817468047E-13		
Y	0.			0.			1.392937542766E-05		
	1.000010001000E+00			0.			3.468423879095E-05		
	0.			0.			1.386397852185E-12		
Z	0.			0.			-4.344817468047E-13		

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	FORCFS	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	7.356191E-01	-1.842899E-01	-7.121605E-01	-1.006965E-08	-7.356191E-01	1.746302E-07	-1.006965E-08		
TOTAL	7.356191E-01	-1.842899E-01	-7.121605E-01	-1.006965E-08	-7.356191E-01	1.746302E-07	-1.006965E-08		
DX	0.	1.000000000000E+00	0.	0.	0.	1.386397862185E-12	-1.914512569526E-05		
DY	0.	0.	0.	0.	0.	0.	0.		
DZ	0.	0.	0.	0.	0.	0.	0.		
GM	0.	0.	0.	0.	0.	0.	0.		
X	0.	0.	0.	0.	0.	0.	0.		
Y	0.	0.	0.	0.	0.	0.	0.		
Z	0.	0.	0.	0.	0.	0.	0.		
STEP	DOUBLED	T =	3.250000	H =	.250000	NSTEP =	71		
STEP	DOUBLED	T =	7.500000	H =	.500000	NSTEP =	41		
STEP	DOUBLED	T =	15.000000	H =	1.000000	NSTEP =	57		
02.00 C	1.682930795167E+07	1.001256909845E+04	-1.001256909845E+04	-8.949604214476E-02					
	1.373055756953E+08	1.227201690960E+03	1.227201690960E+03	-7.301551530551E-01					
	-1.628942793407E-02	-1.807336948206E-05	-1.807336948206E-05	-9.983033663556E-09					
	4.070847007474E-04	2.437527762037E-05	2.437527762037E-05	5.342934860491E-07					
	1.916519326183E-03	1.286730581928E-04	1.286730581928E-04	4.385942515055E-06					
	5.917821148882E-14	7.662493042071E-15	7.662493042071E-15	7.272527446215E-16					
	-2.144625249825E+00	-1.284151381294E-01	-1.284151381294E-01	-2.814794016789E-03					
	-1.009679711925E+01	-6.778813727344E-01	-6.778813727344E-01	-2.310621656102E-02					
	-1.414727134905E-07	-9.464543733016E-09	-9.464543733016E-09	-3.197602452963E-10					
	9.925332139491E-01	-5.102966186224E-04	-5.102966186224E-04	-1.812069354333E-05					
	5.257032259425E-03	3.161725696603E-04	3.161725696603E-04	7.080467209392E-06					

Y	-2.214233915733E-10	-1.557665160814E-11	-5.973181391956E-13
Z	5.251231741357E-03	3.152017735133F-04	6.951250815456E-06
	1.016137602155E+00	1.092830260297E-03	3.607937322965E-05
	6.144239209723E-10	4.061547379242E-11	1.317067303713E-12
	-2.215154120324E-10	-1.559210221234E-11	-5.994337175659E-13
	6.146077081433E-10	4.064573851100E-11	1.321091289946E-12
	9.913970555523E-01	-5.727059617717E-04	-1.898043935721E-05
OX	2.992313041991E+01	9.921252091104E-01	-5.470746835051E-04
	4.732637541441E-02	4.205822502933E-03	2.093005529613E-04
	-2.353551543415E-09	-2.482414436165E-10	-1.823644774703E-11
OY	4.729770487385E-02	4.199991983422F-03	2.083297562321E-04
	3.016339232585E+01	1.016551615658E+00	1.129608695166E-03
	6.088616203347E-09	6.031274802870F-10	3.939547750913E-11
OZ	-2.354115772231E-09	-2.483360037071E-10	-1.825260519330E-11
	6.089525257188E-09	6.033090279937E-10	3.942566661087E-11
	2.991332110270E+01	9.913970528152E-01	-5.727063261363E-04

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	7.356195E-01	-8.949604E-02	-7.301552E-01	-9.983034E-09	-7.356195E-01	1.7463305E-07	1.006966E-08	
TOTAL	7.356195E-01	-8.949604E-02	-7.301552E-01	-9.983034E-09	-7.356195E-01	1.7463305E-07	1.006966E-08	

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 1.137 SECONDS TO INTEGRATE A SPAN OF 30.000 MINUTES ***

*** FROM 0.000 TO 30.000 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 21 AT 115.1 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 3.5 CP SECS., 17.8 PP SECS.

RUNNING TIME FOR SEG21 WILL INCLUDE THAT FOR SEG22, SEG23, AND SEG24.

1 1969 8 22 0 15 0.0000

PARTIALS FOR RING	-7.521539222E-01	-6.574089152E-01	-9.396491570E-02	-1.125646282E+01	-9.839002780E+00
	-1.411202182E+00	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	0.	0.	0.	0.	0.
	2.461772464F-01	7.055398750E-01	-2.196830241E+00	1.000000000E+00	-6.211610330E-01
				3.571280823E-04	

ITEM	DESCRIPTION	REFERENCE SECTION
5	Partial derivatives of the measurement (in this case, range) with respect to all parameters at the <u>observation time</u> shown on the first line. The partials are printed across the page in the order shown in the parameter list. The units are internal units	Case B: Items 4 and 6

PARTIALS FOR AZ		-1.273024078E-01	1.367271389E-01	6.170396870E-02	-1.911401324E+00	2.053488895E+00
		9.256145215E-01	0.	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	0.	1.000000000E+00	0.	0.
		1.336097330E+00	-7.641923509E-01	-1.422546047E-02	2.454676206E-06	
		2.153833637E-02	-4.558491113E-02	1.458813612E-01	3.239806600E-01	-6.855916569E-01
		2.197711353E+00	0.	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	1.000000000E+00	0.	0.	-1.210363503E-01
		-3.437679833E-01	-9.905326916E-01	-3.125024284E-02	5.415401331E-06	
1	1969 8 22 0 15 0.0000					
PARTIALS FOR RD		1.970208850E-03	-3.045492045E-03	7.317243200E-04	-7.174194756E-01	-6.986737655E-01
		-8.33885099E-02	0.	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	0.	0.	0.	0.
		5.439230197E-04	-6.497490595E-04	-2.931598728E-01	4.764305084E-05	-3.402956952E-04
2	1969 8 22 0 15 0.0000					
PARTIALS FOR S2		-4.000359060E-01	-9.191539810E-01	-6.015897430E-03	-5.972374313E+00	-1.377284910E+01
		-1.204351861E-01	4.127522528E-01	1.923551610E+00	-6.161133578E-02	6.198561629E+00
		2.876734710E+01	-9.281750174E-01	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	0.	1.000000000E+00	6.908732761E-01	3.450543492E-01
		-5.473467325E-01	0.	0.	0.	0.
		0.	0.	-6.927454010E+00	1.257255710E-03	
3	1969 8 22 0 15 0.0000					
PARTIALS FOR S3		-4.000359060E-01	-5.131539810E-01	-8.015897430E-03	-5.972374313E+00	-1.377284910E+01
		-1.204351861E-01	-5.921544118E-01	9.957147359E-01	1.221985379E-01	-8.895918843E+00
		1.493335783E+01	1.834238643E+00	1.206307960E+00	9.074322187E-01	-2.062590273E-01
		1.810305479E+01	1.349817808E+01	-3.098335541E+00	1.000000000E+00	7.610603632E-01
		2.078613361E-01	-5.821478754E-01	0.	0.	0.
		0.	0.	0.	0.	0.
		0.	0.	-7.504468632E+00	1.371840296E-03	

1	1969	8 22	0 30	0.0000	-7.043704192E-01	-6.284206452E-02	-2.151174800E+01	-2.095512844E+01
PARTIALS FOR RMC					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
PARTIALS FOR AZ					6.967349549E-01	-8.801036486E+00	1.000088000E+00	-6.261657134E-01
					1.293945144E-01	6.413813284E-02	1.429921570E-03	3.903575530E+00
					0.	0.	-4.032607118E+00	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
PARTIALS FOR EL					-8.033169574E-01	1.000300000E+00	0.	0.
					-4.455868047E-02	-1.41122388E-01	1.974999381E-05	-1.339988130E+00
					0.	1.4463315547E-01	7.918326578E-01	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					1.000000000E+00	0.	0.	-1.205585864E-01
					-9.825893909E-01	-9.930010515E-02	1.883168186E-05	0.
1	1969	8 22	0 30	0.0000	-3.215008508E-03	7.509020686E-04	-6.495953331E-01	-7.832947976E-01
PARTIALS FOR RD					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					0.	0.	0.	0.
					-6.572105216E-04	-5.875671028E-01	9.541199671E-05	-3.269296243E-04
2	1969	8 22	0 30	0.0000	-9.456698769E-01	-5.228423657E-03	-1.034918947E+01	-2.825902750E+01
PARTIALS FOR S2					2.891369076E-01	1.969842606E+00	-5.800483389E-02	8.727462689E+00
					-1.775742642E+00	0.	0.	0.
					0.	0.	0.	0.
					0.	1.000000000E+00	6.878153668E-01	3.450487537E-01
					0.	0.	0.	0.
					-5.511776058E-01	-2.773499914E+01	5.035852028E-03	0.
3	1969	8 22	0 30	0.0000	-9.456698769E-01	-5.228423657E-03	-1.034918947E+01	-2.825902750E+01
PARTIALS FOR S3					-6.438696961E-01	9.646372947E-01	1.428068129E-01	-1.942595224E+01
					4.297560896E+00	1.139284829E+00	9.977219123E-01	-2.285898509E-01
					2.949266130E+01	-6.894942466E+00	1.000000000E+00	7.610603879E-01

2.076613613E-01 -5.821478526E-01 0. 0. 0.
 0. 0. 0. 0. 0.
 0. 0. -3.002659224E+01 5.495521975E-03 0.

TOTAL EDIT SUMMARY

STA	N	TYP	RMS	RMS/SIG	MEAN
1	2	RNG	1.4E+08	1.4E+07	-1.4E+08
2	2	RD	1.8E+02	8.8E+02	1.7E+02
3	2	S2	4.1E+08	4.1E+07	-4.1E+08
3	2	S3	4.5E+08	4.5E+07	-4.5E+08

N	TYP	RMS	RMS/SIG	MEAN	N	TYP	RMS	RMS/SIG	MEAN
2	AZ	1.5E+02	1.4E+04	1.6E+02	2	EL	3.8E+01	3.3E+03	-3.8E+01

ENTER SEGMENT 72 AT 115.9 SECONDS.

EXECUTION TIME FOR SEGMENT 21 WAS

.7 CP SECS.,

12.7 PP SECS

ITEM	DESCRIPTION	REFERENCE SECTION
6	Edit summary. The restriction to the first 6 measurement types encountered for the first 30 stations still holds	Case B: Item 7

 * SIMULTANEOUS VEHICLE COVARIANCE ANALYSIS INPUT AND OUTPUT OPTIONS *

 * OPROX OPTIONS *

* A SORT OF DIAGONAL OF FULL ATA INVERSE INPUT *
 * C PRINT DP/OQ *
 * D NORMAL COVAR. ANALYSIS, OBSERVATIONS INPUT *
 * E NORMAL UPDATE - OUTPUT IS REAL TIME *
 * F GENERAT: PLOT TAPE *
 * H PRINT ENTIRE INTER-SATELLITE COV. MATRIX *

 * PROCV OPTIONS *

* A C(P), CORRELATION AND SORT OF DIAGONAL *
 * R PRINT C(X) AT CURRENT TIME WITH P EFFECTS *
 * C PRINT C(OP) AT CURRENT TIME FOR P EFFECTS *
 * G PRINT CORRELATION AND SORT OF DIAGONAL *
 * H PRINT C(X) AT CURRENT TIME WITH P+Q EFFECTS *
 * I PRINT C(OP) AT CURRENT TIME FOR P+Q EFFECTS *

7

ITEM	DESCRIPTION	REFERENCE SECTION
7	<u>Indicates input/output options requested by ØPBØX and PRCØV for the simultaneous-vehicle error analysis run</u>	2.5.1

COVARIANCE MATRICES AT 0.

MINUTES FROM MIDNIGHT OF EPOCH DATE 8

DATA(INVERSE) FOR P PARAMETERS

[illegible]

ITEM	DESCRIPTION	REFERENCE SECTION
8	<u>Time statement</u> , determined by PTIM, that applies to items 9 through 14. <u>Valid until another time statement is made</u>	
9	<u>$(A^T A)^{-1}$ for P-parameters, identified by parameter name (PRCQV (A) = C).</u> <u>This is the covariance matrix of P-parameters, based on measurement uncertainties (observation weights) only</u>	

	(9)	(10)	(11)	(12)
0001 X	1.000			
0001 Y	0.000			
0001 Z	0.000			
0001 OX	0.000			
0001 DY	0.000			
0001 DZ	0.000			
0002 X	0.000			
0002 Y	0.000			
0002 Z	0.000			
0002 OX	0.000			
0002 DY	0.000			
0002 DZ	0.000			
0003 X	0.000			
0003 Y	0.000			
0003 Z	0.000			
0003 OX	0.000			
0003 DY	0.000			
0003 DZ	0.000			
SQRT DIAG	1.000000E+07	1.000000E+07	1.000000E+07	1.000000E+07
PIVOT RATIOS	1.000000E+00	1.000000E+00	1.000000E+00	1.000000E+00

ITEM	DESCRIPTION	REFERENCE SECTION
10	Correlation matrix for P-parameters, i.e., the matrix of Item 9 normalized to 1s on the diagonal ($\text{PRC}\hat{Q}V(A) = C$)	2.5.1
11	Square roots of the diagonal elements of $(A^T A)^{-1}$ (Item 9) in the order shown in the header of Item 9	2.5.1
12	Pivot ratios encountered in the inversion of $A^T A$ are determined by referencing the original diagonal elements of the $A^T A$ matrix to the diagonal element used in pivoting that particular row and column. These will be printed if Items 9, 10, or 11 are printed	

[illegible]

ATA(INVERSE) FOR P AND Q PARAMETERS (14)

0001 X	0001 Y	0001 Z	0001 DX	0001 DY	0001 DZ	0002 X	0002 Y
0002 Z	0002 DX	0002 DY	0002 DZ	0003 X	0003 Y	0003 Z	0003 DX
0003 DY	0003 DZ						

ITEM	DESCRIPTION	REFERENCE SECTION
13	The $\partial P / \partial Q$ matrix printed when $\Phi P B \Phi X(C) = 1$; P and Z represent P- and Q-parameter lists, respectively	2.5.1
14	<u>Indicates that the next covariance matrix printed will include the effects of the Q-parameters.</u> Since $PRC \Phi V(G) = B$, the $(A^T A)^{-1}$ matrix is not printed, but the correlation matrix (Item 10) is	2.5.1

[illegible]

STATE COVARIANCE AND CORRELATION MATRIX PARTITIONS AT 0.

MMOED 18

ITEM	DESCRIPTION	REFERENCE SECTION
15	<u>Square roots of the diagonal elements of the $(A^T A)^{-1}$ matrix, with the Q-parameter effects included</u>	
16	<u>Indicates time of the state covariance matrix partitions, as indicated by $PRC\phi V(B)$ through (F) and $PRC\phi V(H)$ through (L)</u>	2.5.1

ITEM	DESCRIPTION	REFERENCE SECTION
17	<u>Cartesian covariance matrix for Satellite i with respect to itself in an upper triangular format. The lower triangular matrix printed is the normalized correlation matrix. The top item of each column is the square root of the diagonal element (of that column) in the unnormalized matrix. It is identified as a P-parameter matrix, indicating that only the effects of measurement uncertainties are included</u>	2.5.1 [$\text{QPB}\Phi\text{X}(\text{H})$, $\text{PRC}\Phi\text{V}(\text{B})$]
18	<u>Orbit plane matrices (Item 17)</u>	2.5.1 [$\text{QPB}\Phi\text{X}(\text{H})$, $\text{PRC}\Phi\text{V}(\text{C})$]
19	<u>Cartesian matrices (Item 17), but including both P- and Q-parameter effects</u>	2.5.1 [$\text{QPB}\Phi\text{X}(\text{H})$, $\text{PRC}\Phi\text{V}(\text{H})$]
20	<u>Orbit plane matrices (Item 17), but including both P- and Q-parameter effects</u>	2.5.1 [$\text{QPB}\Phi\text{X}(\text{H})$, $\text{PRC}\Phi\text{V}(\text{I})$]

0.000000	1.0000000E+07	1.0000000E+06	0.	0.
0.000000	0.000000	1.0000000E+06	1.0000000E+06	0.
0.000000	0.000000	1.0000000E+03	1.0000000E+03	1.0000000E+06
0.000000	0.000000	0.000000	0.000000	1.0000000E+03
0.000000	0.000000	0.000000	0.000000	1.0000000E+03

ORBIT PLANE FOR				
	P	PARAMETERS	VEHICLES	2 AND 2
1.0000000E+14	1.6601563E-02	0.	0.	0.
1.0000000E+07	1.0000000E+14	-3.1250000E-02	0.	0.
0.000000	1.0000000E+07	1.0000000E+14	0.	0.
0.000000	0.000000	1.0000000E+07	1.0000000E+06	0.
0.000000	0.000000	0.000000	1.0000000E+06	-1.1641532E-10
0.000000	0.000000	0.000000	1.0000000E+03	-4.6566129E-10
0.000000	0.000000	0.000000	0.000000	1.0000000E+06
0.000000	0.000000	0.000000	1.0000000E+03	1.0000000E+03
0.000000	0.000000	0.000000	0.000000	1.0000000E+03

CAPTESIAN FOR				
	P AND 3	PARAMETERS	VEHICLES	2 AND 2
1.0000000E+14	0.	0.	0.	0.
1.0000000E+07	1.0000000E+14	0.	0.	0.
0.000000	1.0000000E+07	1.0000000E+14	0.	0.
0.000000	0.000000	1.0000000E+07	1.0000000E+06	0.
0.000000	0.000000	0.000000	1.0000000E+06	1.0000000E+06
0.000000	0.000000	0.000000	1.0000000E+03	1.0000000E+03
0.000000	0.000000	0.000000	0.000000	0.000000
0.000000	0.000000	0.000000	0.000000	1.0000000E+03

ORBIT PLANE FOR				
	P AND 3	PARAMETERS	VEHICLES	2 AND 2
1.0000000E+14	1.6601563E-02	0.	0.	0.
1.0000000E+07	1.0000000E+14	-3.1250000E-02	0.	0.
0.000000	1.0000000E+07	1.0000000E+14	0.	0.
0.000000	0.000000	1.0000000E+07	1.0000000E+06	0.
0.000000	0.000000	0.000000	1.0000000E+06	-1.1641532E-10
0.000000	0.000000	0.000000	1.0000000E+03	-4.6566129E-10
0.000000	0.000000	0.000000	0.000000	1.0000000E+06
0.000000	0.000000	0.000000	1.0000000E+03	1.0000000E+03
0.000000	0.000000	0.000000	0.000000	1.0000000E+03

CAPTESIAN FOR				
	P	PARAMETERS	VEHICLES	3 AND 3
1.0000000E+14	0.	0.	0.	0.
1.0000000E+07	1.0000000E+14	0.	0.	0.

1.000000E+07	1.000000E+07	1.000000E+14	0.	0.	0.
0.000000	0.000000	0.000000	1.000000E+06	0.	0.
0.000000	0.000000	0.000000	1.000000E+06	0.	0.
0.000000	0.000000	0.000000	1.000000E+03	1.000000E+06	1.000000E+06
0.000000	0.000000	0.000000	0.000000	1.000000E+03	1.000000E+03
0.000000	0.000000	0.000000	0.000000	0.000000	1.000000E+03

OPRIT PLNE FOR	P	PARAMETERS	VFHICLES	3	AND	3
1.000000E+14	0.	0.	0.	0.	0.	0.
1.000000E+07	1.000000E+14	0.	0.	0.	0.	0.
0.000000	1.000000E+07	1.000000E+14	1.000000E+06	0.	0.	0.
0.000000	0.000000	0.000000	1.000000E+06	1.000000E+06	0.	0.
0.000000	0.000000	0.000000	1.000000E+03	1.000000E+06	1.000000E+06	1.000000E+06
0.000000	0.000000	0.000000	0.000000	0.000000	1.000000E+03	1.000000E+03
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	1.000000E+03

CAPTESIAN FOR	P	AND	3	PARAMETERS	VEHICLES	3	AND	3
1.000000E+14	0.	0.	0.	0.	0.	0.	0.	0.
1.000000E+07	1.000000E+14	0.	0.	0.	0.	0.	0.	0.
0.000000	1.000000E+07	1.000000E+14	1.000000E+06	0.	0.	0.	0.	0.
0.000000	0.000000	0.000000	1.000000E+06	1.000000E+06	0.	0.	0.	0.
0.000000	0.000000	0.000000	1.000000E+03	1.000000E+06	1.000000E+06	1.000000E+06	1.000000E+06	1.000000E+06
0.000000	0.000000	0.000000	0.000000	0.000000	1.000000E+03	1.000000E+03	1.000000E+03	1.000000E+03
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	1.000000E+03	1.000000E+03

OPRIT PLNE FOR	P	AND	3	PARAMETERS	VEHICLES	3	AND	3
1.000000E+14	0.	0.	0.	0.	0.	0.	0.	0.
1.000000E+07	1.000000E+14	0.	0.	0.	0.	0.	0.	0.
0.000000	1.000000E+07	1.000000E+14	1.000000E+06	0.	0.	0.	0.	0.
0.000000	0.000000	0.000000	1.000000E+06	1.000000E+06	0.	0.	0.	0.
0.000000	0.000000	0.000000	1.000000E+03	1.000000E+06	1.000000E+06	1.000000E+06	1.000000E+06	1.000000E+06
0.000000	0.000000	0.000000	0.000000	0.000000	1.000000E+03	1.000000E+03	1.000000E+03	1.000000E+03
0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	1.000000E+03	1.000000E+03

REFERENCE SECTION

DESCRIPTION

ITEM

- 21 The matrices described in Items 17 through 20 for Satellites i and j.
 Since they are asymmetrical, they are printed entirely and as S_{ij} .
 The matrices of Items 17 through 20 are variance-covariance
 matrices of particular satellite state vectors in the indicated coordinate systems; the matrices here are intersatellite covariance matrices

0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000

3D FIT PLANE FOR P PARAMETERS VEHICLES 3 AND 1

COVARIANCE

0.
 0.
 0.
 0.
 0.
 0.

CORRELATION

0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000

CARTESIAN FOR P AND Q PARAMETERS VEHICLES 3 AND 1

COVARIANCE

0.
 0.
 0.
 0.
 0.
 0.

CORRELATION

0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000

ORBIT PLANE FOR P AND Q PARAMETERS VEHICLES 3 AND 1

COVARIANCE

0.	0.	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.

CORRELATION

0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000

CAPTESTAN FOR P PARAMETERS VEHICLES 3 AND 2

COVARIANCE

0.	0.	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.
0.	0.	0.	0.	0.

CORRELATION

0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000
0.0000000	0.0000000	0.0000000	0.0000000	0.0000000

ORBIT PLANE FOR P PARAMETERS VEHICLES 3 AND 2

COVARIANCE

0.0000000
0.0000000
0.0000000
0.0000000
0.0000000


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0. 0. 0. 0. 0. 0. 0. 0.
CORRELATION
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000 0.000000
COVARIANCE MATRICES AT 1.500000000E+01 MINUTES FROM MIDNIGHT OF EPOCH DATE

ATA(INVERSE) FOR P PARAMETERS
0001 X 0001 Y 0001 Z 0001 DX 0001 DY 0001 DZ 0002 X 0002 Y 0002 Z
0002 Z 0002 DX 0002 DY 0002 DZ 0003 X 0003 Y 0003 Z
0003 DY 0003 DZ
3.531205E+11 4.60113E+11
-3.95845E+11 4.98050E+10 7.98815E+11
-5.69830E+10 -4.98050E+10 7.98815E+11
-3.91601E+08 4.38308E+08 6.34054E+07 4.34672E+05
4.38931E+08 -5.10171E+08 5.58214E+07 -4.97127E+05 5.66192E+05
6.31783E+07 5.52199E+07 -8.85759E+08 -7.03628E+04 -6.15027E+04 9.83064E+05
5.33716E+08 -6.29350E+04 1.25965E+08 -5.82422E+05 6.87427E+05 -1.36915E+05 7.60206E+13
-2.40359E+08 2.96756E+08 -5.27310E+07 1.47751E+05 -1.88544E+05 2.55990E+04 -1.59975E+13 4.30231E+12
-1.30249E+07 1.63585E+07 -7.93590E+06 1.18180E+04 -1.50363E+04 8.05975E+03 4.45137E+12 2.19633E+12
9.91881E+13
-1.13203E+04 1.32132E+04 -2.35961E+03 1.26326E+01 -1.48246E+01 2.63983E+00 -2.19683E+08 -1.43406E+08
3.94952E+07 9.93174E+05
3.25854E+04 -3.67183E+04 -2.57392E+03 -3.72067E+01 4.20588E+01 2.56069E+00 -1.45203E+08 -8.58606E+08
1.99298E+07 -1.30267E+03 9.92470E+05
-2.02055E+03 2.31452E+03 2.47115E+00 2.21733E+00 -2.53874E+00 -9.66537E-03 3.98806E+07 1.99271E+07
-7.31579E+06 3.59396E+02 1.82549E+02 9.9932E+05
7.95618E+08 -9.14109E+08 5.95473E+07 -3.34592E+05 1.07601E+06 -9.15048E+04 3.12931E+12 -6.90444E+12
-5.88683E+12 2.78551E+08 -6.49518E+07 -3.41541E+07 5.08940E+13
-7.22552E+08 8.31115E+08 2.34831E+05 7.62724E+05 -8.75805E+05 -1.33712E+04 2.33184E+13 -5.15376E+12
-4.58690E+12 2.11323E+08 -4.39960E+07 -4.12697E+07 -3.60614E+13 7.19750E+13
-2.12015E+06 -7.63588E+06 5.25016E+07 1.13195E+04 -2.09949E+03 -6.68831E+04 -5.36032E+12 1.18309E+12
1.01227E+12 -4.75526E+07 1.01820E+07 3.19850E+06 8.31580E+12 6.27613E+12 9.86246E+13
2.45174E+04 -2.82214E+04 1.56221E+03 -2.76669E+01 3.18611E+01 -1.06213E+00 2.83191E+08 -6.25285E+07
-5.32841E+07 2.47599E+03 -4.35056E+02 -4.89451E+02 -4.35214E+08 -3.32488E+08 7.56176E+07 9.95984E+05

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22. A PIVOT RATIO EXCEEDS 10**5.
CHECK ATA MATRIX FOR ILL CONDITIONING.

[illegible]

ITEM	DESCRIPTION	REFERENCE SECTION
22	<u>A remark printed when the $A^T A$ matrix is inverted if a pivot ratio exceeds 10^5. It hints that the $A^T A$ may be ill-conditioned</u>	

0003 DY -2.87436E-06-2.16307E-06-2.14964E-01 5.16675E-01 1.26298E-06 8.74711E-07 1.59626E-01-2.53642E-01
 0003 FZ 7.37147E-01-1.05361E+00 1.36986E-06-1.10765E-06-1.53908E+00 4.35296E-01 1.95535E+02-3.65703E-02
 6.59625E-07 5.09326E-07 5.07943E-02-1.40773E-01-2.62087E-07-1.81147E-07-3.31229E-02 5.25211E-02
 -1.69743E-01 2.41374E-01-3.07621E-07 2.47328E-07 3.53863E-01-9.60879E-02-5.05561E+01 9.41950E-03

ATA(INVERSE) FOR P AND Q PARAMETERS

	0001 X	0001 Y	0001 Z	0001 DX	0001 DY	0001 DZ	0002 X	0002 Y	0002 Z	0002 DX	0002 DY	0002 DZ
0001 X	1.000											
0001 Y	-0.978	1.000										
0001 Z	-0.091	-0.112	1.000									
0001 DX	-0.920	0.862	0.101	1.000								
0001 DY	0.920	-0.916	0.077	-0.981	1.000							
0001 DZ	0.101	0.073	-0.887	-0.107	-0.082	1.000						
0002 X	0.000	-0.000	0.000	-0.000	-0.000	-0.000	1.000					
0002 Y	-0.015	0.018	-0.007	-0.001	-0.001	-0.001	-0.000	1.000				
0002 Z	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	1.000			
0002 DX	0.000	-0.000	0.000	-0.000	-0.000	-0.000	0.000	0.000	0.000	1.000		
0002 DY	-0.000	0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	1.000	
0002 DZ	-0.000	0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	1.000

CORRELATION MATRIX

	0001 X	0001 Y	0001 Z	0001 DX	0001 DY	0001 DZ	0002 X	0002 Y	0002 Z	0002 DX	0002 DY	0002 DZ
0001 X	1.000											
0001 Y	-0.978	1.000										
0001 Z	-0.091	-0.112	1.000									
0001 DX	-0.920	0.862	0.101	1.000								
0001 DY	0.920	-0.916	0.077	-0.981	1.000							
0001 DZ	0.101	0.073	-0.887	-0.107	-0.082	1.000						
0002 X	0.000	-0.000	0.000	-0.000	-0.000	-0.000	1.000					
0002 Y	-0.015	0.018	-0.007	-0.001	-0.001	-0.001	-0.000	1.000				
0002 Z	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	1.000			
0002 DX	0.000	-0.000	0.000	-0.000	-0.000	-0.000	0.000	0.000	0.000	1.000		
0002 DY	-0.000	0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	1.000	
0002 DZ	-0.000	0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	1.000
0003 X	-0.002	0.002	-0.001	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
0003 Y	1.000	-0.001	-0.001	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
0003 Z	-0.536	1.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
0003 DX	-0.117	0.074	1.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
0003 DY	-0.051	-0.039	-0.008	1.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
0003 DZ	-0.046	-0.329	0.006	-0.003	1.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
SQRT DIAG	6.378695E+05	7.439833E+05	1.004285E+06	6.596158E+06	7.525788E+02	9.915107E+02						

0.718984E+06 2.076192E+06 9.959324E+06 9.990364E+02 9.962284E+02 9.999658E+02
 7.134112E+06 8.483860E+06 9.930992E+06 9.979902E+02 9.989385E+02 9.999427E+02

STATE COVARIANCE AND CORRELATION MATRIX PARTITIONS AT 1.500000000E+01 MWOED

CARTESIAN FOR	P	PARAMETERS	VEHICLES	1 AND	1
3.2175436E+08	-3.606708E+00	-5.102480E+07	2.208294E+04	1.6878030E+04	2.4263728E+03
1.7937529E+04	4.191498E+08	-4.529713E+07	-2.707472E+04	-1.9063559E+04	-3.4465145E+03
-9821162	2.0473149E+04	7.270038E+08	6.225284E+03	5.4383081E+03	4.6664559E+03
-1670885	-0.020075	2.6979426E+04	4.3609561E+05	-4.888323E+05	-7.0230478E+04
.0019318	-0.020026	.0003494	6.6037536E+02	5.6810087E+05	-6.1300055E+04
.0012336	-0.012072	.0002574	-9.021153	7.5372467E+02	9.8642773E+05
.0001352	-0.0001695	.0001741	-1.070705	-0.0020047	9.9319068E+02

ORBIT PLANE FOR	P	PARAMETERS	VEHICLES	1 AND	1
2.7777930E+06	3.7919996E+07	7.0223517E+07	-2.3640455E+03	3.2425201E+02	6.0705633E+02
2.9627340E+03	7.3241417E+00	-3.6698800E+06	-4.4261641E+04	6.1262670E+03	4.3502473E+03
.4729304	2.7063152E+04	7.2760224E+08	-5.2678386E+02	4.2365401E+01	3.9236209E+03
.8787046	-0.050272	2.6974103E+04	1.1898322E+04	9.9268444E+03	9.5165149E+04
-0.0073151	-0.0149936	-0.001790	1.0907943E+02	-4.9926390E+03	9.8604146E+05
.0001098	.0002272	.0000016	.4720854	9.9633551E+02	9.9299620E+02
.0002053	.0001619	.0001465	.8785925	-0.0050463	

CARTESIAN FOR	P AND Q	PARAMETERS	VEHICLES	1 AND	1
6.2200139E+10	-7.1403303E+10	1.6742802E+09	4.5846001E+06	3.3563025E+06	5.51233725E+05
2.4939956E+05	8.6394210E+10	-3.2655144E+10	-5.6863541E+06	-4.1999294E+06	-8.4880572E+05
-0.0741042	2.9391192E+05	2.1393226E+11	3.0695054E+06	2.5056440E+05	1.5101347E+06
.0145141	-0.2402132	4.6252812E+05	4.3647236E+05	-4.0855900E+05	-7.0169303E+04
.0278250	-0.0292845	.0100450	6.6066055E+02	5.6030829E+05	-6.1341510E+04
-0.178514	-0.0149554	.0071855	-9.809513	7.5306225E+02	9.0644313E+05
.0022254	-0.0023077	.0033047	-1.069383	-0.0019269	9.9319843E+02

ORBIT PLANE FOR	P AND Q	PARAMETERS	VEHICLES	1 AND	1
2.6822083E+09	1.1571932E+10	2.1456425E+10	-7.2146624E+05	9.0954600E+04	1.8545159E+05
5.1790041E+04	1.5695296E+11	3.4073570E+10	-9.5157091E+06	1.3155750E+06	1.1250127E+06
		2.0298145E+11	-2.3165101E+06	3.1210067E+05	1.3097766E+06

.5641743	3.9604666E+05	1.2473137E+04	5.1313587E+04	9.5096076E+04
.0199946	.1954444	4.5053463E+05	9.9269943E+05	-4.9831336E+03
-.1247332	-.2151330	1.1168320E+02	9.9634102E+02	9.8605522E+05
.0019177	.0033340	.4611439		
.0035051	.0024606	.8574802	-.0050367	9.9300313E+02

CAPTESIAN	FOR	P	PARAMETERS	VEHICLES	2	AND	2
7.6105349E+13	-1.6288492E+13	4.5017469E+12	3.1628196E+08	-3.0290905E+08			1.3216039E+07
8.7238379E+06	3.5903182E+12	2.2519239E+12	-6.7715842E+07	6.7798093E+07			1.0688901E+07
-.9853870	1.8949135E+06	9.9558389E+13	1.7985559E+07	7.3707056E+07			4.1820151E+08
.0517171	.1131100	9.9778350E+06	9.9762234E+05	-1.3567849E+03			5.4543889E+01
.0362981	-.0357800	.0018047	9.9881046E+02	9.8498301E+05			5.4700879E+01
-.0343857	.0350526	.0074431	-.0013687	9.9246310E+02			9.9797595E+05
.0015155	.0055469	.0419553	.0000547	.0000552			9.9898746E+02

OPBIT PLNE	FOR	P	PARAMETERS	VEHICLES	2	AND	2
5.0255705E+12	1.9042156E+13	2.9388060E+12	8.3808996E+07	7.6922440E+07			1.2424508E+07
2.2418007E+06	7.4163309E+13	-2.9536344E+12	3.1663350E+08	-2.9974764E+08			-1.1871329E+07
.0862954	8.6121605E+06	1.0005308E+14	5.5407029E+07	-1.2868180E+07			4.1872493E+08
.1310526	-.0342860	1.0002353E+07	9.8510818E+05	1.8315264E+03			2.3123263E+02
.0376652	.0370427	.0055808	9.9752616E+02	9.9749443E+05			-6.3530632E+01
.0343559	.0344488	-.0012881	.0018476	9.9874643E+02			9.9797868E+05
.0055478	-.0017798	.0419025	.0002332	-.0000637			9.9898883E+02

CAPTESIAN	FOR	P	AND Q	PARAMETERS	VEHICLES	2	AND	2
7.6105407E+13	-1.6283194E+13	4.5017313E+12	3.1628212E+08	-3.0292179E+08			1.3215736E+07	
8.7238413E+06	3.5907853E+12	2.2521128E+12	-6.7717793E+07	6.7951823E+07			1.0692555E+07	
-.9842692	1.8970465E+06	9.9558393E+13	1.7985515E+07	7.3710470E+07			4.1820160E+08	
.0517169	.1142798	9.9778352E+06	9.9762234E+05	-1.3568203E+03			5.4543046E+01	
.0362981	-.0337389	.0018047	9.9881046E+02	9.8498301E+05			5.4767227E+01	
-.0349871	.0560918	.0074435	-.0013688	9.9246451E+02			9.9797595E+05	
.0015154	.0055421	.0419553	.0000547	.0000552			9.9898746E+02	

OPBIT PLNE	FOR	P	AND Q	PARAMETERS	VEHICLES	2	AND	2
5.0341812E+12	1.9042550E+13	2.9387430E+12	8.3963136E+07	7.6918836E+07			1.2424516E+07	
	7.4159327E+13	-2.9536373E+12	3.1664063E+08	2.9974748E+08			-1.1871329E+07	

2.2436981E+06		1.0005908E+14	5.5405890E+07	-1.2868154E+07	4.1872493E+08
.9854816	8.6121616E+06		9.8511097E+05	1.8314611E+03	2.3123278E+02
.1309390	-.0342860	1.0002953E+07		9.9749443E+05	-6.3930635E+01
.0377035	.0370435	-.0055807	9.9252757E+02		9.9797888E+05
.0343252	.0343488	-.0012981	.0018476	9.9874643E+02	
.0055431	-.0013798	.0419025	.0002332	-.8000637	9.9898883E+02

CAPTEIAN FOR					
	P	PARAMETERS	VEHICLES	3 AND	3
5.0629232E+13	-3.6557197E+13	8.4278945E+12	1.4277494E+08	-4.9555185E+08	3.5499598E+07
	7.2805002E+13	6.4011415E+12	3.4237504E+07	1.1819530E+09	2.7180448E+07
7.1154221E+06		9.8986190E+13	6.1108247E+07	1.3776983E+08	4.1398887E+08
-.6021277	8.5325433E+06		9.9620641E+05	-1.7982520E+03	2.527148E+02
.1190505	.0754026	9.9491804E+06		1.0037179E+06	5.7554781E+02
.0201037	.0040202	.0061537	9.9810141E+02		9.9796212E+05
-.0695155	.1392645	.0138217	-.0017983	1.0018572E+03	
.0049942	.0031864	.0416528	.0002932	.0005751	9.9898883E+02

ORBIT PLNE FOR					
	P	PARAMETERS	VEHICLES	3 AND	3
5.8638558E+13	3.8077557E+13	7.8605884E+12	1.0612808E+09	1.4011883E+08	3.3304398E+07
	6.4795676E+13	-7.0862562E+12	6.6990658E+08	2.6343999E+08	-2.9811547E+07
7.657818E+06		9.8986190E+13	1.4678912E+08	-3.4343804E+07	4.1398887E+08
.6177334	8.0435383E+06		1.8027977E+06	3.8494283E+03	6.1251480E+02
.1031754	-.0884818	9.9491804E+06		9.9712662E+05	-1.4870627E+02
.1383996	.0831058	.0147293	1.0013979E+03		9.9796212E+05
.0183243	.0327741	-.0034568	.0030496	9.9856228E+02	
.0043536	-.0037072	.0416528	.0006123	-.8001411	9.9898883E+02

CAPTEIAN FOR					
	P AND Q	PARAMETERS	VEHICLES	3 AND	3
5.0630830E+13	-3.6555984E+13	8.4278945E+12	1.4278609E+08	-4.9552519E+08	3.5498540E+07
	7.2805923E+13	6.4009328E+12	3.4245938E+07	1.1819727E+09	2.7159649E+07
7.1155344E+06		9.8986237E+13	6.1106336E+07	1.3776539E+08	4.1398905E+08
-.6020944	8.5325973E+06		9.9620649E+05	-1.7980722E+03	2.5246418E+02
.1190447	.0753997	9.9491827E+06		1.0037183E+06	5.7553882E+02
.0201050	.0040211	.0061535	9.9810144E+02		9.9796212E+05
-.0695108	.1382659	.0138212	-.0017982	1.0018574E+03	
.0049940	.0031863	.0416528	.0002932	.0005751	9.9898883E+02

ORBIT PLNE FOR					
	P AND Q	PARAMETERS	VEHICLES	3 AND	3
5.8639947E+13	3.8075304E+13	7.8603321E+12	1.0613136E+09	1.4011235E+08	3.3303411E+07

7.6576725E+06	6.4737606E+13	-7.0860351E+12	6.6980348E+08	2.6344511E+08	-2.9810664E+07
.6177004	8.0497084E+06	9.8986237E+13	1.4674439E+08	-3.4341956E+07	4.139895E+08
.1031708	-.0884781	9.9491827E+06	1.0027981E+06	3.0493235E+03	6.1251675E+02
.1384013	.0831022	.0147288	1.0013981E+03	9.9712664E+05	-1.4070227E+02
.0183233	.0327744	-.0034567	.0030495	9.9796212E+05	9.9796212E+05
.0043535	-.0037071	.0416528	.0006123	9.98562229E+02	9.9898054E+02
				-.0001410	

CARTESIAN FOR P PARAMETERS VEHICLES 2 AND 1

COVARIANCE					
8.9345990E+06	-1.0595572E+07	2.6084191E+06	-5.7085902E+05	6.7375314E+05	-1.3448435E+05
-1.0831504E+08	1.2023072E+08	-2.9982556E+07	1.1551890E+05	-1.5208875E+05	2.8172856E+04
-2.4000922E+06	2.8437946E+06	-6.8103335E+05	1.3843679E+04	-1.7347943E+04	8.0536665E+03
2.4704883E+01	-2.9352397E+01	7.6393884E+00	1.5411378E+01	-1.8101439E+01	3.2920418E+00
-1.9641803E+03	2.3264094E+03	-5.5121137E+02	-3.5973200E+01	4.8461576E+01	2.8325075E+00
-4.6799327E+01	5.5381141E+01	-1.2793777E+01	2.2038050E+00	-2.5225904E+00	-3.9131161E-02

CORRELATION					
.0000571	-.0031868	-.0000134	.0000014	-.0001103	-.0000026
-.0000593	.0033055	.0000139	-.0000814	.0001145	.0000027
.0000111	-.0005865	-.0000025	.0000003	-.0000206	-.0000005
-.0000991	.0000923	.0000021	.0000234	-.0000549	.0000033
.0001025	-.0001065	-.0000023	-.0000240	.0000541	-.0000034
-.0000155	.0000150	.0000008	.0000033	.0000029	-.0000000

ORBIT PLNE FOR P PARAMETERS VEHICLES 2 AND 1

COVARIANCE					
-7.9585977E+06	-1.7071423E+08	-3.8553223E+05	2.1637573E+04	2.2444095E+05	-6.0226233E+03
-4.2530105E+05	-7.8662167E+06	-1.4692637E+05	4.4653358E+04	8.8274587E+05	-2.0269566E+04
6.5781894E+04	1.2632631E+06	-2.4304708E+03	-2.4454433E+03	-5.6316699E+04	5.9439000E+03
-1.6285789E+02	-3.0901438E+03	-1.4150869E+01	-1.4279296E+00	-3.3534847E+01	1.2191114E+01
3.7535057E+00	7.2419108E+01	-3.1988955E-01	-1.0963108E+00	-2.1573836E+01	3.6749836E-01
2.3497174E-02	-2.5862197E-01	3.8244596E-01	2.4532861E-01	6.4853808E+01	-9.6722833E-01

CORRELATION					
-.0013488	-.0000167	.0000022	-.0000554	.0000013	.0000000
-.0029138	-.0000338	.0000047	-.0001150	.0000027	-.0000000
-.0000054	-.0000006	-.0000008	-.0000005	-.0000000	.0000000
.0000885	.00000475	-.0000022	-.0000132	-.0000101	.0000023

.0001005	.0001029	-.0000357	-.0000541	-.0000217	.0000065
-.0000027	-.0000024	.0000006	.0000124	.0000004	-.0000010

CARTESIAN FOR P AND Q PARAMETERS VEHICLES 2 AND 1

COVARIANCE

1.7929353E+09	-2.2310125E+09	1.2508071E+09	-4.2283156E+05	7.6356927E+05	-1.7023655E+05
-2.1703684E+10	2.6947660E+10	-1.4682790E+10	-1.6705065E+06	-1.4765808E+06	-2.6216529E+05
-4.8132437E+08	5.9814394E+08	-3.3032415E+08	-2.5820093E+04	-4.6767197E+04	1.5830111E+03
4.9646370E+03	-5.1954654E+03	3.5873131E+03	1.5822968E+01	-1.7795963E+01	3.3600461E+00
-3.9380451E+05	4.9917853E+05	-2.6849246E+05	-6.8400543E+01	1.6411591E+01	-2.4491887E+00
-9.3774215E+03	1.1633327E+04	-6.2961199E+03	1.4329710E+00	-3.0941809E+00	-1.6421889E-01

CORRELATION

.0006241	-.0458860	-.0001334	.0000199	-.0015910	-.0000376
-.0009701	.0493310	.0002040	-.0000211	.0016768	.0000396
.0003100	-.0157337	-.0000715	.0000078	-.0005849	-.0000136
-.0000734	-.0013329	-.0000039	.0000240	-.0001043	.0000022
.0001131	-.0010325	-.0000152	-.0000236	.0000219	-.0000041
-.00000127	-.00001391	.0000002	.0000034	-.0000025	-.0000002

ORBIT PLNE FOR P AND Q PARAMETERS VEHICLES 2 AND 1

COVARIANCE

-2.7339520E+09	-3.6620775E+10	-8.4749313E+09	2.2333139E+06	-8.134371E+04	-2.6946647E+05
-1.2975691E+08	-1.6937524E+09	-4.2657753E+08	1.4698314E+05	8.6860064E+05	-3.2641239E+04
2.0074590E+07	2.7073002E+08	6.1238609E+07	-1.8794398E+04	-5.4056464E+04	7.8838342E+03
-4.9700173E+04	-5.6323391E+05	-1.5543071E+05	3.8629511E+01	-5.9072546E+01	7.4095292E+00
1.1454750E+03	1.5511296E+04	3.4602115E+03	-2.0329611E+00	-2.1444342E+01	4.7838349E-01
7.1896143E+00	-3.6705656E+01	9.4110508E+01	2.4743495E-01	6.4850854E+00	-9.6693755E-01

CORRELATION

-.0235277	-.0002910	.0000388	-.0009669	.0000221	.0000001
-.0412113	-.0004966	.0000593	-.0016872	.0000392	-.0000001
-.0003039	-.0001099	.0000136	-.0003475	.0000077	.0000002
.0003125	.0001528	-.0000168	.0003485	-.0000182	.0000022
-.0000354	.0001012	-.0000054	-.0000597	-.0000216	.0000065
-.00001209	-.0000038	.0000008	.0000075	.0000005	-.0000010

CARTESIAN FOR P PARAMETERS VEHICLES 3 AND 1

COVARIANCE

-4.7072220E+07	5.5719171E+07	-1.2973433E+07	-9.5053022E+05	1.1031335E+06	-9.3143039E+04
-3.5747314E+07	4.230831E+07	-9.8167056E+06	7.6735620E+05	-8.6119579E+05	-1.3701253E+04
8.0924852E+06	-9.5814814E+06	2.2473430E+06	1.3403693E+04	-4.5173460E+03	-6.7029143E+04
-3.2652510E+02	3.8691540E+02	-9.2290060E+01	-2.1487343E+01	2.4755126E+01	-1.5277315E+00
-7.6135299E+02	9.0141211E+02	-2.1116079E+02	5.5762450E+00	-5.4063330E+00	-5.7775596E-01
3.0752677E+01	-3.6473753E+01	9.0161460E+00	2.3323757E+00	-2.6832796E+00	1.3464129E-01

CORRELATION

-0.0003688	-0.0002336	0.0000453	-0.0000162	-0.0000424	0.0000017
0.0003825	0.0002422	-0.0000470	0.0000169	0.0000439	-0.0000018
-0.0000676	-0.0000426	0.0000084	-0.0000074	-0.0000078	0.0000003
-0.0002040	0.0001362	0.0000020	-0.0000328	0.0000084	0.000003
0.0002057	-0.0001370	-0.0000005	0.0000329	-0.0000085	-0.0000007
-0.0000132	-0.0000016	-0.0000068	-0.0000015	-0.0000005	0.000000

ORBIT PLANE FOR P PARAMETERS VEHICLES 3 AND 1

COVARIANCE

-3.6119072E+06	-5.8997043E+07	-6.9181319E+04	3.1336702E+04	6.5621658E+05	-1.8235477E+05
3.2605457E+05	5.2210135E+07	9.9138303E+04	6.2719971E+04	1.6428049E+06	-1.9951150E+05
6.6835049E+05	1.2723825E+07	3.5376742E+04	-7.3386461E+03	6.6245002E+02	-6.8107633E+04
-6.6810547E+01	-1.2718436E+03	-3.5651900E+00	6.6506855E-02	2.0495404E+00	-1.2271795E+00
1.4944146E+01	2.8159102E+02	2.3602907E+00	1.2980074E+00	3.3492600E+01	-4.4945657E+00
2.5914387E+00	4.8494593E+01	5.9594340E-01	1.3417492E-01	3.5220987E+00	-4.8467717E-01

CORRELATION

-0.0001592	0.0001367	0.0000227	-0.0000225	0.0000051	0.0000009
-0.0003329	0.0002856	0.0000473	-0.0000469	0.0000104	0.0000018
-0.0000003	0.0000005	0.0000001	-0.0000001	0.0000001	0.0000000
0.0000375	0.0000714	-0.0000068	0.0000006	0.0000119	0.0000012
0.0001122	0.0002848	0.0000001	0.0000021	0.0000337	0.0000035
-0.0000240	-0.0000250	-0.0000069	-0.0000012	-0.0000045	-0.0000005

CAPTESTAN FOR P AND Q PARAMETERS VEHICLES 3 AND 1

COVARIANCE

-9.4338096E+09	1.1707609E+10	-6.3640370E+09	-1.7344136E+06	5.2776632E+05	-2.1919405E+05
-7.1635924E+09	9.8897466E+09	-4.8224169E+09	1.7832682E+05	-1.3179879E+06	-1.8934715E+05
1.6221027E+09	-2.0137731E+09	1.0991525E+09	1.4688048E+05	9.4469452E+04	-4.5321068E+04

-6.5476689E+04 8.1352974E+04 -4.4829563E+04 -2.6881528E+01 2.0754286E+01 -2.4072221E+00
 -1.5260734E+05 1.8944432E+05 -1.0332328E+05 -6.9601579E+00 -1.5720116E+01 -2.6195112E+00
 6.1720029E+03 -7.6819708E+03 4.3192140E+03 2.8421303E+00 -2.3050970E+00 2.1819919E-01

CORRELATION

-0.053160 -.0033663 .0006537 -.0002630 -.0006108 .0002248
 .0055981 .0035444 -.0006887 .0002773 .0006434 -.000262
 -.0019337 -.0012219 .0002389 .0000971 -.0002230 .0000093
 -.0003689 .0000316 .0002223 -.0000408 -.0000105 .0000043
 .0000984 -.0002049 .0000126 .0000276 -.0000208 -.0000031
 -.0000310 -.0000129 -.0000046 -.0000024 -.0000026 .0000002

ORBIT PLNE FOR P AND Q PARAMETERS VEHICLES 3 AND 1

COVARIANCE

-1.1022504E+09 -1.4794515E+10 -3.4006298E+09 9.2481217E+05 7.3269624E+05 -2.8859861E+05
 9.9505853E+08 1.3342944E+10 3.0768329E+09 -7.4310476E+05 1.7542074E+06 -1.0358416E+05
 2.0396584E+08 2.7297776E+09 6.3352011E+08 -1.7220284E+05 2.3454186E+04 -4.8460640E+04
 -2.0388035E+04 -2.7296356E+05 -6.3333280E+04 1.6546038E+01 -2.2868040E-01 -3.1911187E+00
 4.5605331E+03 6.0430028E+04 1.4460859E+04 -2.3557267E+00 3.3997695E+01 -4.0568125E+00
 7.9045116E+02 1.0424517E+04 2.5428107E+03 -4.9554400E-01 3.6091494E+00 -4.0898026E-01

CORRELATION

-0.0027793 .0023868 .0003358 -.0003931 .0000882 .0000153
 -.0048782 .0041853 .0006328 -.0006880 .0001530 .000263
 -.0009857 .0008484 .0001413 -.0001404 .0000321 .0000056
 .0010814 -.0008266 .0001350 .0001479 -.0000211 -.0000044
 .0000950 .0002187 .0000024 -.0000082 .0000342 .0000034
 -.0000380 -.0000130 -.0000049 -.0000032 -.0000041 -.0000004

CARTESIAN FOR P PARAMETERS VEHICLES 3 AND 2

COVARIANCE

3.1709093E+13 -7.0437679E+12 -6.0675963E+12 1.2982352E+08 -1.3570345E+08 -2.7984726E+07
 2.378979E+13 -5.2885328E+12 -4.6791937E+12 1.0170649E+08 -9.7512713E+07 -2.1305368E+07
 -5.4229338E+12 1.2042102E+12 1.0245682E+12 -2.2138259E+07 2.2273272E+07 4.7706077E+06
 2.2762875E+08 -5.0548372E+07 -4.3062959E+07 9.0087824E+02 -8.6890320E+02 -2.0552304E+02
 5.1910930E+08 -1.1537144E+08 -1.0112271E+08 2.1737610E+03 -2.1477007E+03 -4.5707086E+02
 -2.1875331E+07 4.8614707E+06 4.2641136E+06 -9.8855506E+01 9.3499666E+01 1.8132437E+01

CORRELATION

.5108290	.3195837	-.0624798	.0261421	.0593944	-.0025101
-.5224418	-.3271035	.0638776	-.0267280	-.0607751	.0025865
-.0854628	-.0549602	.0103208	-.0043240	-.0101159	.0004276
.0182671	.0119339	-.0022278	.0009037	.0021723	-.0000991
-.0192156	-.0115150	.0022557	-.0008772	-.0021600	.0000943
-.0039375	-.0024995	.0004900	-.0002061	-.0004567	.0000162

OREIT PLNE FOR P PARAMETERS VEHICLES 3 AND 2

COVARIANCE

-7.7038152E+12	-2.9331922E+13	-3.0946338E+12	-1.2612934E+08	-1.2118719E+08	-1.2869571E+07
7.0200599E+12	2.6802400E+13	2.6861559E+12	1.1953547E+08	1.8970563E+08	1.1696893E+07
1.4244650E+12	5.4397275E+12	5.3697096E+11	2.3170555E+07	2.1596085E+07	2.3862947E+06
-1.4528942E+08	-5.5441033E+08	-5.7692753E+07	-2.3652478E+03	-2.2481974E+03	-2.4034054E+02
3.3283377E+07	1.2717354E+08	1.2047932E+07	4.7293946E+02	4.7016263E+02	6.4628846E+01
5.7537103E+06	2.1953896E+07	2.2966167E+06	9.7430944E+01	9.6399917E+01	7.6318236E+00

CORRELATION

-.4487632	.3890160	.0638657	-.0647188	.0148681	.0025692
-.4455811	.3856208	.0634960	-.0642854	.0147880	.0025518
-.0404007	.0333600	.0053355	-.0057595	.0012062	.0002298
-.0165952	.0149616	.0023464	-.0023797	.0004772	.0000983
-.0158456	.0131482	.0021734	-.0022479	.0004714	.0000966
-.0016823	.0014546	.0002401	-.0002402	.0000658	.0000076

CARTESIAN FOR P AND Q PARAMETERS VEHICLES 3 AND 2

COVARIANCE

3.1708788E+13	-7.0400897E+12	-6.0675147E+12	1.2982287E+08	-1.3563666E+08	-2.7987139E+07
2.3788748E+13	-5.2857404E+12	-4.6791277E+12	1.0170589E+08	-9.7462013E+07	-2.1384163E+07
-5.4228814E+12	1.2035774E+12	1.0245541E+12	-2.2138113E+07	2.2261783E+07	4.7703346E+06
2.2762463E+08	-5.0522799E+07	-4.3062391E+07	9.0087239E+02	-8.6843889E+02	-2.0551200E+02
5.1910437E+08	-1.1531191E+08	-1.0112139E+08	2.1737473E+03	-2.1466199E+03	-4.5704517E+02
-2.1875131E+07	4.8594540E+06	4.2640500E+06	-9.8857949E+01	9.3455788E+01	1.8131339E+01

CORRELATION

.5108159	.3195785	-.0624791	.0261419	.0593930	-.0025101
-.5215451	-.3255439	.0637589	-.0265830	-.0606723	.0025642
-.0854603	-.0549591	.0103207	-.0043240	-.0101158	.0004276
.0182657	.0119337	-.0022278	.0009037	.0021723	-.0000991
-.0192068	-.0115089	.0022545	-.0008767	-.0021569	.0000943

--.0039372 --.0024993 .0004900 --.0002061 --.0004567 .0000162

ORBIT PLANE FOR P AND Q PARAMETERS VEHICLES 3 AND 2

COVARIANCE

-7.7003770E+12 -2.9391763E+13 -3.0946592E+12 -1.2606707E+08 -1.2118864E+08 -1.2869568E+07
 7.0169590E+12 2.6802257E+13 2.6861788E+12 1.1947931E+08 1.0570694E+08 1.1696890E+07
 1.4238306E+12 5.4395981E+12 5.3697565E+11 2.3159065E+07 2.1596353E+07 2.3862941E+06
 -1.4522600E+08 -5.5440740E+08 -5.7693221E+07 -2.3640991E+03 -2.2482243E+03 -2.4034048E+02
 3.3269319E+07 1.2717289E+08 1.2048036E+07 4.7268483E+02 4.7015859E+02 6.5628833E+01
 5.7512874E+06 2.1953784E+07 2.2966346E+06 9.7387060E+01 9.6400943E+01 7.6318213E+00

CORRELATION

-.4481793 .3895119 .0637832 -.0646358 .0148492 .0025659
 -.4455734 .3855153 .0634955 -.0642851 .0147879 .0025518
 -.0404006 .0333600 .0053956 -.0057596 .0012062 .0002298
 -.0165858 .0149544 .0023453 -.0023786 .0004769 .0000982
 -.0151456 .0131483 .0021734 -.0022479 .0004714 .0000966
 -.0015823 .0014546 .0002401 -.0002402 .0000658 .0000076

COVARIANCE MATRICES AT 3.000000000E+01 MINUTES FROM MIDNIGHT OF EPOCH DATE

ATA(INVERSE) FOR P PARAMETERS

0001 X	0001 Y	0001 Z	0001 DX	0001 DY	0001 DZ	0002 X	0002 Y
0002 Z	0002 DX	0002 DY	0002 DZ	0003 X	0003 Y	0003 Z	0003 DX
0003 DY	0003 DZ						
2.74180E+08							
-2.37417E+08	2.61362E+08						
-6.54772E+08	2.37305E+08	3.50382E+09					
-8.69804E+04	3.07262E+04	4.66406E+05	7.26134E+01				
5.22055E+04	-3.35331E+04	-1.89425E+05	-3.14774E+01				
4.64280E+05	-1.97844E+05	-2.31668E+06	-3.43168E+02	1.63858E+01			
-1.85173E+07	1.56370E+07	4.16309E+07	1.12133E+04	-7.75487E+03	1.71392E+03	5.06787E+13	
-5.03252E+07	6.64376E+07	-1.32954E+07	-3.29124E+03	-3.08653E+03	-1.07060E+03	-1.43006E+13	4.16315E+12
0002 Z							
-1.71157E+05	1.25592E+06	-5.48692E+06	-1.46479E+03	7.28113E+02	4.45781E+03	3.62444E+12	2.34449E+12
9.85472E+13							
3.60854E+01	-3.37343E+02	1.54137E+03	4.13523E-01	-2.07000E-01	-1.26241E+00	4.50141E+08	-2.20514E+08
3.29638E+08	8.72337E+05						
3.44405E+03	-2.84389E+03	-8.04082E+03	-2.22292E+00	1.52633E+00	7.52866E+00	3.84385E+09	-1.08679E+09

[illegible]

A PIVOT RATIO EXCEEDS 10**5.
CHECK ATA MATRIX FOR ILL CONDITIONING.

DECODE MATRIX

[illegible]


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0002 D7 -1.68013E+01 5.67442E-01-2.40011E-05 1.00242E-05 4.86547E+00 6.40969E+00-2.33809E+04 2.54449E-01
-2.02159E-07-1.98434E-07-1.49435E-02 5.38782E-02-9.93411E-07-7.70007E-07-1.25535E-01 1.59639E-01
3.41740E-01-1.14339E+00 5.58461E-07-5.11778E-07-1.56746E+00 6.65707E-01 1.12404E+03-3.63706E-01
-4.52332E-01-3.45528E-01-3.79708E+04 9.50312E+04 2.45970E-01 1.68943E-01 3.07509E+04-4.87076E+04
1.64714E+05-1.27533E+05 3.04479E-01-2.35827E-01-2.06057E+05 2.24005E+04 9.86071E+07 4.10603E+03
-3.12820E-01-2.35701E-01-2.33405E+04 6.64257E+04 6.25801E-02 3.91121E-02 8.00472E+03-1.48663E+04
1.11264E+05-1.85411E+05 2.01251E-01-1.64122E-01-2.67674E+05 8.59450E+04 1.26004E+00-2.98046E+03
7.75337E-02 5.98431E-02 6.06188E+03-1.67792E+04-6.11210E-03-3.06940E-03-7.56864E+02 1.71574E+03
-2.55452E+04 4.29393E+04-4.08368E-02 3.43725E-02 6.23106E+04-1.05604E+04-3.65000E+07 0.27783E+03
-2.05308E-06-2.37326E-06-2.44175E-01 5.30212E-01-7.73917E-06-5.67014E-06-9.75341E-01 1.39904E+00
-6.21898E-02-6.75162E+00 2.09376E-07-5.39953E-07-8.58990E+00 4.97702E+00 4.75360E+03-2.40246E+00
1.53581E-06 1.06196E-06 8.23593E-02-3.68984E-01-4.02431E-06-3.09770E-06-5.07052E-01 6.53160E-01
-2.74237E-01-6.62721E+00 8.18641E-07-9.57218E-07-8.28604E+00 5.23600E+00 1.72556E+03-1.04088E+00
4.76837E-07 3.61470E-07 4.06354E-02-1.10296E-01 1.71264E+06 1.25716E-06 2.15830E-01-3.07555E-01
8.04524E-02 1.53335E+00 3.27507E-07-1.03958E-07 1.96453E+00-1.09046E+00-1.07458E+03 5.61272E-01

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ATA(INVERSE) FOR P AND Q PARAMETERS

	0001 X	0001 Y	0001 Z	0001 DY	0001 DX	0001 OY	0001 OZ	0002 X	0002 Y
0001 X	1.000								
0001 Y	-.966	1.000							
0001 Z	.012	-.279	1.000						
0001 DX	.852	-.904	.323						
0001 DY	.855	-.945	.471						
0001 OZ	-.053	.087	-.140						
0002 X	-.001	-.001	-.002						
0002 Y	-.041	-.044	-.016						
0002 Z	-.000	-.000	-.000						
0002 DX	.001	-.001	-.001						
0002 DY	.002	-.003	.005						
0002 OZ	-.000	.000	-.000						
0003 X	-.006	.007	-.005						
0003 Y	1.000	.026	-.002						
0003 Z	-.006	.026	-.002						

CORRELATION MATRIX

	0001 X	0001 Y	0001 Z	0001 DY	0001 DX	0001 OY	0001 OZ	0002 X	0002 Y
0001 X	1.000								
0001 Y	-.966	1.000							
0001 Z	.012	-.279	1.000						
0001 DX	.852	-.904	.323						
0001 DY	.855	-.945	.471						
0001 OZ	-.053	.087	-.140						
0002 X	-.001	-.001	-.002						
0002 Y	-.041	-.044	-.016						
0002 Z	-.000	-.000	-.000						
0002 DX	.001	-.001	-.001						
0002 DY	.002	-.003	.005						
0002 OZ	-.000	.000	-.000						
0003 X	-.006	.007	-.005						
0003 Y	1.000	.026	-.002						
0003 Z	-.006	.026	-.002						

0003 Z	1.000	.000	.001	.001	.000	.042	.048	.019	.047	.036	.011
0003 CX	.001	1.000	.001	.001	.000	.032	.010	.053	.214	.061	.049
0003 DY	.089	.068	1.000	.001	.000	.040	.019	.052	.211	.069	.048
0003 DZ	.310	.066	.001	.000	.000	.008	.004	.011	.044	.014	.010
	.001	.000	.000	.000	.000						
	.330	.066	.000	.000	.000						
	.000	.000	.000	.000	.000						
	.070	.067	.066	1.000							
SQRT DIAG	2.331531E+05	3.093228E+05	4.680919E+05	2.062853E+01	1.750148E+01	4.161849E+01					
	7.115913E+06	2.042353E+06	9.927094E+06	9.339901E+02	5.468413E+02	9.960463E+02					
	5.499440E+06	7.144174E+06	9.870712E+06	8.691755E+02	8.711595E+02	9.932011E+02					

STATE COVARIANCE AND CORRELATION MATRIX PARTITIONS AT 3.000000000E+01 MNOED

CARTESIAN FOR	P	PARAMETERS	VEHICLES	1 AND 1
1.9378948E+08	-1.8779915E+08	-9.2356584E+07	4.2205168E+04	-3.3341856E+03
1.3920829E+04	1.9162336E+08	9.1805733E+06	-2.4879282E+04	-5.0279636E+03
.9744986	1.3842809E+04	7.1258805E+08	-1.5345976E+05	7.0338859E+04
.2485329	.0243443	2.6694345E+04	7.2405166E+01	-3.1832935E+01
.3562999	-.2112170	-.6756013	8.5091275E+00	1.6839958E+01
-.0583652	-.0895110	.6421342	-.9116359	1.4584082E+02
-.2655849	.1121873	.6989377	-.9738315	1.7256827E+03
				4.1541338E+01

OPRIT PLNE FOR	P	PARAMETERS	VEHICLES	1 AND 1
7.5416975E+06	1.8191153E+07	6.8709125E+07	5.9283546E+03	-2.2023952E+03
2.7462151E+03	3.6526704E+08	-1.2824916E+07	-2.4087103E+04	-2.3470338E+03
.3465935	1.9111961E+04	7.2519215E+08	7.5337461E+03	-2.4320681E+04
.2290804	-.0249185	2.6929392E+04	1.7323869E+01	-4.0186420E+00
.5146533	-.3024007	.6721435	4.1621952E+00	7.9231670E+00
-.2843125	.0435279	-.3208483	-.3430105	-4.9077642E+01
.6530257	-.0246598	.7057051	.9578592	1.7896808E+03
				2.8148121E+00
				-.4121416
				4.2304619E+01

CARTESIAN FOR	P AND Q	PARAMETERS	VEHICLES	1 AND 1
6.9493670E+10	-7.1830395E+10	4.2433111E+09	4.2629431E+06	4.4721147E+06
2.5361632E+05	7.7301799E+10	-2.9825505E+10	-4.6071619E+06	-5.0536823E+06
		2.1202344E+11	1.9324431E+06	3.8624062E+06
				-1.1995292E+06

-0.9800333	2.7803201E+05	3.4519835E+02	2.7106465E+02	-4.3066653E+02
.0349575	-0.2329706		3.6431550E+02	3.9940895E+01
.8703673	.8919757	1.8579514E+01		1.7619041E+03
.8887948	-0.9523012	.7643631	1.9087051E+01	
-0.1177634	.1259406	-0.5522244	.0498526	4.1975041E+01

ORBIT PLNE	FOR	P AND Q	PARAMETERS	VEHICLES	1 AND 2
2.6202313E+09		1.432274E+10	2.1031839E+10	-7.5854122E+05	-1.6429767E+05
		1.5434906E+11	3.3389114E+10	-9.8017970E+06	-6.6493119E+05
5.1189135E+04			2.0124362E+11	-2.44816375E+06	-1.3476150E+05
.5673726		3.9353569E+05		6.3680297E+02	4.0897672E+01
.0159828		.1837788	4.4860854E+05		1.7995868E+01
-0.5872281		-0.9857535	-0.2192140	2.5234955E+01	-3.5179945E+01
-0.7565154		-0.3991950	-0.7081282	.3820407	1.8166191E+03
-0.0703347		-0.1112393	-0.0296434	.2674675	4.2621815E+01

CARTESIAN	FOR	P	PARAMETERS	VEHICLES	2 AND 2
5.4232313E+13		-8.0842703E+12	3.0686477E+12	1.5211476E+09	-1.4371358E+08
		1.2937805E+12	2.4813391E+12	-2.1902841E+08	4.5161370E+07
7.3642592E+06			9.9779704E+13	3.4338042E+08	7.6011698E+08
-0.9626553		1.1375362E+06		8.5404882E+05	2.9573637E+04
.0539501		.2137734	9.9889791E+06		1.4363980E+04
.2235120		-0.2093502	.0371374	9.2414762E+02	9.8564079E+05
.9235150		-0.8970681	.0205239	-0.1617016	
-0.0196556		.0399892	.0766479	.0322353	9.9279444E+02

ORBIT PLNE	FOR	P	PARAMETERS	VEHICLES	2 AND 2
3.6829691E+12		1.3463305E+13	3.9702101E+12	-8.2344615E+08	7.1922790E+07
		5.16311479E+13	-6.9103222E+11	-3.2118127E+09	1.5259108E+08
1.9191053E+06			9.9991358E+13	3.8165380E+08	7.7204580E+08
.9763272		7.1855040E+06		2.8421278E+05	2.2111891E+04
.2068868		-0.0936174	9.9995779E+06		-2.2259905E+04
-0.8049489		-0.8394383	.0715926	5.3311611E+02	9.8894463E+05
.2602507		.2759922	-0.0497496	.2798882	
.0375861		.0213543	.0776382	.0417079	9.9445695E+02

CARTESIAN	FOR	P AND Q	PARAMETERS	VEHICLES	2 AND 2
5.4232538E+13		-8.06355165E+12	3.9686515E+12	1.5211418E+09	-1.4371197E+08
		1.3017608E+12	2.4816414E+12	-2.1911644E+08	4.5164722E+07

7.3642744E+06	9.9779717E+13	3.4377671E+08	1.8481321E+88	7.6011794E+08
-9.9598855	1.1409473E+06	8.5404987E+05	-7.6397725E+04	2.9573381E+04
.0533502	.2177471		2.6136848E+05	1.4364187E+84
.2235106	-2.079106	9.2414819E+02		9.8564067E+05
.9235960	-8.943767	-1.617088	5.1124218E+82	
-0.0196564	.0338902	.0322329	.8283004	9.9279447E+82

ORBIT PLANE FOR	P AND Q PARAMETERS	VEHICLES	2 AND 2	
3.6905235E+12	1.3461816E+13	3.9703971E+12	-8.2343366E+08	4.5453006E+08
	5.1631930E+13	-6.9106564E+11	-3.2117847E+09	1.8189572E+09
1.9210735E+05	7.1855362E+06	9.9991562E+13	3.815557E+08	-4.5264418E+08
.9752153	-0.096179	9.9995781E+06	2.8421869E+05	1.3576699E+05
.2066847	-8.344187	.0715320		0.2789591E+05
-8.040045	.2759881	-0.0497493	5.3312168E+02	9.0938785E+02
.2600344	.0213538	.0776382	.2798853	-0.0246006
.0375557			.0417074	

CAPTESIAN FOR	P	PARAMETERS	VEHICLES	3 AND 3	
3.7245357E+13	-2.3817105E+13	5.3646343E+12	2.3848586E+09	8.603599E+08	-3.2538613E+88
	4.6287769E+13	1.3549892E+13	-2.5138399E+09	2.8103371E+08	5.4426187E+08
6.1029793E+05	5.8035115E+06	9.8460349E+13	7.0947847E+08	9.2211095E+08	7.8328052E+88
-5734378	.2007114	9.9227188E+06	6.9611045E+05	-2.9547439E+05	5.7171170E+04
.0885855	-4.424589	.0856378		7.2506712E+05	5.8256413E+84
.4683604	-0.045105	.1091348	8.3433238E+02		9.8897333E+05
.1655576	.0807693	.0715598	-4.159026	8.5158873E+02	
-0.0538173			.0691846	.0690758	9.9044898E+82

ORBIT PLANE FOR	P	PARAMETERS	VEHICLES	3 AND 3	
4.0403480E+13	2.4137076E+13	1.4101305E+13	-4.4124417E+04	2.1674425E+89	5.0864289E+88
	4.3137646E+13	-3.6762375E+12	-1.2067573E+04	2.5450611E+89	3.8918487E+08
6.3533732E+06	6.5673927E+06	9.8460349E+13	1.8015768E+09	-5.9282378E+08	7.8328052E+88
.5796429	-0.0554140	9.9227188E+06	6.5327743E+05	2.9822430E+05	6.4779147E+84
.2235824	-2.273412	.1248834		7.6790014E+05	-4.9658983E+84
-0.0858857	.4422347	-0.080857	8.0825579E+02		9.8097333E+85
.3891220	.0594196	.0715598	.4097628	8.7629912E+02	
.0795224			.0809204	-0.8572159	9.9044098E+02

CARTESIAN FOR	P AND Q PARAMETERS	VEHICLES	3 AND 3		
3.7245213E+13	-2.3809235E+13	5.36462157E+12	2.3848818E+09	8.6043756E+88	-3.2531024E+08

6.1031314E+06
 -.5733652
 .0805773
 .4683543
 .1655679
 -.0533156
 4.6289908E+13
 1.3549412E+13
 9.8460456E+13
 9.9227242E+06
 .0876953
 .1091318
 .0715500
 8.3433341E+02
 -.4158968
 .0691841
 -2.5137905E+09
 7.0946735E+08
 6.9611223E+05
 8.5151164E+02
 .0690750
 -2.8093463E+08
 9.2208069E+08
 -2.9547162E+05
 7.2507207E+05
 5.4425434E+08
 7.0328222E+08
 5.7170863E+04
 5.8255964E+04
 9.8097338E+05
 9.9044100E+02

ORBIT PLANE FOR P AND Q PARAMETERS VEHICLES 3 AND 3
 4.0406066E+13 2.4193298E+13 1.4101377E+13 -4.4113075E+08 2.1674032E+09 5.0963408E+08
 4.3132055E+13 -3.6759404E+12 -1.2068248E+09 -5.9201545E+08 2.5450780E+09 3.8910804E+08
 6.3565756E+06 6.5674998E+06 9.9227242E+06 6.5328301E+05 2.9022200E+05 6.4778664E+04
 .5795723 -.0554076 .1248799 .4397575 8.7629978E+02 9.8097338E+05
 .2235668 -.2273492 -.0680947 .0809194 -0.0572156 9.9044100E+02
 -.0858605 .4422301 .0715500
 .3891022 .0533193
 .0795186

CAPTESIAN FOR P PARAMETERS VEHICLES 2 AND 1
 COVARIANCE
 3.1232090E+06 2.9443001E+05 -2.9135322E+07 1.1909740E+04 -8.1240811E+03 -4.0640668E+04
 -5.7815657E+07 5.9930272E+07 -5.3566240E+06 -6.9105460E+03 -1.5820805E+03 1.2684075E+04
 -3.1591471E+06 2.9093819E+06 2.7709021E+06 -1.5894972E+03 7.7654782E+02 4.8814804E+03
 8.1295620E+02 -7.7942765E+02 -4.5706182E+02 3.0540392E-01 -1.2608278E-01 -8.9877067E-01
 -1.6500722E+03 1.0481929E+03 5.3717277E+03 -2.3378132E+00 1.4914903E+00 7.6940044E+00
 -2.1045612E+02 2.0354249E+02 1.0370547E+02 -7.3030366E-02 2.8508172E-02 2.1078724E-01

CORRELATION
 .0000305 -.0036511 -.0000227 .0000632 -.0002319 -.0000152
 .0000029 .0038091 .0000210 -.0000609 .0001481 .0000148
 -.0001482 -.0001764 .0000104 -.0000165 .0003936 .0000039
 .0001901 -.0007139 -.0000187 .0000388 -.0005374 -.0000086
 -.0002688 -.0003389 .0000169 .0000332 .0007109 .0000070
 -.0001328 .0002684 .0000118 -.0000234 .0003623 .8000051

ORBIT PLANE FOR P PARAMETERS VEHICLES 2 AND 1
 COVARIANCE
 -3.2101955E+06 -9.2249597E+07 1.2148580E+07 6.4650181E+03 -2.4010691E+03 1.7431795E+04

3.2847022E+06 1.1240000E+07 2.8084919E+07 2.5264149E+03 -6.8370408E+03 4.1128104E+04
 -3.5453554E+04 -2.1195159E+06 8.0711496E+05 2.2524963E+02 -1.8921858E+02 1.2019700E+03
 4.8391383E+02 -1.0637869E+03 5.6521594E+03 6.9654083E-01 -1.3624322E+00 8.0928454E+00
 -4.3420216E+01 -9.4392402E+02 7.0660722E+01 6.7854998E-02 -1.0115450E-02 1.1438717E-01
 -1.1312092E+01 -1.6093321E+02 -2.8776739E+01 6.7724037E-03 8.0499974E-03 -4.1385660E-02

CORRELATION

-.0005031 .0001665 -.0000013 .0003305 -.0000174 -.0000041
 -.0022425 .0000818 -.0000111 -.0001050 -.0000543 -.0000065
 .0002351 .0001451 .0000030 .0003937 -.0000029 -.0000011
 .0004094 .0007845 .0000054 .0003139 .0000179 .0000016
 -.0004445 -.0003380 -.0000067 -.0009079 -.0000039 .0000029
 .0002147 .0001353 .0000020 .0003566 .0000030 -.0000010

CAPTESIAN FOR P AND Q PARAMETERS VEHICLES 2 AND 1

COVARIANCE

-1.3072635E+09 2.1359723E+09 -6.6122571E+09 -1.2402219E+05 -2.0094045E+05 3.9707840E+04
 -2.2436245E+10 2.4454244E+10 -1.2137929E+10 -1.4625283E+06 -1.6254091E+06 4.8064544E+05
 -9.6213838E+08 9.7711148E+08 8.6431540E+07 -5.8759995E+04 -5.8768303E+04 1.9498230E+04
 2.6993597E+05 -2.8156152E+05 3.853176E+04 1.6887681E+01 1.7622769E+01 -5.5622534E+00
 -1.6868081E+05 4.5522667E+04 1.0621093E+06 -3.2982160E+00 8.4643878E+00 8.4311686E-01
 -7.1151417E+04 7.4590888E+04 -1.3059782E+04 -4.4690406E+00 -4.6981252E+00 1.4661769E+00

CORRELATION

-.0006734 -.0745954 -.0003554 .0011080 -.0012516 -.0002719
 .0010432 .0771838 .0003518 -.0010962 .0003203 .0002702
 -.0019500 -.0231040 .0000188 .0000905 .0004518 -.0000286
 -.0000054 -.0683929 -.0003166 .0009835 -.0003472 -.0002423
 -.0016295 -.0746377 -.0003082 .0009991 .0008674 -.0002479
 .0001285 .0100362 .0000465 -.0001434 .0000393 .0000352

ORBIT PLANE FOR P AND Q PARAMETERS VEHICLES 2 AND 1

COVARIANCE

-2.3483103E+09 -3.4215789E+10 -5.5318956E+09 2.1612656E+06 1.3376933E+05 4.1591467E+05
 1.0115646E+09 6.9751266E+09 6.6956134E+09 -4.4987975E+05 -6.8392068E+04 -6.8014209E+04
 -4.9714549E+07 -8.4327316E+08 -5.1045140E+07 5.3131244E+04 2.5493703E+03 1.0595635E+04
 1.0160626E+05 -1.1027380E+04 1.0679347E+06 -1.1199628E+00 -7.8125594E+00 2.8602480E+00
 -2.895820E+04 -3.9853282E+05 -8.0973104E+04 2.5223731E+01 1.6773461E+00 4.8419719E+00
 -5.8540882E+03 -7.1116741E+04 -2.1668442E+04 4.5093504E+00 3.5281451E-01 8.3781869E-01

CORRELATION							
-.023804	.0027502	-.0009371	.0037233	-.0006216	-.0001150		
-.0452468	.0024664	-.0002142	-.0000525	-.0011135	-.0001817		
-.0064189	.0029771	-.0000114	.0044656	-.0001984	-.0000486		
.0445822	-.0024810	.0002106	-.0000832	.0010985	.0001797		
.0164144	-.0027437	.0000525	-.0003454	.0004346	.0000836		
.0050796	-.0002221	.0002249	.0001259	.0001249	.0000198		
CARTESIAN FOR				PARAMETERS VEHICLES 3 AND 1			
COVARIANCE							
-1.8155415E+07	2.2433560E+07	-3.1441192E+07	9.4384103F+03	-8.7797011E+03	-3.6094135E+04		
-3.1930248E+07	3.2489390E+07	2.5006973E+06	-5.8862105E+03	6.2647240E+02	1.4014430E+04		
7.2395136E+06	-7.3257214E+06	-8.6192345E+05	1.4623386E+03	-2.2015746E+02	-3.7037926E+03		
-1.2687544E+03	1.0732745E+03	1.8883986E+03	-9.3378403E-01	5.2499057E-01	2.9673554E+00		
-1.8737562E+03	1.7455359E+03	1.4683916E+03	-8.5921878F-01	4.0581661E-01	2.5799959E+00		
2.2010438E+02	-1.8034485E+02	-3.750439E+02	1.8071642E-01	-1.0520995E-01	-5.7435009E-01		
CORRELATION							
-.0002137	-.0033371	.0000524	-.0001092	-.0001581	.0000160		
.0002653	.0034448	-.0000533	.0000931	.0001482	-.0000132		
-.0001930	.0031138	-.0000033	.0000846	.0000646	-.0000143		
.0001817	-.0001017	.0000173	-.0001315	-.0001186	.0000214		
-.0003506	.0000224	-.0000054	.0001533	.0001161	-.0000259		
-.0001424	.0031496	-.0000090	.0000856	.0000729	-.0000140		
ORBIT PLANE FOR				PARAMETERS VEHICLES 3 AND 1			
COVARIANCE							
-1.8796040E+06	-4.8154533E+07	7.1111918E+06	3.7491541E+03	-1.4007183E+03	9.8390697E+03		
4.0708517E+06	2.7940878E+07	2.7021943E+07	1.3369839E+03	-6.6890432E+03	3.9255811E+04		
2.7938005E+05	3.9912867E+06	-2.6314635E+06	-9.2257022E+02	5.5496434E+02	-3.6400340E+03		
7.5987196E+01	-2.4121402E+03	2.1344342E+03	3.8871669E-01	-5.0272685E-01	3.0474027E+00		
-1.2724545E+02	1.0234537E+03	-1.8987911E+03	-2.7790057E-01	4.5328522E-01	-2.7459871E+00		
-2.8814194E+01	2.1453347E+02	-4.2035352E+02	-5.9881533E-02	1.0134343E-01	-5.9979105E-01		
CORRELATION							
-.0001077	.0002257	.0000103	.0000342	-.0000529	-.0000106		
-.0003964	.0002226	.0000527	-.0001562	.0000611	.0000113		
.0000415	.0001528	-.0000098	.0000981	-.0000805	-.0000158		

.0001417	.0000409	-.0000223	.0001150	-.0000762	-.0000149
-.0000767	-.0003618	.0000199	-.0002210	.0001030	.0000364
.0000366	.0001413	-.0000091	.0000091	-.0000741	-.0000143

CARTESIAN FOR P AND Q PARAMETERS VEHICLES 3 AND 1

COVARIANCE

-9.588520E+09	1.1192143E+10	-1.1247665E+10	-6.6512593E+05	-0.0355705E+05	2.1638300E+05
-1.1928532E+10	1.2872958E+10	-5.2511087E+09	-7.6930121E+05	-0.4270991E+05	2.520294E+05
2.6745368E+09	-2.0852031E+09	1.1505800E+09	1.7271647E+05	1.8873897E+05	-5.6984837E+04
-3.2072065E+05	3.0054090E+05	2.3016841E+05	-1.0177074E+01	-1.5040705E+01	5.9550021E+00
-5.8642160E+05	5.9899544E+05	2.7939600E+04	-3.5947322E+01	-3.6327432E+01	1.1715750E+01
5.1360163E+04	-4.6009381E+04	-5.5700899E+04	2.7895226E+00	2.2222067E+00	-0.9420201E-01

CORRELATION

-.0059599	-.0055508	.0010244	-.0014502	-.0026147	.0001967
.0065958	.0068052	-.0010469	.0012956	.0025301	-.0001671
-.0040024	-.0013762	.0002518	.0006199	.0000713	-.0001223
-.0058657	-.0050065	.0009360	-.0011727	-.0022722	.0001516
-.0068980	-.0064893	.0009965	-.0009547	-.0022351	.0001175
.0005525	.0008824	-.0001366	.0001701	.0003270	-.0000215

ORBIT PLNE FOR P AND Q PARAMETERS VEHICLES 3 AND 1

COVARIANCE

-1.3652682E+09	-2.0015227E+10	-3.1479570E+09	1.2600391E+06	7.7709051E+04	2.4249670E+05
1.5311329E+09	1.4049993E+10	8.1955842E+09	-8.9739305E+05	-9.8561522E+04	-1.5405704E+05
2.5948243E+08	4.0713392E+09	4.4981908E+08	-2.5683337E+09	-1.4303279E+04	-5.0211404E+04
-2.582972E+04	-8.6223096E+05	2.0917799E+05	5.3069577E+01	8.1263956E-01	1.1342264E+01
-1.2095153E+04	2.8987493E+05	-2.8701045E+05	-1.7699408E+01	1.3286231E+00	-4.4402149E+00
-3.2930006E+03	5.8256275E+04	-6.6786493E+04	-3.5504179E+00	3.3208109E-01	-0.9645641E-01

CORRELATION

-.0041959	.0045545	.0005109	-.0006241	-.0002696	-.0000650
-.0079991	.0054340	.0010423	-.0027101	.0008360	.0001494
-.0011039	.0027817	.0001011	.0005769	-.0007301	-.0001503
.0078802	-.0054148	-.0010257	.0026411	-.0003004	-.0001421
.0028818	-.0035377	-.0003417	.0002370	.0003574	.0000790
.0008951	-.0005504	-.0001187	.0003292	-.0001109	-.0000212

CAPTESIAN FOR P PARAMETERS VEHICLES 3 AND 2

COVARIANCE
 2.2099148E+13 -3.4395954E+12 -3.3545699E+12 -8.2197762E+08 1.7413755E+09 1.8014646E+08
 1.6565361E+13 -2.8084893E+12 -9.9709359E+12 2.0249311E+09 7.2744922E+08 -4.3770901E+08
 -3.7197699E+12 6.3182045E+11 2.2769325E+12 -4.7166258E+08 -1.5958532E+08 1.032171E+08
 1.4906768E+07 -1.9471392E+07 -5.5782561E+08 1.9200818E+05 -4.0939931E+04 -4.1525955E+04
 4.7325437E+08 -9.3138514E+07 -7.0281540E+08 2.0080918E+05 -1.0478753E+04 -4.3489009E+04
 1.8933087E+07 2.9428271E+05 1.0211158E+08 -3.6748088E+04 9.3734110E+03 7.9424910E+03

CORRELATION

.4917049 .3306273 -.0509045 .0024261 .0754704 .0025958
 -.4954505 -.3628895 .0559755 -.0205160 -.0961557 .0002612
 -.0550267 -.4457183 .0229720 -.0669327 -.0826287 .0103211
 -.1157393 .3220593 -.0514352 .2490229 .2551838 -.0401481
 .5581215 .2091451 -.0314587 -.0959812 -.0240713 .0185117
 .0297320 -.0648027 .0104770 -.0501327 -.0514436 .0080773

ORBIT PLANE FOR P PARAMETERS VEHICLES 3 AND 2

COVARIANCE
 -5.4445418E+12 -1.9471883E+13 -8.5829534E+12 7.2253027E+08 -2.0234636E+09 -2.7125238E+08
 5.1369829E+12 1.9600803E+13 3.6226599E+11 -1.7454422E+09 -9.0223646E+08 -1.0475984E+08
 1.0755021E+12 3.8074465E+12 1.9408642E+12 -1.0774311E+08 4.9247107E+08 6.6711463E+07
 -1.6579252E+08 -5.1997125E+08 -7.2071049E+08 -3.9331202E+04 -2.2307450E+05 -2.8941321E+04
 1.8166733E+07 -5.1115869E+06 4.6981564E+08 5.7072649E+04 1.6355908E+05 2.0914424E+04
 1.5489345E+06 -1.0483846E+07 1.0331038E+08 1.3286883E+04 3.6105381E+04 4.6071216E+03

CORRELATION

-.4463267 .4075830 .0564783 -.1068851 .0108025 .0000149
 -.4263255 .4153590 .0534006 -.0895310 -.0008118 -.0014731
 -.1350350 .0055164 .0195506 -.0891724 .0536160 .8184312
 .2132185 -.4985293 -.0203675 -.0912781 .1221670 .0251636
 -.3498633 -.1509871 .0545459 -.3033287 .2051326 .0488641
 -.0429119 -.0150404 .0067506 -.0360067 .0239998 .0046775

CARTESIAN FOR P AND Q PARAMETERS VEHICLES 3 AND 2

COVARIANCE
 2.2099656E+13 -3.4359649E+12 -3.3544447E+12 -8.2201590E+08 1.7413449E+09 1.8013669E+08
 1.6565725E+13 -2.8044183E+12 -9.9708343E+12 2.0248845E+09 7.2745509E+08 -4.3769665E+08

-3.719500E+12 6.3090745E+11 2.2768961E+12 -4.7165319E+08 -1.5958678E+08 1.0320893E+08
 1.4904914E+07 -1.9331267E+07 -5.5782101E+08 1.9200696E+05 -4.0937866E+04 -4.1525639E+04
 4.7326349E+08 -9.2937797E+07 -7.0280726E+08 2.0080692E+05 -1.0477024E+04 -4.3488413E+04
 1.8933926E+07 2.8074875E+05 1.0211094E+08 -3.6747896E+04 9.3729922E+03 7.9424010E+03

CORRELATION

.4917030 .3305263 -.0509055 .0024258 .0754714 .0025959
 -.4934355 -.3612718 .0557274 -.0203600 -.0956767 .0002484
 -.0550233 -.1467125 .0229716 -.0669320 -.0826275 .0103210
 -.1457424 .3220442 -.0514340 .2490209 .2551799 -.0401478
 .5580916 .2031397 -.0314586 -.0959752 -.0240669 .0185107
 .0297330 -.0647994 .0104768 -.0501323 -.0514427 .0080773

ORBIT PLANE FOR P AND Q PARAMETERS VEHICLES 3 AND 2

COVARIANCE

-5.4401219E+12 -1.9472752E+13 -8.5828540E+12 7.2253794E+08 -2.0234121E+09 -2.7124325E+08
 5.1339354E+12 1.9601572E+13 3.6219315E+11 -1.7454148E+09 -9.0227242E+08 -1.0476644E+08
 1.0745013E+12 3.8076181E+12 1.9408418E+12 -1.0774571E+08 4.9246061E+08 6.6709613E+07
 -1.6559894E+08 -5.1990950E+08 -7.2070555E+08 -3.9328983E+04 -2.2307227E+05 -2.8940839E+04
 1.8099837E+07 -5.1079851E+06 4.6981484E+08 5.7070717E+04 1.6355833E+05 2.0914303E+04
 1.5353686E+06 -1.0481338E+07 1.0331001E+08 1.3286445E+04 3.6105230E+04 4.6070975E+03

CORRELATION

-.4454935 .4059175 .0563732 -.1066505 .0107517 .0008069
 -.4263290 .4133667 .0534027 -.0895350 -.0008112 -.0014730
 -.1350289 .0055152 .0195604 -.0891714 .0536157 .0104311
 .2132117 -.4985082 -.0203677 -.0912716 .1221615 .0251625
 -.3498430 -.1503905 .0545447 -.3033242 .2051314 .0400639
 -.0425031 -.0150412 .0067504 -.0360061 .0239996 .0046775

** A BINARY PLOT FILE HAS BEEN GENERATED ON TAPE 12
WITH THE FOLLOWING COMMENTS AND RECORD FORMAT **

WORD	PARAMETER	IN VALUE	MAX VALUE
1	TIME (MIN)	0.	3.00000E+01
** ATA INVERSE WITH P-PARAMETER EFFECTS **			
2 0001	X	1.65584E+04	1.00000E+07
3 0001	Y	1.61729E+04	1.00000E+07
4 0001	Z	5.91930E+04	1.00000E+07
5 0001	OX	8.52135E+00	1.00000E+03
6 0001	OY	4.04794E+00	1.00000E+03
7 0001	OZ	4.13995E+01	1.00000E+03
8 0002	X	7.11930E+06	1.00000E+07
9 0002	Y	2.04038E+07	1.00000E+07
10 0002	Z	3.92709E+06	1.00000E+07
11 0002	OX	3.33330E+02	1.00000E+03
12 0002	OY	5.46933E+02	1.00000E+03
13 0002	OZ	3.96346E+02	1.00000E+03
14 0003	X	5.49928E+06	1.00000E+07
15 0003	Y	7.14504E+06	1.00000E+07
16 0003	Z	3.87071E+06	1.00000E+07
17 0003	OX	8.69174E+02	1.00000E+03
18 0003	OY	8.71158E+02	1.00000E+03
19 0003	OZ	3.93201E+02	1.00000E+03
* C(X) P - PARAMETER EFFECTS *			
20 1	X	1.39208E+04	1.00000E+07
21 1	Y	1.38428E+04	1.00000E+07
22 1	Z	2.65343E+04	1.00000E+07
23 1	OX	3.50912E+00	1.00000E+03
24 1	OY	4.10355E+00	1.00000E+03
25 1	OZ	4.15413E+01	1.00000E+03
* C(P) P - PARAMETER EFFECTS *			
26 1	P	2.74522E+03	1.00000E+07
27 1	T	1.91120E+04	1.00000E+07
28 1	C	2.69234E+04	1.00000E+07
29 1	OP	4.16220E+00	1.00000E+03
30 1	OT	2.81441E+00	1.00000E+03
31 1	DC	4.23041E+01	1.00000E+03

* C(X) P - PARAMETER EFFECTS *
 32 2 X 7.36426E+06 1.00000E+07
 33 2 Y 1.13754E+06 1.00000E+07
 34 2 Z 9.97730E+06 1.00000E+07
 35 2 DX 9.24148E+02 1.00000E+03
 36 2 DY 5.11236E+02 1.00000E+03
 37 2 DZ 9.92714E+02 1.00000E+03

 * C(OP) P - PARAMETER EFFECTS *
 38 2 R 1.91911E+06 1.00000E+07
 39 2 T 7.18550E+06 1.00000E+07
 40 2 C 9.99358E+06 1.00030E+07
 41 2 DR 5.33116E+02 1.00000E+03
 42 2 DT 9.09897E+02 1.00000E+03
 43 2 DC 7.94457E+02 1.00000E+03

 * C(X) P - PARAMETER EFFECTS *
 44 3 X 6.10298E+06 1.00000E+07
 45 3 Y 6.80351E+06 1.00000E+07
 46 3 Z 9.92272E+06 1.00000E+07
 47 3 DX 8.34332E+02 1.00000E+03
 48 3 DY 8.51509E+02 1.00185E+03
 49 3 DZ 9.90441E+02 1.00000E+03

 * C(OP) P - PARAMETER EFFECTS *
 50 3 R 6.35637E+06 1.00000E+07
 51 3 T 6.56739E+06 1.00000E+07
 52 3 C 9.92272E+06 1.00000E+07
 53 3 DR 8.08256E+02 1.00140E+03
 54 3 DT 9.76239E+02 1.00000E+03
 55 3 DC 9.90441E+02 1.00000E+03

 ** ATA INVERSE WITH P+Q PARAMETER EFFECTS **
 56 0001 X 2.33153E+05 1.00000E+07
 57 0001 Y 1.09323E+05 1.00000E+07
 58 0001 Z 4.68032E+05 1.00000E+07
 59 0001 DX 2.06245E+01 1.00000E+03
 60 0001 DY 1.75015E+01 1.00000E+03
 61 0001 DZ 4.16195E+01 1.00000E+03
 62 0002 X 7.11991E+06 1.00000E+07
 63 0002 Y 2.04235E+06 1.00000E+07
 64 0002 Z 9.92709E+06 1.00000E+07
 65 0002 DX 9.33390E+02 1.00000E+03

66 0002	0Y	5.46844E+02	1.00000E+03
67 0002	0Z	3.96046E+02	1.00000E+03
68 0003	X	5.49344E+06	1.00000E+07
69 0003	Y	7.14417E+06	1.00000E+07
70 0003	Z	3.97071E+06	1.00000E+07
71 0003	0X	9.59175E+02	1.00000E+03
72 0003	0Y	3.71160E+02	1.00000E+03
73 0003	0Z	3.93201E+02	1.00000E+03
* C(X) P+C PARAMETER EFFECTS *			
74 1	X	3.49400E+05	1.00000E+07
75 1	Y	2.78032E+05	1.00000E+07
76 1	Z	4.60450E+05	1.00000E+07
77 1	0X	1.85735E+01	1.00000E+03
78 1	0Y	1.90871E+01	1.00000E+03
79 1	0Z	3.19750E+01	1.00000E+03
* C(P) P+C PARAMETER EFFECTS *			
80 1	P	3.11932E+04	1.00000E+07
81 1	T	3.93536E+05	1.00000E+07
82 1	C	4.48509E+05	1.00000E+07
83 1	0P	2.52350E+01	1.00000E+03
84 1	0T	4.24215E+00	1.00000E+03
85 1	0C	3.26218E+01	1.00000E+03
* C(X) P+C PARAMETER EFFECTS *			
86 2	X	7.36477E+06	1.00000E+07
87 2	Y	1.14075E+06	1.00000E+07
88 2	Z	9.97790E+06	1.00000E+07
89 2	0X	9.24148E+02	1.00000E+03
90 2	0Y	5.11242E+02	1.00000E+03
91 2	0Z	3.92734E+02	1.00000E+03
* C(P) P+C PARAMETER EFFECTS *			
92 2	P	1.02107E+06	1.00000E+07
93 2	T	7.18534E+06	1.00000E+07
94 2	C	3.99358E+06	1.00000E+07
95 2	0P	5.33122E+02	1.00000E+03
96 2	0T	3.09848E+02	1.00000E+03
97 2	0C	3.94457E+02	1.00000E+03

* C(X) P+C PARAMETER EFFECTS *			
08 3	X	5.10313E+06	1.00000E+07
09 3	Y	6.80367E+06	1.00000E+07
100 3	Z	3.92272E+06	1.00000E+07
101 3	DX	9.34333E+02	1.00000E+03
102 3	DY	9.51512E+02	1.00185E+03
103 3	DZ	3.90441E+02	1.00000E+03
(23)			
* C(OP) P+C PARAMETER EFFECTS *			
104 3	P	6.35558E+06	1.00000E+07
105 3	T	6.56750E+06	1.00000E+07
106 3	C	3.92272E+06	1.00000E+07
107 3	DP	9.08259E+02	1.00140E+03
108 3	DT	9.76370E+02	1.00000E+03
109 3	DC	3.90441E+02	1.00000E+03

ITEM	DESCRIPTION	REFERENCE SECTION
23	The record formats of TAPE12, containing the square roots of the diagonal elements of the matrices indicated. The minimum and maximum values on the tape for the computations are also printed	2.5.1 [ØPBØX(F)]


```

MODEL DATA
DTIN 3
INFORM1
INTERM0
IPLANT1
22 .6944444444E-3
PLANT
25 1.
PLANT
IIGENM1
SGM .6802328701E-4
INTL 1
LUNAR MODEL
MYRMS04,60
D 02,00
H0 2
FND

2 0
23 16.28810076
17 1.
26 1.
16 1.00002516
ILNORM1
AM .27249217

21 1
24 .6944444444E-3
18 .6944444444E-3
TAPE7-1

CARD 1
CARD 2
CARD 3
CARD 4
CARD 5
CARD 6
CARD 7
CARD 8
CARD 9
CARD 10
CARD 11
CARD 12
CARD 13
CARD 14
CARD 15
CARD 16

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***** LUNAR GRAVITY MODEL *****

GM = 6.802328701E-05 ER**3/MIN**2 = 1.731400L009E+14 FT**3/SEC**2 = 4.9027792902E+12 M**3/SEC**2
 NO NORMALIZATION WITH 1 TERMS.

N	M	CNM	SNM	**	N	M	CNM	SNM
2	0	0.	0.					

***** EARTH GRAVITY MODEL *****

GM = 5.530393500E-03 ER**3/MIN**2 = 1.4076539841E+16 FT**3/SEC**2 = 3.9860318297E+14 M**3/SEC**2
 SPHERICAL EARTH

***** PHYSICAL CONSTANTS *****

GM(ER**3/MIN**2)	=	5.530393500E-03	OMEGA(RAD/MIN)	=	4.375269100E-03	GMLAT(DEG)	=	7.830000000E+01
CMKM(KM**3/MIN**2)	=	0.	OMEGA(RAD/MIN)	=	4.375269100E-03	GMLNG(DEG)	=	2.910030000E+02
SGM(FR**3/MIN**2)	=	6.802328701E-05	OMEGA(RAD/MIN)	=	0.	AM(ER)	=	2.724921700E-01
ERFT(FT/ER)	=	2.092573900E+07	ERKM(KM/ER)	=	6.378164900E+03	ERNM(M/ER)	=	3.443933600E+03
ETKM(FT/KM)	=	3.280839900E+03	FTNM(FT/NM)	=	6.076115500E+03	AE(ER)	=	1.800000000E+00
3SUB0(FT/SEC**2)	=	3.217400000E+01	DGREE(DEG)	=	5.729577951E+01	SLT	=	2.820176300E+03

ITEM	DESCRIPTION	REFERENCE SECTION
1	<p>Card images of the input MODEL data. Emphasis is on the variables associated with a run in the <u>lunar integration mode</u>:</p> <p>PLANT ICENM LNϕRM, NTL SGM, AM</p>	<p>2.1.3 2.1.2.2 2.1.1</p>

CKEP = 1.00000000E-07 F = 3.352329869E-03 PI = 3.141592654E+00

***** INPUT/OUTPUT CONVERSION FACTORS *****

DF(I/O-ER) = 2.09257380E+07 VF(I/O-ER/MIN) = 3.48762300E+05 AF(I/O-ER/MIN**2) = 5.81270500E+03

***** INTEGRATION INPUTS *****

IFORM = 1 ISENT = 1 NSTEP = 2
 NPCMP = 0 IR = 8 ER = 1.00000000E-10
 HMIN = 2.00000000E+00 HMAX = 2.00000000E+00 H0 = 2.00000000E+00

***** SPECIAL OPTIONS *****

TAPE2 = 0 TAPE7 = -1 TELEM = 0 PTAPE = 0 NPDOT = 0
 PRHO = 0 NOOPR = 0 CLASS = 0 LEMSP = 0 PTNS = 10000

***** CRASH ALTITUDE *****

ECI CRASH ALTITUDE(FT) = 3.00000000E+05 MCI CRASH ALTITUDE(FT) = 3.00000000E+03

ENTER SEGMENT 01 AT 121.7 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 121.7 CP SECS., 430.1 PP SECS.

***** VEHICLE DATA *****

IVEHID1	IMNTH 4	IDAY 18	CARD 1
IYEAR 1967	HR 0	MIN 2.468833333E3	CARD 2
TZNE 0			CARD 3
SEC 0			CARD 4
IICYP-11	IC 1.10617555345	2 -4.8269172572	CARD 5
3 -3.3136952336	4 -1.885658509E-3	5 1.010441446E-2	CARD 6
6 7.05817720489E-3			CARD 7
PHASE1			CARD 8
PTIM 1	2 2.842833333E3	3 0	CARD 9
4 720.			CARD 10
6 30.	7 2876.		CARD 11
6 30.	7 3876.		CARD 12
6 30.	7 400.		CARD 13
DPRCODEX			CARD 14
DPRCODE X			CARD 15
END			CARD 16

ITEM	DESCRIPTION	REFERENCE SECTION
2	Card images of the input <u>VEHICLE</u> data. The variables associated with a lunar integration run are emphasized:	11.1.4 11.1.6
	ICTYP PHASE	


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***** HYPERBOLIC ORBIT. F AND G ELEMENT SET IS UNAVAILABLE AT PRESENT. *****
EPOCH
YR/MO/DAY      X,Y,Z,CL,JY,OZ      A,O,B,A,R,V      A,E,I,O,U,TAU      AF,AG,N,L,CHI,PSI
TZME,HP,MIN,SEC  1.967/ 4/18      2.31475398135E+07  2.82907487377E+02  -1.07315621590E+07  0.
1.01005805972E+08  -3.37887309789E+01  1.09681141984E+00  0.
-6.93415182702E+07  1.77947341526E+02  3.87507025093E+31  0.
-6.57645633490E+02  6.97802462480E+01  3.34391443389E+02  0.
2.46688333330E+03  3.52403882722E+03  1.24685322263E+08  9.09284281807E+01  0.
0. 2.46162611579E+03  4.34867242779E+03  2.88904557605E+03  0.

```

THE FOLLOWING BODIES ARE USED FOR PLANETARY PERTURBATIONS
MOON

** NO ATMOSPHERE MODEL **

***** PLANETARY TAPE CONSTANTS *****

BODY	MASS(M)	DIST. SCALE FACTOR(ER)	VEL. SCALE FACTOR(ER/MIN)
SUN	3.32951300E+05	2.34548550E+04	1.62881008E+01
MOON	1.22999000E-02	1.00002516E+00	6.9444444E-04
VENUS	8.14979000E-01	1.00000000E+00	1.00000000E+00
MARS	1.07821000E-01	6.9444444E-04	1.00000000E+00
JUPITER	3.17887000E+02	2.34548550E+04	0.
SATURN	9.51290000E+01	2.34548550E+04	0.

*** PLUS ***

NUTATION(RAC) = 1.000000000E+00 NUTATION RATE(RAD/MSDYS) = 6.9444444E-04

3

REFERENCE
SECTION

DESCRIPTION

ITEM

- | | | |
|---|---|-------------------|
| 3 | A table of planetary constants, as preset or input, and of options requiring the planetary ephemeris tape. In this case, the options are moon perturbations and eclipsing | 2.1.3
11.3.1.2 |
|---|---|-------------------|

***** ECLIPSING CONSTANTS *****
 RE = 1.0000000E+00 RS = 1.09121800E+02 RM = 2.72506300E-01 ERAU = 2.34548650E+04 ④

 ***** PLANETARY EPHEMERIS FILE INITIALIZED WITH 6 BODIES). ⑤ *****

 ENTER SEGMENT 10 AT 122.3 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .5 CP SECS., 3.6 PP SECS.

TRAJECTORY INTEGRATION FOR CASE 1

INVP	0	ICENT	1	IDRAG	0	ALP4G	3.58532850E+00	COAM	0.
JVFP	0	JNORM	1	IR	8	ALG-OES	2.054241915E+02	ER	1.000000000E-10
MVEP	0	MAJOR	0	ISRP	0	TJOATE	2.439598500E+06	HMIN	2.000000000E+00
KVEP	0	MASS	0	NEQS	3	TSTART	2.468833333E+03	HMAX	2.000000000E+00
LVEP	0	NT	0	RECP	0	TSTOP	3.268833333E+03	H0	2.000000000E+00
ICENTX	1	JNORMX	1	NMASSX	0	FLIGHT	8.000000000E+02	NTX	0.
				NASA	0	SSTEP	1.000000000E+02	SORD	1.500000000E+00

* PREDETERMINED EVENT TABLE *

TIME(MME) TYPE
 2468.8333 TZFO
 3268.8333 TSTOP

*** TRAJECTORY START

***** MCI ***** ⑥
 SEG12 ENTRY TIME IS 122.45500

PRECESION MATRIX FROM MEE-EPOCH TO MEE-DATE

9.999999999993E-01	1.7494515030427E-05	4.5619121073485E-07	⑦
-1.0494516030427E-06	9.999999999994E-01	-2.3937529677164E-13	
-4.5619121073485E-07	-2.3937530062820E-13	9.9999999999989E-01	

SELENOGRAPHIC MATRIX FROM MEE-DATE TO MF-DATE

8.5791576365784E-01	5.1353198153613E-01	-1.62925255578576E-02	⑧
-4.4065053901101E-01	7.309717531435E-01	-3.7860096960385E-01	
-1.8133677808800E-01	3.3263875116427E-01	9.2541658696247E-01	

ITEM	DESCRIPTION	REFERENCE SECTION
4	The constants for the determination of eclipsing, requested by PROCDE(H), are the radii of the earth, sun, and moon (in er) and the number of er/au (au = astronomical unit)	11.3.1
5	Indicates the planetary ephemeris file TAPE7 has been initialized (i. e., read) to the date of epoch, with two bodies (sun and moon)	16
6	Output comment specifying the coordinate system in which the numerical integration will be performed	11.1.6
7	Precession matrix used to rotate from MEE of midnight day of epoch to MEE of current date, printed whenever LEMSP = 0	2.1.4
8	<u>Selenographic matrix</u> from MEE to MF, printed when LEMSP = 0	2.1.4

MCI	VECTORS	AT	T	=	2458.833333	U	=	.250000	NSTEP	=	0
			2.31733981	350E+07		-6.57646633	4896E+02		-3.43367990	1077E-04	
			-1.01095805	9718E+08		3.52403882	7223F+03		8.73107496	4750E-03	
			-6.93413182	7016E+07		2.46162611	15785E+03		6.07974970	4093E-03	

ECI	VECTORS
-9.193076299099E+08	-2.605945998745E+03
5.322930504899E+08	9.355392952157E+02
3.230949691360E+08	1.226209106591E+03
	7.263048026485E-03
	3.726008404297E-03
	2.978264333485E-03

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
SELENOPORENTI	1.113596E-02	-2.067551E-03	9.021985E-03	6.193624E-03	-1.113696E-02	3.469447E-17	1.387779E-16	
OTHER BODIES	1.752257E-03	1.724183E-03	-2.909101E-04	-1.138740E-04	6.190841E-04	1.611891E-03	-2.982365E-04	
TOTAL	1.054485E-02	-3.433680E-04	8.731075E-03	6.079750E-03	-1.051788E-02	1.611891E-03	-2.982365E-04	

STEP	DOUBLE	T	H	NSTEP	25
STEP	DOUBLE	T	H	NSTEP	41
STEP	DOUBLE	T	H	NSTEP	57

```

**** CRASH *** ALTITUDE = -76344.0 TIME = 2000.83333 (10)

```

SE612 EXIT TIME IS 125.26410 TOTAL TIME IN SF612 WAS 2.0000 SECONDS TO PROCESS 247 STEPS

MCI	AT	T	=	2980.833333	4	=	2.000000	NSTEP	=	247
		3.791575050137E+06			-2.685598080263E+03			-3.687047484945E+00		
		-3.7441306220623E+06			7.04657935072E+03			3.640811386103E+00		
		-1.8033199931610E+06			4.555337144496E+03			1.754145097956E+00		

FCI VECTORS

ITEM	DESCRIPTION	REFERENCE SECTION
9	The vectors \underline{r} , \underline{i} , and $\underline{\ddot{r}}$ in the integration coordinate frame and in the <u>ECI frame at epoch</u>	Case A: Item 30
10	<u>Indicates when and where the vehicle crashed into the moon</u>	2.1.3 2.1.4

	5.640676741008E+08	4.338720210350F+03	3.636268229247E+00
	3.591575454330E+08	3.245180355542E+03	1.751256984947E+00

	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
SELENOPTENTI	5.470625E+00	-3.587125E+00	3.640842E+00	1.754169E+00	-5.470625E+00	7.203194E-09	4.973799E-14	
OTHER BODYFS	8.737533E-05	7.797226E-05	-3.102316E-05	-2.433802E-05	8.100298E-05	2.006469E-05	-1.689197E-05	
TOTAL	5.470544E+00	-3.547047E+00	3.640811E+00	1.754145E+00	-5.470544E+00	2.007190E-05	-1.689197E-05	

*** VEHICLE CRASHED (U)

*** THIS CASE TOOK 2.876 SECONDS TO INTEGRATE A SPAN OF 412.0000 MINUTES ***

*** FROM 2468.833 TO 2880.833 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 50 AT 125.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 3.0 CP SECS., 49.1 PP SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
11	Remark giving reason for termination (in this case, because the vehicle crashed)	

DATE,...	HF,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	REMARKS
MO/DAY/YR	MIN FROM EPOCH	X (FT)	DX (FT/SEC)	LATITUDE (DEG)	ALPHA (DEG)	REV COUNT	.
HR/MIN	MIN FROM MIDNIGHT	Y (FT)	DY (FT/SEC)	LONGITUDE (DEG)	DELTA (DEG)	PERIOD	.
SEC	SEC FROM MIDNIGHT	Z (FT)	DZ (FT/SEC)	ALTITUDE (NM)	BETA (DEG)	PER-DECAY	.
	STEP SIZE (MIN)	R (FT)	V (FT/SEC)	S-VEH-LAT (DEG)	AZIMUTH (DEG)	NOD-REG	.
	DIST TO MOON (ER)	LAT-MOON (DEG)	LDN-MOON (DEG)	LAT-EARTH (DEG)	LDN-EARTH (DEG)		.

13

SPECIAL OUTPUT OPTIONS REQUESTED

C APOGEE-PERIGEE
J MOON - FIX

401 TRAJECTORY

ITEM	DESCRIPTION	REFERENCE SECTION
12	<u>Key to additional ephemeris output provided in lunar runs</u>	
13	<u>Special output options requested by PRCDE</u>	11.3.1.2

*** CASE 1

*** PUNCH PRINT

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,OZ,V	LAT,...	ALPHA,...	REV,...	MCI
4/19/67	0.00000	2.31475398E+07	-6.57546633E+02	-33.78873098	282.90748738	.77972	
17/ R	2468.83333	-1.01006806E+08	3.52403803E+03	-77.09251221	-33.78873098	0.00000	
50.00000	61730.00000	-6.93415183E+07	2.46162612E+03	19582.12025	177.94734153	0.00000	
	.25000	1.24685322E+08	4.34416724E+03	-33.78873098	69.78024625	0.00000	

CLASSICAL ELEMENTS (A,E,I,O,U,TAU)

-1.07315622E+07 1.09681142E+00 3.87507025E+01 3.39391443E+02 9.09284222E+01 2.60928866E+03

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,OZ,V	LAT,...	ALPHA,...	REV,...	MCI
4/19/67	0.00000	8.09956508E+07	-2.94728354E+03	-12.17957226	311.64849893	.86253	
17/ R	2468.83333	-9.10722076E+07	3.05296783E+03	-48.35150066	-12.17957226	0.00000	
50.00000	61730.00000	-2.63056484E+07	9.54549037E+02	19582.12025	177.65893199	0.00000	
	.25000	1.24685322E+08	4.34416724E+03	-12.17957226	282.52768331	0.00000	
	58.16398	1.89276533E+01	4.23325212E+01	-6.56148470	-6.51581120		

CLASSICAL ELEMENTS (A,E,I,O,U,TAU)

-1.07267055E+07 1.12438170E+00 1.62595798E+02 2.68132925E+02 1.05503772E+02 2.61038237E+03

*** REQUESTED PRINTS

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,OZ,V	LAT,...	ALPHA,...	REV,...	MCI
4/19/67	0.00000	2.31475398E+07	-6.57546633E+02	-33.78873098	282.90748738	.77972	
17/ R	2468.83333	-1.01006806E+08	3.52403803E+03	-77.09251221	-33.78873098	0.00000	
50.00000	61730.00000	-6.93415183E+07	2.46162612E+03	19582.12025	177.94734153	0.00000	
	.25000	1.24685322E+08	4.34416724E+03	-33.78873098	69.78024625	0.00000	

DATE,...	ME,MM,ST,DT	X,Y,Z,R	OX,OY,OZ,V	LAT,...	ALPHA,...	REV,...	MCI
4/19/67	0.00000	8.09956508E+07	-2.94728354E+03	-12.17957226	311.64849893	.86253	
17/ R	2468.83333	-9.10722076E+07	3.05296783E+03	-48.35150066	-12.17957226	0.00000	
50.00000	61730.00000	-2.63056484E+07	9.54549037E+02	19582.12025	177.65893199	0.00000	
	.25000	1.24685322E+08	4.34416724E+03	-12.17957226	282.52768331	0.00000	
	58.16398	1.89276533E+01	4.23325212E+01	-6.56148470	-6.52038802		

ITEM	DESCRIPTION	REFERENCE SECTION
14	Epoch print in lunar mode in MCI and MF (moon-fixed) coordinate frames (Item 38 of Case A plus one line at the end of the MF output, as in Item 12 of this case). The classical elements in MCI and MF coordinate frames are also shown	

DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	MF
4/20/67	411.83356	5.32324080E+06	-6.08367879E+03	-3.31007435	333.16785725	.94144	+CRASH*
0/ 0	2880.66689	-2.02552741E+06	6.09263787E+03	-20.83214234	-3.31007435	0.00000	
40.01336	40.01336	-3.29409986E+06	1.58840219E+03	.49376	154.94370509	0.00000	
	2.00000	5.7050989E+06	8.75525015E+03	-3.31007435	72.21872601	0.00000	
	67.87118	-1.61428184E+01	1.24793857E+02	5.78130875	175.80364851		

CLASSICAL ELEMENTS (A,E,I,O,U,TAU)

-1.08498492E+07 1.11275053E+00 1.80769519E+01 3.49374042E+02 1.88718229E+02 2.60561349E+03

DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	MC1
4/20/67	412.00000	3.79157606E+06	-2.68559808E+03	-18.70238820	315.36187189	.86771	PRE-EVMT
0/ 0	2880.83333	-3.74408062E+06	7.04557936E+03	-44.63812771	-18.70238820	0.00000	
50.00000	50.00000	-1.80390993E+06	4.55533714E+03	-12.56592	154.62950533	0.00000	
	2.00000	5.62574778E+06	8.81009729E+03	-18.70238820	55.93435572	0.00000	

CLASSICAL ELEMENTS (A,E,I,O,U,TAU)

-1.07774001E+07 1.11430955E+00 3.83112676E+01 3.40732834E+02 8.76630660E+01 2.60846103E+03

DATE,...	ME,MM,ST,DT	X,Y,Z,R	DX,DY,DZ,V	LAT,...	ALPHA,...	REV,...	MF
4/20/67	412.00000	5.26223684E+06	-6.13368611E+03	-3.19484861	339.52754951	.94247	PRE-EVMT
0/ 0	2880.83333	-1.96458627E+06	6.11193076E+03	-20.47235007	-3.19484861	0.00000	
50.00000	50.00000	-3.13531907E+05	1.59145781E+03	-12.56592	154.71321546	0.00000	
	2.00000	5.62574778E+06	8.80400709E+03	-3.19484861	72.20012514	0.00000	
	57.92550	1.74346113E+01	3.03008926E+02	-6.41658430	-6.21646446		

CLASSICAL ELEMENTS (A,E,I,O,U,TAU)

-1.08498490E+07 1.11277339E+00 1.80751758E+01 3.49375107E+02 1.88710806E+02 2.60561375E+03

*** VEHICLE CRASHED

*** END OF TRAJECTORY ***

[illegible]

TRA 66-66 (A0104A)

[illegible]

(02/21/74)


```

MODEL DATA
M1 TRPX MODEL
INFORM1
D 02.000
D J3.000
D J4.000
CRASHJ.
LEMSPJ
ER 1.E-11
END

INTERMS
-1.0827E-3
2.693E-6
1.4E-6
HMIN C.0.390625
GM C.55339362E-2
INPCMP1

MTERMS04,60
0.
0.
0.
H0 0.015525
IPINS 100
DITIN 3

CARD 1
CARD 2
CARD 3
CARD 4
CARD 5
CARD 6
CARD 7
CARD 8
CARD 9
    
```

***** GRAVITY MODEL *****

GM = .5531936200E-02 ER**3/MIN**2 = .1437792019E+17 FT**3/SEC**2 = .3986422981E+15 M**3/SEC**2
 NO NORMALIZATION WITH 3 TERMS.

N	M	CNM	SNM	**	W	P	CNM	SNM
2	-1.7827	0E-02	0.	**	4	C	.1437792019E-05	0.
3	.2693	0E-05	0.	**				

***** GENERAL PERTURBATIONS GRAVITY MODEL *****

GM = .5530+177+4E-02 ER**3/MIN**2 = .1437660055E+17 FT**3/SEC**2 = .3986049304E+15 M**3/SEC**2

***** ZONAL HARMONICS *****

EJ2 = .1032549000E-02 EJ3 = -.2435000000E-05 EJ4 = -.1232000000E-05

***** PHYSICAL CONSTANTS *****

GM(ER**3/MIN**2)	=	.5531936200E-02	DYGE(RAD/MIN)	=	.437526917E-02	GMLAT(DEG)	=	.793000000E+02
GMKM(KM**3/SEC**2)	=	0.	DMEGA(RAD/MIN)	=	.437526917E-02	GMLNG(DEG)	=	.291000000E+02
SGM(ER**3/MIN**2)	=	0.	OMEGA(RAD/MIN)	=	0.	AM(ER)	=	.272516277E+02
ERFT(FT/ER)	=	.69257390E+09	ERKM(KM/ER)	=	.637616490E+04	ERNM(NM/ER)	=	.344393360E+04
FTKM(FT/KM)	=	.328183990E+01	FTNM(FT/NM)	=	.607611559E+03	AE(ER)	=	.100000000E+01
GSUBJ(FT/SEC**2)	=	.321740000E+02	DGREE(DEG)	=	.372957795E+02	SLT(ER/MIN)	=	.292017630E+04
CKEP	=	.1000000E-11	F	=	.335232997E-02	PI	=	.314159265E+01

ITEM	DESCRIPTION	REFERENCE SECTION
1	<p>Card images of the input MODEL data. Emphasis is given to the variates associated with a powered flight run (ITIN = 3), the others having been discussed earlier:</p> <p>NPCMP, PTNS, ER, CRASH</p>	2.1.4


```

***** INPUT/OUTPUT CONVERSION FACTORS *****
OF(I/O-ER) = .21925738E+09 VF(I/O-ER/MIN) = .34876230E+06 AF(I/O-ER/MIN**2) = .58127150E+04

***** INTEGRATION INPUTS *****
I/CENT = 1 NSTEP = 2
IR = 8 ER = .1000000E-10
HMIN = .39062510E-02 HMAX = .64010000E+02 HQ = .15625100E-11

***** SPECIAL OPTIONS *****
TAPE2 = 0 TAPE7 = 0 TELEM = 0 PTAPE = 0 NEDOT = 0
PRHO = 0 NUOPR = 0 CLASS = 0 LEMSP = 0 PTNS = 100

***** CRASH ALTITUDE TABLE *****
(IN FT)
ECI CRASH ALTITUDE = 0. MCI CRASH ALTITUDE = .32000000E+04

***** INTERPLANETARY CRASH ALTITUDES TABLE *****
(IN FT)
BODY(1) CRASH ALTITUDE = .30000000E+05 BODY(2) CRASH ALTITUDE = 0.
BODY(3) CRASH ALTITUDE = .30000000E+05 BODY(4) CRASH ALTITUDE = 0.
BODY(5) CRASH ALTITUDE = 0. BODY(6) CRASH ALTITUDE = 0.
BODY(7) CRASH ALTITUDE = 0.

ENTER SEGMENT 01 AT 12.6 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 12.6 CP SECS.

```

2

ITEM	DESCRIPTION	REFERENCE SECTION
2	Crash altitude table. ECI and MCI crash altitudes at which to stop integrating for the sun and moon, respectively	2.1.3 2.1.4
	Interplanetary crash altitude table. Crash altitudes at which to stop integrating for solar system bodies	2.1.3

ITEM	DESCRIPTION	REFERENCE SECTION
3	<p>Card images of input <u>VEHICLE</u> data. Emphasis is given to the variables associated with a powered flight run (ITIN = 3), the others having been discussed earlier:</p> <p>AL, DL, IØTPF, NPFRP, PFRP, DALPH, KDRAG ALTPR CDAS</p>	<p>11.1.5 11.3.1.2 11.1.8</p>

EPOCH
YR/MC/DAY
TZNE,HR,MIN,SEC
1971/ 1/ 1
C.
0.
0.
0.

X,Y,Z,DX,DY,DZ
-36312964377E+J7
.206E255543E+J4
C.
-15027777375E+J4
-2047036.31E+J3
-13459535244E+J1

INITIAL CONDITIONS
A,B,C,A,R,V
.39993272396E+02
0.
.9010000000E+02
3000000000E+02
.2032573300E+08
.1525928924E+04

A,E,I,O,U,TAU
.10491036770E+08
.99653932592E+09
.50536033438E-12
.27999327240E+03
.3600000000E+03
-14973935691E+02

AF,AG,N,L,CHI,PSI
.17293193251E+00
-98141957265E+00
.20634939238E+02
.99993272396E+02
-47433638210E-14
.76512639055E-15

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

ENTER SEGMENT 02 AT 12.8 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .2 CP SECS.

ENTER SEGMENT 10 AT 12.8 SECONDS. EXECUTION TIME FOR SEGMENT 2 WAS .0 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

IVERP	1	ICENT	1	IDRAG	3	ALPHG	.174521183E+01	CDAM	.800000000E+02
JVEP	0	JNORM	1	IR	9	ALG-DEG	.969932724E+02	ER	.100000000E-10
MVEP	0	MAJOR	0	ISRF	0	TJDATE	.244095250E+07	HMIN	.195312500E-02
KVEP	0	NMASS	0	NEQS	3	TSTART	0.	HMAX	.600000000E+02
LVEP	0	NT	3	RECMP	2	TSTOP	.600000000E+02	HJ	.125000000E+00
ICENTX	1	JNORMX	0	NMASSX	0	FLIGHT	.600000000E+02	NTX	0.
				NASA	0	SSTEP	.100000000E+03	SORC	.100000000E+01
				NRING	0	CPAW	0.	UTD	.350000000E+02
				IFORM	0				

ITEM	DESCRIPTION	REFERENCE SECTION
4	<u>Quantities associated with the current vehicle (Table C-1)</u>	

Table C-1. Definitions of Initialized Integration Quantities

Symbol	Definition	Reference Section
IVEP	Number of C and S parameters (GPRAM)	2.1.5.2
JVEP	Number of other model parameters (\emptyset PRAM)	2.1.5.3
MVEP	Number of mass parameters (MPRAM)	2.1.5.1
KVEP	Number of vehicle-dependent parameters (VPRAM)	11.1.14
LVEP	Number of delayed parameters (i.e., THRUST, DRAG, etc.)	11.1.14
ICENTX	Central force flag for the moon	2.1.2.2
ICENT	Central force flag for the earth	
JNORM	Normalization for the earth gravity model	
MAJOR	Flag for the integration of the variational equations	
MASS	Number of masses in the earth gravity model	2.1.2.2
NT	Number of terms in the earth gravity model	
JNORMX	Normalization for the lunar gravity model	2.1.2.2
IDRAG	Flag indicating the atmospheric model used	11.1.8
IR	Ratio of Runge-Kutta to Cowell step size (H0/IR)	2.1.4
ISRP	Flag for solar radiation pressure	2.1.2.6
NEQS	Total number of equations to be integrated	2.1.4
RECOMP	Flag for recomputation of perturbations	
NMASSX	Number of masses in the lunar gravity model	2.1.4
NASA	Coordinate and timekeeping transformation option flag	

Table C-1. Definitions of Initialized Integration Quantities (Continued)

Symbol	Definition	Reference Section
ALPHG	Right ascension of Greenwich (rad at midnight of epoch day)	
ALC-DEG	Right ascension of Greenwich (deg at midnight of epoch day)	
TJDATE	Julian date of epoch day	
TSTART	Trajectory start time (MME)	
TSTOP	Trajectory stop time (MME)	
FLIGHT	Duration of flight (TSTOP-TSTART, min)	
SSTEP	Number of integration steps specified per rev when the regularized time variable is used	11.1.6
CDAW	Reciprocal of the ballistic coefficient	
ER	Error control in integration ($ER = 1. \cdot 10^{-S}$, where S is the number of significant figures)	2.1.4
HMIN	Minimum absolute step size for integration	2.1.4
HMAX	Maximum absolute step size for integration	2.1.4
H0	Initial integration step size: A negative value indicates backward integration	2.1.4
NTX	Number of terms in the lunar gravity model	2.1.2.2
SORD	Power of the regularization transformation	11.1.6
CPAW	Solar radiation pressure coefficient	11.1.4
UTD	Correction that relates iteration time to ephemeris time, sec	2.1.4

ASSOCIATED QUANTITIES

STAGE	T, ST, SDT	TF, WF, DV, HF, AA AZ	ISP, AS, WD, WD, DRAG BETA	RATES, WR, WP, WY, LIFT, Z, LIFTAL
NO. 1	0.000000	.16666667E+00	.291666667E+03	CONSTANT
	0.000000	0.	.60000000E+04	0.
	10.000000	0.	.40000000E+06	0.
PRIMARY		0.	.24000000E+04	0.
		0.	.80000000E+02	0.
		0.	0.	0.

STAGE	T,ST,SDT	TF,WF,DV,HF,AA	SP,AE,W0,WD,DRAG	RATES,WR,WP,WY,LIFT,ALIFTA
NO. 2	166667 10.000000 1.000000	1.3333333E+00	BETA .291666667E+03 .6000000E+04 .3760000E+06 .2400000E+04 .8000000E+02 0.	CONSTANT 1. -.5000000E+01 0. 0. 0.
SECONDARY				

STAGE	T,ST,SDT	IF,WF,DV,HF,AP	ISP,AE,W0,WD,DRAG	RATES,WR,WP,WY,LIFTZ,LIFTAL
NO. 3	.183333	27751333E+00	BETA	CONSTANT
	11.101030	0.	.291666667E+03	0.
	5.657870	0.	.60000000E+04	0.
		0.	.37363000E+06	0.
		0.	.24000000E+04	0.
		0.	.80000000E+02	0.
SECONDARY		0.	0.	0.

STAGE	T,ST,SOT	TF,MF,OV,HF,AA	ISP,AS,WI,WD,DRAG	FATES,WR,WP,WY,LIFT,Z,LIFTAL
NO. 4	.277513	.181333333E+01	RETA .29166667E+03	GRAVITY TURN 1.
	16.550800	.	.6000000E+04	0.
	93.349230	.	.3600380E+06	0.
		.	.2400000E+04	1.
		.	.8000000E+02	0.
SECONDARY		.	C.	1.

ITEM	DESCRIPTION	REFERENCE SECTION
5	<u>Quantities associated with the predetermined event table (Table C-2)</u>	

Table C-2. Definitions of Predetermined Event Table Quantities

Symbol	Definition	Reference Section
TZERØ	Time to start integration	11.1.15
AL	Right ascension of launch α_L , deg	11.1.15
DL	Declination of launch δ_L , deg	11.1.15
STAGE	Stage number	11.1.15
T	Start time of this stage, minutes from epoch	11.1.15
ST	Start time t , sec	11.1.15
SDT	Δt , sec, where the start time of the next stage is $t + \Delta t$, min	11.1.15
TF	Termination time for this stage, minutes from epoch	
WF	Final weight, lb	11.1.15
DV	Achieved change in velocity during this stage, ft/sec	11.1.15
HF	Cutoff altitude for this stage, ft	11.1.15
AA	Cutoff angle of attack for this stage, deg	11.1.15
AZ	Roll axis azimuth at the start of this stage	11.1.15
ISP	Specific impulse, sec	11.1.15
AE	Exit area, ft ²	11.1.15
W0	Initial vehicle weight for this stage, lb	11.1.15
WD	Weight flow rate, lb/sec	11.1.15
DRAG	Drag reference area, $C_D A$ or A	11.1.15
BETA	Roll axis pitch attitude at the start of this stage	11.1.15

Table C-2. Definitions of Predetermined Event Table Quantities (Continued)

Symbol	Definition	Reference Section
RATES	= CONSTANT; WR, WP, WY are constant throughout this stage	11.1.15
	= GRAVITY TURN; this is a gravity turn stage (Item 11)	
	= FREE FLIGHT; this is a free flight stage (Item 12)	
WR	Roll axis turning rate, deg/sec	11.1.15
WP	Pitch axis turning rate, deg/sec	
WY	Yaw axis turning rate, deg/sec	
LIFTZ	Constant lift reference area coefficient C_{L0A} or A	11.1.15
LIFTAL	Lift slope reference area coefficient $C_{L\alpha A}$ or A	
TSTØP	Time to stop integration (Item 5)	
PRIMARY ^a	Certain primary parameters (ISP, AE, W0, WD, DRAG, LIFTZ, and LIFTAL) are defined for a primary stage and are held constant until the next primary stage is reached	11.1.15
SECONDARY ^b	Secondary parameters (WR, WP, WY, TF, DV, HF, WF, AA, AZ, and BETA) can change at each secondary stage (for secondary stages occurring within a primary stage), while the primary parameters remain constant	11.1.15

^aPrimary parameters define the vehicle configuration.

^bSecondary parameters control maneuvering of the vehicle specified by the primary parameters.

STAGE	T, ST, SDT	TF, WF, DV, HF, AF AZ	ISP, AE, W3, WD, DRAG BETA	RATES, WR, WP, WY, LIFTZ, LIFTAL CONSTANT
NO. 5	1.833333 110.000000 .600000	.184333333E+01	.54000000E+02 .60000000E+04 .13600000E+06 .37570000E+04 .80000000E+02 0.	0. 0. 0. 0. 0.
PRIMARY				
STAGE	T, ST, SDT	TF, WF, DV, HF, AA AZ	ISP, AE, W3, WD, DRAG BETA	RATES, WR, WP, WY, LIFTZ, LIFTAL FREE FLIGHT
NO. 6	1.943333 110.500000 1.000000	.18666667E+01	0. 0. .13374580E+06 0. .80000000E+02 0.	0. 0. 0. 0. 0.
PRIMARY				
STAGE	T, ST, SDT	TF, WF, DV, HF, AA AZ	ISP, AE, W3, WD, DRAG BETA	RATES, WR, WP, WY, LIFTZ, LIFTAL CONSTANT
NO. 7	1.866667 112.000000 135.000000	.41166667E+01	.30000000E+03 .60000000E+04 .11548500E+06 .75000000E+03 .80000000E+02 0.	0. 0. 0. 0. 0.
PRIMARY				
STAGE	T, ST, SDT	TF, WF, DV, HF, AA AZ	ISP, AE, W3, WD, DRAG BETA	RATES, WR, WP, WY, LIFTZ, LIFTAL FREE FLIGHT
NO. 8	4.116667 247.000000 3353.000000	.50000000E+02	0. 0. .10000000E+05 .50000000E+02 0.	0. 0. 0. 0. 0.
PRIMARY				

60.0000 TSTOP

*** TRAJECTORY START
*** POWERED FLIGHT

⑧

*** ENTRY TIME IS 12.89900

TSEC = .000000 T = 0.000000 H = .015625 NSTEP = 0
X, Y, Z X0, Y0, Z0 X00, Y00, Z00
- .363129649775E+07 - .150277773754E+04 - .295181229789E+01
.20608255546E+08 - .264798324310E+03 - .1675210.7208E+02
0. - .13459535204E-10 - .129863715188E-03

} ⑦

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
GEOPOTENTIAL 3.220200E+01 5.588194E+00 -3.171343E+01 -1.298687E-04 -3.220200E+01 1.145514E-18 -1.298687E-04
ATMOSPHERIC 1.529623E-16 1.586416E-16 2.65442E-17 2.159191E-22 1.838109E-22 -1.529623E-16 2.159191E-22
THRUST 4.921208E+01 -9.53997E+00 4.846544E+01 0. 4.921208E+01 -3.979039E-13 -3.231174E-27
TOTAL 1.731009E+01 -2.951812E+00 1.675200E+01 -1.298687E-04 1.701004E+01 -3.979039E-13 -1.298687E-04

REFERENCE SECTION

ITEM	DESCRIPTION
6	<p>Powered flight. This notation indicates that the vehicle is thrusting, i.e., that <u>ISP</u> and <u>WD</u> are nonzero. If <u>ISP</u> and <u>WD</u> are zero, the vehicle's trajectory is controlled by external forces only, i.e., the pull of the earth or the moon. In this case, the vehicle is considered to be in free flight.</p>
7	<p><u>Trajectory print at the beginning of this stage:</u></p> <p style="margin-left: 40px;">TSEC = time from epoch, sec T = time from epoch, min H = integration step size NSTEP = number of integration steps X, Y, Z = vehicle position at time t, ft XD, YD, ZD = vehicle velocity at time t, ft/sec XDD, YDD, ZDD = vehicle acceleration at time t, ft/sec²</p>

STAGE
NO. 1
CONSTANT

T, ST, STAU
0.00000
0.00000
0.00000

H, RHO, MACH, P, VA
-0.74343158E-07
.23768946E-02
.35465123E-08
.14695972E+02
.9535.590E-05

LAT, LONG, R, V, AA
C.
.3600000E+03
.20925738E+08
.15259289E+04
.90000069E+02

ISP, W, CDAM, CLAW
.25492674E+03
.4300000E+05
.4400000E-04
?
?
?
0.

XI, WR, WP, WY
-0.17353254E+00
.98482814E+00
0.
0.
0.
0.

TSEC =

1.000000 T = .166667 H = .015525 NSTEP = 11

X, Y, Z

XD, YD, ZD XCD, YCD, ZCD

-0.364E-05 4873E+17
.20E-06 496957E+18
-0.640979943981E-12

-0.153495603531E+04
-0.81505027405E+02
-0.129721395149E-02

-0.35064446474E+01
.200344323840E+02
-0.12941977535E-03

FORCES

MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 3.219920E+01 5.610725E+00 -3.171659E+01 -1.298305E-04 -3.219921E+01 1.104126E-10 -1.298405E-04

ATMOSPHERIC 5.952140E-02 1.027157E-02 -5.862842E-02 4.124370E-07 -5.952132E-02 1.016091E-04 4.125050E-07

THRUST 5.259766E+01 -9.127405E+00 5.179965E+01 0. 5.259764E+01 -3.835217E-02 -1.629693E-08

TOTAL 2.033896E+01 -3.50604E+00 2.003443E+01 -1.294181E-04 2.033893E+01 -3.825055E-02 -1.294443E-04

STAGE
NO. 1
CONSTANT

T, ST, STAU
.166667
10.00000
10.00000

H, RHO, MACH, P, VA
.90832625E+03
.23143607E-02
.16920852E+00
.14219973E+02
.18720916E+03

LAT, LONG, R, V, AA
-0.17888378E-07
.3600000E+03
.20926646E+08
.15371184E+04
.56033344E-01

ISP, W, CDAM, CLAW
.25611673E+03
.3760000E+05
.45615542E-04
0.
0.
0.
0.

XI, WR, WP, WY
-0.17353254E+00
.98482814E+00
0.
0.
0.
0.

ITEM	DESCRIPTION	REFERENCE SECTION
8	Quantities associated with the powered flight output at the beginning of <u>this stage (Table C-3)</u>	
9	Trajectory print at the end of this stage	Item 7
10	Powered flight output at the end of this stage	Item 8

Table C-3. Definitions of Powered Flight Output Quantities

Symbol	Definition	Reference Section
T	Time from epoch, min	11.1.15
ST	Time from epoch, sec	
STAU	Time from the beginning of this stage, sec	
H	Vehicle altitude, ft	
RHØ	Atmospheric density at altitude h, slug/ft ³	
MACH	Mach number (the ratio of the speed of the body to the speed of sound in the surrounding atmosphere)	
P	Pressure at altitude h, lb/in ²	
VA	Absolute value of the relative velocity vector	
LAT	Vehicle geodetic latitude, deg	
LØNG	Vehicle geodetic longitude, deg	
R	Vehicle geocentric radius, ft	11.1.14
V	Vehicle velocity, ft/sec	11.1.14
AA	Angle of attack, deg	11.1.15
ISP	$(ISP_i \cdot \dot{W} - Ae P(h))/\dot{W}$, where ISP_i (in sec), \dot{W} , and Ae are input quantities for the i^{th} stage and $P(h)$ is computed.	11.1.15
W	Current vehicle weight, lb	11.1.15
CDAW	$C_D A/W$	
CLAW	$(C_{L0} + C_{L\alpha} \cdot \alpha)A/W$, where α is the angle of attack	
XI	Roll axis = $\underline{\xi} = \begin{Bmatrix} \xi_1 \\ \xi_2 \\ \xi_3 \end{Bmatrix}$	11.1.15
WR	Roll axis turning rate, deg/sec	11.1.15
WP	Pitch axis turning rate, deg/sec	11.1.15
WY	Yaw axis turning rate, deg/sec	11.1.15

*** POWERED FLIGHT

 SEG18 ENTRY TIME IS 12.96800
 ***** ECI *****

TSEC = 1.00000 T = .166667 H = .001953 NSTEP = 11
 X,Y,Z XD,YD,ZD XDD,YDD,ZDD

-.364648054873E+07
 .206004966957E+08
 -.648979943981E-02
 -.153495603531E+04
 -.815050274055E+02
 -.129721395149E-02
 -.350641446474E+01
 .20034323840E+02
 -.129418077535E-03

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL I'-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.215920E+01 5.610729E+00 -3.173659E+01 -1.298305E-04 -3.219920E+01 1.104124E-10 -1.298405E-04
 ATMOSPHERIC 5.952149E-02 1.027157E-02 -5.862842E-02 4.124370E-07 -5.952132E-02 1.015091E-04 4.125050E-07
 THRUST 5.259766E+01 -5.127405E+00 5.179965E+01 0. 5.259764E+01 -3.835217E-02 -1.629603E-04
 TOTAL 2.033896E+01 -3.506444E+00 2.003443E+01 -1.294181E-04 2.033893E+01 -3.825056E-02 -1.294443E-04

STAGE T,ST,STAU H,RHO,MACH,P,VA LAT, LONG,R,V,AA ISP,W,CDAM,CLAW XI,WR,WP,WY
 NO. 2 .166667 -.17988378E-07 .25611673E+03 -.17353254E+00
 CONSTANT 10.000000 .23143607E-02 .36000000E+03 .37600000E+06 .98482814E+00
 0.000000 .16827852E+00 .20926646E+08 .45615542E-04 0.
 .14219973E+02 .15371184E+04 0.
 .18720916E+03 .56033344E-01 -.50000000E+01
 0.

NODE T = .17321522E+00
 DT = .19531250E+00
 .364683744089E+07 .206164797969E+08 .620239748153E-03
 -.1535570390157E+04 -.772317138037E+02 .102815667043E+00

TSEC = 11.000000 T = .183333 H = .001953 NSTEP = 20
 X,Y,Z X0,Y0,Z0 X00,Y00,Z00

FORCES
 GEOPOTENTIAL 3.219859E+01 5.612935E+00 -3.170558E+01 -1.310070E-04 -3.219859E+01 -1.96E-07 -1.298381E-04
 ATMOSPHERIC 7.316137E-02 1.261795E-02 -7.205949E-02 -8.109075E-04 -7.315575E-02 1.356065E-04 -8.111105E-04
 THRUST 5.298815E+01 -9.160178E+00 5.193565E+01 4.618222E+00 5.278659E+01 -3.536627E-02 4.618278E+00
 TOTAL 2.112799E+01 -3.534626E+00 2.020800E+01 4.617280E+00 2.051475E+01 -3.523086E-02 4.617338E+00

STAGE
 NO. 2
 CONSTANT

ST, STAU H, RHO, MACH, P, VA LAT, LONG, R, Y, AA ISP, W, CDAM, CLAA XI, WR, WP, WY
 .183333 .11058060E+04 .20937778E-05 .25637126E+03 -.17257220E+00
 1.000000 .23009341E-02 .36000000E+03 .37360000E+05 .98108057E+00
 1.000000 .18683094E+00 .20926844E+08 .45775654E-04 .87155743E-01
 .14119162E+02 .15397068E+04 .0. 0.
 .20779337E+03 .43653501E+01 -.50000000E+01 0.

** POWERED FLIGHT

 SEG18 ENTRY TIME IS 13.03700 ECI *****

TSEC = 11.000000 T = .183333 H = .000244 NSTEP = 20
 X,Y,Z X0,Y0,Z0 X00,Y00,Z00

FORCES
 GEOPOTENTIAL 3.219859E+01 5.612935E+00 -3.170558E+01 -1.310070E-04 -3.219859E+01 -1.96E-07 -1.298381E-04
 ATMOSPHERIC 7.316137E-02 1.261795E-02 -7.205949E-02 -8.109075E-04 -7.315575E-02 1.356065E-04 -8.111105E-04
 THRUST 5.298815E+01 -9.160178E+00 5.193565E+01 4.618222E+00 5.278659E+01 -3.536627E-02 4.618278E+00
 TOTAL 2.112799E+01 -3.534626E+00 2.020800E+01 4.617280E+00 2.051475E+01 -3.523086E-02 4.617338E+00

FORCES
 GEOPOTENTIAL 3.219859E+01 5.612935E+00 -3.170558E+01 -1.310070E-04 -3.219859E+01 -1.96E-07 -1.298381E-04
 ATMOSPHERIC 7.316137E-02 1.261795E-02 -7.205949E-02 -8.109075E-04 -7.315575E-02 1.356065E-04 -8.111105E-04
 THRUST 5.298815E+01 -9.160178E+00 5.193565E+01 4.618222E+00 5.278659E+01 -3.536627E-02 4.618278E+00
 TOTAL 2.112799E+01 -3.534626E+00 2.020800E+01 4.617280E+00 2.051475E+01 -3.523086E-02 4.617338E+00

STAGE	T,ST,STAL	H,RHO,MACH,P,VA	LAT, LONG,R,V,AA	ISP,W,CDAM,CLAW	XI,WR,WP,WY		
NO. 3	.183333	.1105860E+04	.20937778E-05	.25637126E+03	-.17287220E+00		
CONSTANT	11.070000	.23009341E-02	.36000000E+03	.37360900E+05	.98198057E+00		
	C.000000	.1868394E+00	.20926844E+08	.45775654E-04	.87155743E-01		
		.1411316E+02	.15397068E+04	0.	0.		
		.20779307E+03	.43653501E+01	0.	0.		
	STEP DOUBLED	T =	.189681	H =	.003906	NSSTEP =	45
	STEP DOUBLED	T =	.197982	H =	.009977	NSSTEP =	61
	STEP DOUBLED	T =	.214583	H =	.001953	NSSTEP =	77
	STEP DOUBLED	T =	.247786	H =	.003906	NSSTEP =	93

TSEC = 16.650800 T = .277513 H = .003906 NSSTEP = 191

X,Y,Z

XO,YO,ZO

XOO,YOO,ZOO

-.365676933541E+07
 .206064118510E+08
 .885024034732E+02

-.155951933440E+04
 .590891818731E+02
 .289348445908E+02

-.391945831400E+01
 .224672720221E+02
 .48116479747E+01

FORCES	MAGNITUDE	X	Y	Z	(EXTERNAL UNITS)	RADIAL	IN-TRACK	CROSS-TRACK
GEOPOTENTIAL	3.219392E+01	5.625178E+00	-3.169867E+01	-2.663227E-04	-3.219392E+01	-2.470050E-06	-1.302060E-04	
ATMOSPHERIC	1.819448E-01	3.117549E-02	-1.785510E-01	-1.586009E-02	-1.912516E-01	2.010433E-04	-1.586599E-02	
THRUST	5.539249E+01	9.575821E+00	5.434449E+01	4.827774E+00	5.518169E+01	2.458609E-02	4.827942E+00	
TOTAL	2.330864E+01	3.519468E+00	2.246727E+01	4.811647E+00	2.289651E+01	2.478537E-02	4.811946E+00	

STAGE	T,ST,STAL	H,RHO,MACH,P,VA	LAT, LONG,R,V,AA	ISP,W,CDAM,CLAW	XI,WR,WP,WY
NO. 3	.277513	.26210510E+04	.24392663E-03	.25827539E+03	-.17287220E+00
CONSTANT	16.650800	.21998930E-02	.35999999E+03	.35003808E+06	.98198057E+00
	5.65800	.30002963E+00	.20928359E+08	.46660853E-04	.87155743E-01
		.13356512E-02	.15609066E+04	0.	0.
		.33193661E+03	.88776889E-01	0.	0.

*** POWERED FLIGHT

 SEG18 ENTRY TIME IS 13.17100

TSEC = 16.653800 T = .277513 H = .007488 NSTEP = 101
 X,Y,Z X0,Y0,Z0 XCO,YCO,ZCO
 -.765676923541E+J7 -.155951933440E+04 -.391945641149E+01
 .206054128510E+J8 .590891818731E+J2 .224672044732E+02
 .885724034732E+J2 .289348449908E+02 .491243101494E+01

FORCES
 GEOPOTENTIAL 3.219392E+01 5.625178E+00 -3.169867E+01 -2.663727E-04 -3.219392E+01 -2.470050E-06 -1.302068E-04
 ATMOSPHERIC 1.819449E-01 3.117549E-02 -1.785510E-01 -1.588009E-02 -1.912516E-01 2.017433E-04 -1.586599E-02
 THRUST 5.539249E+01 -9.575809E+00 5.434438E+01 4.828557E+00 5.518162E+01 2.460175E-02 4.828726E+01
 TOTAL 2.330873E+01 -3.194566E+00 2.246720E+01 4.812431E+00 2.257644E+01 2.487032E-02 4.812730E+00

STAGE NO. 4
 GRAVITY TURN (11)
 T,ST,STAL H,R40,MACH,P,VA LAT, LONG,R,V,AA ISP,M,COAM,CLAY XI,WR,WP,WY
 .277513 .26210510E+04 .24392863E-03 .25827539E+03 -.17287198E+00
 16.653800 .21993930E-02 .35999999E+03 .36003808E+06 .98107935E+00
 0.007000 .30002963E+00 .20923359E+08 .46660853E-04 .87169895E-01
 .13358512E+02 .15609066E+04 0. 0.
 .33193661E+03 .88773158E-01 -.40254883E+00 0.

* STEP OCCURRED T = .290209 H = .007977 NSTEP = 126
 * STEP OCCURRED T = .306810 H = .001953 NSTEP = 142
 * STEP OCCURRED T = .340013 H = .003906 NSTEP = 158
 * STEP OCCURRED T = .406420 H = .007813 NSTEP = 174

ITEM	DESCRIPTION	REFERENCE SECTION
11	Gravity turn. This notation indicates that the pitch plane is fixed, i.e., that the <u>pitch</u> axis is fixed throughout the stage (the vehicle's body orientation is defined by the roll, pitch, and yaw axes)	

TSEC = 37.041425 T - .617357 H = .007913 NSTEP = 201

X,Y,Z X0,Y0,Z0 X00,Y00,Z00

--.268948050576E+07 --.165353137363E+04 --.523071513431E+01
 .206128555857E+08 .599829537238E+03 .301543083636E+02
 .251071623358E+04 .254268688923E+03 .180934763362E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 3.215672E+01 5.685668E+00 -3.165367E-01 -3.997464E-03 -3.215672E+01 -2.337933E-05 -1.400003E-04
 ATMOSPHERIC 1.865508E+00 3.57639E-01 -1.766205E+00 -5.168669E-01 -1.792509E+00 -7.503355E-02 -5.112762E-01
 THRUST 6.718376E+01 -1.112215E+01 8.357418E+01 1.861434E+01 6.455557E+01 2.892963E+00 1.838115E+01
 TOTAL 3.555301E+01 (1-5.230715E+00 3.015431E+01 1.809348E+01 3.361635E+01 2.817906E+00 1.786973E+01

STAGE T,ST,STAU H,RHO,MACH,P,VA LAT,LCNG,R,V,AA ISP,W,CDAN,CLAM XI,WR,WP,WY

NO. 4 .617357 .14703844E+05 .69159383E-02 .27067544E+03 --.16673889E+00
 GRAVITY TURN 37.041425 .15106449E-02 .35999984E+03 .31110058E+06 .94627297E+00
 20.39 625 .86695869E+00 .20940442E+08 .91145875E-04 .27706606E+00
 .83964901E+01 .17772490E+04 0. 0.
 .91772245E+03 .16490276E+00 --.55408289E+00
 0.

TSEC = 83.916425 T = 1.398607 H = .007913 NSTEP = 301

X,Y,Z X0,Y0,ZD X00,Y00,Z00

-.377394742125E+07
.206811551825E+08
.49311155605E+05
-.198734950895E+04
.252901478822E+04
.21248307985E+04
-.982785276440E+01
.56860152852E+02
.668531214065E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
GEOPOTENTIAL 3.190506E+01 5.727514E+00 -3.138666E+01 -7.520497E-02 -3.190506E+01 -3.003464E-04 -2.128450E-04
ATMOSPHERIC 1.379395E+01 1.861784E+01 -1.389365E+00 -8.254415E-01 -1.107023E+00 -6.641848E-01 -4.858907E-01
THRUST 1.132224E+02 -1.574155E+01 8.933608E+01 6.775377E+01 9.786935E+01 5.473739E+01 3.958199E+01
TOTAL 8.831190E+01 -9.627853E+00 5.686035E+01 6.685312E+01 5.785727E+01 5.41293E+01 3.901509E+01

STAGE T,ST,STAL H,RHO,MACH,P,VA LAT, LONG,R,V,AA ISP,M,COAM,CLAW XI,WR,WP,WY

NO. 4
GRAVITY TURN
1.398607
83.916425
67.265625
.56995094E+05
.38200033E-04
.35906091E+01
.18530648E+00
.35501050E+04
.13529935E+07
.35999780E+03
.21022733E+08
.38549163E+04
.23615894E+00
.29120340E+03
.19860058E+06
.17803128E-03
-.13903212E+00
.7893208E+00
.59841328E+00
0.
-.30602977E+00
0.

STEP DOUBLED T = 1.429857 H = .015625 NSTEP = 304

TSEC = 11.000000 T = 1.833333 M = .015625 NSTEP = 33

X,Y,Z X0,Y0,Z0 X00,Y00,Z00

--.382962956769E+17 --.230522033241E+04 --.152285317936E+02
 .207693535782E+08 .436610387306E+04 .878655526931E+02
 .132011674266E+06 .441316756336E+04 .112924426454E+03

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 3.161173E+01 5.732095E+00 -3.108706E+01 -1.983311E-01 -3.161173E+01 -7.155289E-04 -2.408080E-04
 ATMOSPHERIC 1.096775E-01 1.3432257E-02 -7.891688E-02 -7.497224E-02 -8.051137E-02 -7.022966E-02 -2.479635E-02
 .RUST 1.655963E+02 -2.097406E+01 1.193315E+02 1.131977E+02 1.215666E+02 1.362614E+02 3.677242E+01
 TOTAL 1.438895E+02 -1.522853E+01 8.786555E+01 1.129244E+02 8.987438E+01 1.06195E+02 3.674738E+01

STAGE T,SI,STAU H,RHO,MACH,P,VA LAT, LONG,R,V,AA ISP,W,CDAM,CLAW XI,WR,WP,WY

NO. 4 1.833333 .19414958E+06 .36051912E+01 .29165760E+03 --.12665776E+00
 GRAVITY TURN 110.00.000 .65685542E-06 .35999448E+03 .13600000E+06 .71880538E+00
 93.349200 .61184691E+01 .21119885E+08 .24902211E-07 .68357636E+01
 .36276746E-02 .66221561E+04 0. 0. -0.19060108E+00
 .64560562E+04 .24337381E+09 0. 0.

*** POWERED FLIGHT

 SEG18 ENTRY TIME IS 13.50200
 ***** ECI *****

I SEC = 11.00000 Y = 1.83333 H = .001953 NSTEP = 330

X,Y,Z X0,Y0,Z0 X00,Y00,Z00
 --.382962556769E+17 --.230522033241E+14 --.33283650638E+00
 .207693535792E+18 .436610387306E+04 .33297948901E+01
 .132001167426E+16 .441316756336E+14 .325318098148E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.161173E+01 5.732195E+00 -3.108706E+01 -1.983311E-01 -3.161173E+01 -7.155289E-04 -2.408005E-04
 ATMOSPHERIC 1.096775E-01 1.343257E-02 -7.891688E-02 -7.497224E-02 -8.051137E-02 -7.022966E-02 -2.479635E-02
 THRUST 4.799042E+01 -6.078358E+00 3.449577E+01 3.280511E+01 3.523045E+01 3.079494E+01 1.065678E+01
 TOTAL 3.270347E+01 -3.328307E-01 3.329795E+00 3.253181E+01 3.538208E+00 3.072403E+01 1.063174E+01

STAGE NO. 5
 CONSTANT
 T,ST,STAU 1.83333
 110.00 000
 0.00000
 H,RHO,MACH,P,VA LAT, LONG,R,V,AA ISP,M,CDAM,CLAW XI,WR,WP,WY
 .19414958E+06 .36051912E+00 .53994207E+02 --.12665776E+00
 .65685542E-06 .35999448E+03 .13600000E+06 .71880538E+00
 .61184691E+01 .21119885E+03 .24902211E-03 .68357636E+00
 .36276746E-02 .66221561E+04 0.
 .64560562E+04 .24337381E+00 0.
 0.

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TSEC = 11.500000 T = 1.843333 H = .01953 NSTEP = 336

X,Y,Z X0,Y0,Z0 X00,Y00,Z00
 -.3831 1276599E+07 -.230545103455E+04 -.43673 857491E+04
 .20719738754E+08 .436827993374E+04 .392689255561E+01
 .134654956746E+06 .443285237602E+04 .330972257944E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.160320E+01 5.731847E+00 -3.107044E+01 -2.022339E-01 -3.160320E+01 -7.273982E-04 -2.436814E-01
 ATMOSPHERIC 1.006490E-01 1.229866E-02 -7.229698E-02 -6.894616E-02 -7.375664E-01 -6.460791E-02 -2.271563E-02
 THRUST 4.879982E+01 -6.180376E+00 3.507758E+01 3.335841E+01 3.582877E+01 3.132467E+01 1.779313E+01
 TOTAL 3.332239E+01 -4.367309E-01 3.926883E+00 3.308723E+01 4.151911E+00 3.125926E+01 1.077017E+01

STAGE NO. 5 T,ST,STAL H,RHO,MACH,P,VA LAT,LCNG,R,V,AA ISP,W,COAM,CLAW XI,WR,WP,WY
 1.843333 .19619408E+06 .36771767E+03 .53994927E+02 -.12665776E+00
 CONSTANT 110.600000 .59038429E-06 .35999437E+03 .13374580E+06 .7188538E+00
 .61531690E+01 .21122729E+08 .25306629E-03 .6835636E+00
 .32390035E-02 .66368030E+04 0. 0.
 .64711681E+04 .27092423E+03 0. 0.

*** FREE FLIGHT (12)

 SEG18 ENTRY TIME IS 13.56630

TSEC = 11.60000 T = 1.843333 H = .00244 NSTEP = 336

X,Y,Z X0,Y0,Z0 X00,Y00,Z01
 - .38311276599E+17 - .230545103455E+04 .574414546184E+01
 .207719738754E+18 .436827993374E+04 - .311505933932E+02
 .134674956746E+16 .443285237612E+04 - .27118010601E+09

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.160320E+01 5.731847E+00 -3.107841E+01 -2.022339E-01 -3.150321E+01 -7.27392E-04 -2.436414E-04
 ATMOSPHERIC 1.006490E-01 1.229866E-02 -7.223688E-02 -6.894616E-02 -7.375864E-02 -6.46791E-02 -2.271563E-02
 TOTAL 3.167703E+01 5.744145E+00 -3.115069E+01 -2.711800E-01 -3.167696E+01 -5.533531E-02 -2.295931E-02

STAGE NO. 6
 FREE FLIGHT
 T,ST,STAU H,RHO,MACH,P,VA LAT, LONG,R,V,FA ISP,W,COAM,CLAW XI,WR,WP,MY
 1.843333 .19699478E+06 .36771767E+00 .13374580E+06 - .12665776E+00
 110.871000 .59038429E-06 .35999437E+03 .25376629E-03 .71809539E+00
 C.CC ICC .61531680E+01 .21122729E+19 .25376629E-03 .68357636E+00
 .3239035E-02 .66368030E+14 .27092423E+11
 .64711631E+04 .27092423E+11
 STEP DOUBLED T = 1.849681 H = .007488 NSTEP = 361
 STEP DOUBLED T = 1.857982 H = .0071977 NSTEP = 377

REFERENCE
SECTION

ITEM

DESCRIPTION

- 12 Free flight. This notation indicates that the vehicle is not thrusting; its acceleration is caused by external bodies only. When the vehicle is thrusting, i.e., when ISP and WD are nonzero, it is considered to be in powered flight

TSEC = 112.000000 T = 1.866667 H = .000977 NSTEP = 386

X, Y, Z X0, Y0, Z0 XCD, YCD, ZCD

- .383423476890E+07 - .229741172949E+04 .574073159275E+01
 .207780589512E+08 .432469532185E+04 - .311139471337E+02
 .140863685853E+06 .443247766411E+04 - .264903787812E+00

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 3.158340E+01 5.731280E+00 3.105832E+01 2.113492E-01 3.154343E+01 7.543195E-04 2.527050E-02

ATMOSPHERIC 7.779577E-02 9.451416E-03 5.563053E-02 5.355461E-02 5.677779E-02 5.015867E-02 1.765153E-02

TOTAL 3.164323E+01 5.740732E+00 3.111395E+01 2.649038E-01 3.164013E+01 5.092292E-02 1.790423E-02

STAGE T, ST, STAL H, RHO, MACH, P, VA LAT, LONG, R, V, AA ISP, M, CDAM, CLAY XI, WR, WP, WY

NO. 6 1.866667 .20360331E+06 .38454428E+00 0. - .12665776E+00

FREE FLIGHT 112.000000 .46115832E+06 .35999412E+03 .13374580E+05 .71880538E+00

1.400000 .51815487E+01 .21129338E+08 .25294121E-02 .68357636E+00

.24818540E-02 .66051456E+04 0. 0. 0.

.84388136E+04 .45772102E+00 0. 0. 0.

*** POWERED FLIGHT

 SEG18 ENTRY TIME IS 13.70800

TSEC = 112.00000 T = 1.866667 H = .000122 NSTEP = 386
 X,Y,Z X0,Y0,Z0 A00,Y00,Z00
 -.383423476890E+07
 .207780589512E+08
 .140863685853E+06
 -.229741172949E+04
 .432469532185E+04
 .443247766411E+04
 -.219675022102E+01
 .139324201798E+02
 .425736149216E+02

FORCES
 GEOPOTENTIAL 3.154340E+01 5.731280E+00 -3.105832E+01 -2.113492E-01 -3.153343E+01 -7.503195E-04 -2.527058E-04
 ATMOSPHERIC 9.005705E-02 1.054590E-02 -6.442698E-02 -6.202281E-03 -6.575565E-02 -5.810139E-02 -2.044263E-02
 THRUST 6.268062E+01 -7.538986E+00 +.505516E+01 4.284699E+01 4.603243E+01 4.0322043E+01 1.386341E+01
 TOTAL 4.434920E+01 -2.596760E+00 1.393242E+01 4.257361E+01 1.438323E+01 4.016156E+01 1.384271E+01

STAGE	T,ST,STAU	H,RHO,MACH,P,VA	LAT, LONG,R,V,AA	ISP,W,COAM,CLAY	XI,WR,WP,WY
NO. 7	1.866667	.20360331E+06	.38454428E+00	.29998015E+03	-.12665776E+00
CONSTANT	112.000000	.46115832E-06	.35999412E+03	.11548500E+06	.71880538E+00
	0.000000	.61815497E+01	.21129338E+08	.29293695E-03	.60357636E+00
		.24818540E-02	.66051456E+04	0.	0.
		.64388106E+04	.4577212E+07	0.	0.
STEP	DOUBLED	T = 1.869840	H =	.000244	NSTEP = 411
STEP	DOUBLED	T = 1.873991	H =	.000488	NSTEP = 427
STEP	DOUBLED	T = 1.882292	H =	.000977	NSTEP = 443
STEP	DOUBLED	T = 1.898893	H =	.001953	NSTEP = 459
STEP	DOUBLED	T = 1.932056	H =	.003906	NSTEP = 475

TSEC = 118.503906 T = 1.975965 H = .003976 NSTEP = 486

X,Y,Z

X0,Y0,Z0

X00,Y00,Z00

-.384922502343E+07
 .218764958677E+08
 .170672656257E+06
 -.231285933147E+04
 .442215320756E+04
 .471544839794E+04
 -.255743145381E+01
 .-60586177275E+02
 .444626616191E+02

FORCES
 GEOPOTENTIAL 3.149106E+01 5.728487E+00 -3.095460E+01 -2.548245E-01 -3.14916E+01 -8.87133E-04 -2.789860E-04
 ATMOSPHERIC 3.031712E-02 3.596359E-03 -2.125757E-02 -2.131455E-02 -2.172825E-02 -2.06839E-02 -6.653651E-07
 THRUST 6.544814E+01 -8.289515E+00 4.704447E+01 4.473881E+01 4.312664E+01 4.218989E+01 1.368571E+01
 TOTAL 4.734288E+01 -2.557431E+00 1.605862E+01 4.446266E+01 1.661385E+01 4.215893E+01 1.367877E+01

STAGE NO. 7
 CONSTANT 118.503906
 T,ST,STAU 1.975965
 H,RHO,MACH,P,VA .23451826E+06
 LAT, LONG, R, V, AA .46506004E+00
 ISP, H, CDAM, CLAM .29999490E+03
 XI, WR, WP, WY -.12665776E+00
 .13888424E-06 .35999289E+03 .11060737E+06 .71887538E+00
 .69724422E+01 .21160244E+08 .30164087E-03 .68357636E+00
 .63747380E-03 .6865829E+04 0. 0. 0.
 .67071013E+04 .15741246E+01

* STEP DOUBLED T = 1.998503 H = .007813 NSTEP = 491
 * STEP DOUBLED T = 2.568815 H = .01625 NSTEP = 563
 * STEP DOUBLED T = 2.831315 H = .03250 NSTEP = 582

TSEC = 18.378906 T = 3.006315 H = .031250 NSTEP = 506

X,Y,Z X0,Y0,Z0 X00,Y00,Z00

-.403011248067E+37
 .211276732021E+38
 .562590189677E+36
 -.262491720264E+04
 .631051391112E+04
 .827314231983E+04
 -.861493221308E+01
 .511206184033E+02
 .762791813285E+02

FORCES
 GEOPOTENTIAL 3.047258E+01 5.666731E+00 -2.993037E+01 -7.995558E-01 -3.047258E+01 -2.527709E-03 -4.387555E-04
 ATMOSPHERIC 1.035905E-06 1.055633E-07 -6.427877E-07 -8.054691E-07 -6.729490E-07 -7.738396E-07 -1.504130E-07
 THRUST 1.127579E+02 -1.420166E+01 8.105099E+01 7.707864E+01 8.428078E+01 7.361773E+01 1.383926E+01
 TOTAL 9.222816E+01 -8.614932E+00 5.112162E+01 7.627908E+01 5.390820E+01 7.361520E+01 1.383882E+01

STAGE
 NO. 7
 CONSTANT
 T,ST,STAU 3.006315
 180.378906
 68.378906
 H,RHO,MACH,P,VA
 .58467941E+08
 .12012368E-11
 .12036283E+02
 .32685824E-07
 .10640072E+05
 LAT, LONG, R, V, AA
 .15088004E+01
 .35997403E+03
 .21510369E+08
 .10731154E+05
 .79260581E+01
 ISP, W, CDAM, CLAW
 .37000000E+01
 .64200823E+03
 .47351420E-07
 0.
 0.
 0.
 X,WR,WP,WY
 -.12665776E+00
 -.2280538E+00
 .68357626E+00
 0.
 0.
 0.

TSEC = 247.00000 T = 4.116667 H = .031259 NSTEP = S22

X, Y, Z X0, Y0, Z0 X00, Y00, Z00

-.4209 2756395E+07 -.409508972969E+04 -.58982 216885E+02
 .21146669866E+08 .148220688719E+05 .337494301321E+03
 .13622961196E+07 .101294576360E+05 .345867499614E+03

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 2.8626J7E+01 5.429254E+00 -2.805118E+01 -1.762413E+00 -2.862607E+01 -5.154654E-03 -3.617778E-04
 ATMOSPHERIC 3.040219E-07 3.212708E-07 3.212708E-07 -2.321154E-07 -2.101540E-07 -2.101540E-07 -2.062929E-08
 THRUST 5.085458E+02 -6.441128E+01 3.655455E+02 3.476299E+02 3.917646E+02 3.229610E+02 2.90610E+01
 TOTAL 4.868322E+02 -5.698202E+01 3.374943E+02 3.450675E+02 3.631386E+02 3.229558E+02 2.890574E+01

STAGE NO. 7 CONSTANT

T, ST, STAL 4.116667 H, RHO, MACH, P, VA LAT, LONG, R, V, AA ISP, M, COAM, CLAW XI, WR, WP, WY

247.000000 135.000000 .12666332E+07 .35430573E+01 .31000000E+03 -.12665776E+00
 .15694309E-13 .35992879E+03 .14235007E+05 .71889538E+00
 .26861833E+02 .22192103E+08 .21355813E-02 .68357636E+00
 .7121247E-09 .23772889E+05 0. 0.
 .23745743E+05 .66601955E+01 0. 0.

*** FREE FLIGHT

 SEG18 ENTRY TIME IS 14.19000
 ***** ECI *****

TSEC = 247.00000 T = 4.116667 H = .003906 NSTEP = 622

X,Y,Z
 X0,Y0,Z0
 - .4209 2756395E+07
 .21746669866E+08
 .136229621196E+07
 - .409508972969E+04
 .148220688719E+05
 .181294576360E+05
 .542925433743E+01
 -.280511831564E+02
 -.176241280538E+01
 X00,Y00,Z00

FORCES
 GEOPOTENTIAL 2.862607E+01 5.429254E+00 -2.805118E+01 -1.762413E+00 -2.862607E+01 -5.154654E-03 -3.617778E-04
 ATMOSPHERIC 2.704845E-07 2.158307E-08 -1.723323E-07 -2.065102E-07 -1.869714E-07 -1.945937E-07 -1.835362E-08
 TOTAL 2.862607E+01 5.429254E+00 -2.805118E+01 -1.762413E+00 -2.862607E+01 -5.154654E-03 -3.617778E-04

STAGE NO. 8
 FREE FLIGHT
 T,ST,STAL 4.116667
 247.000000
 0.000000
 H,RHO,MACH,P,VA
 .12666302E+07
 .15694339E-13
 .26861883E+02
 .71212477E-09
 .23745743E+05
 LAT, LONG, R, V, AA
 .35430573E+01
 .35992879E+03
 .22192103E+08
 .23772689E+05
 .66601955E+01
 ISP, H, CDAM, CLAW
 .007613
 .015625
 .031250
 .062500
 .125000
 XI,HR,MP,MY
 -.12665776E+90
 .71885538E+00
 .68357636E+00
 0.
 0.
 0.

STEP DOUBLED
 STEP DOUBLED
 STEP DOUBLED
 STEP DOUBLED
 T = 4.218229
 T = 4.351042
 T = 4.616667
 T = 5.147917
 T = 6.210417
 NSTEP = 647
 NSTEP = 663
 NSTEP = 679
 NSTEP = 695
 NSTEP = 711

ISEC = 455.125000 T = 7.585417 H = .125000 NSTEP = 722
 X,Y,Z X00,Y00,Z00
 -.495277400816E+07
 .2428 6764386E+08
 .507374050676E+07
 -.309059259393E+04
 .976697315619E+04
 .174450958375E+05
 .431202169556E+01
 -.211394267967E+02
 -.44272 917503E+01

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 2.202428E+01 4.312022E+00 -2.113943E+01 -4.427209E+00 -2.202428E+01 -9.645462E-03 -6.098423E-04
 ATMOSPHERIC 1.450350E-11 9.470552E-13 -7.266496E-12 -1.251610E-11 -9.571156E-12 -1.073070E-11 -1.293165E-12
 TOTAL 2.202428E+01 4.312022E+00 -2.113943E+01 -4.427209E+00 -2.202428E+01 -9.645462E-03 -6.098423E-04

STAGE NO. 8
 FREE FLIGHT
 T, ST, STAL H, RHO, MACH, P, VA LAT, LONG, R, V, AA ISP, M, COAM, CLAW XI, WR, WP, WY
 7.585417 .43718419E+07 .11647006E+02 0. 10000000E+02 -.12665776E+00
 455.125000 .11611533E-17 .35963422E+03 .10000000E+02 .71807538E+00
 208.125000 .22867990E+02 .25294744E+08 .19000000E+02 .68357636E+00
 .94622027E-13 .20230593E+05 0. 0.
 .20215166E+05 .16602444E+02 0. 0.

* STEP DOUBLED T = 8.335417 H = .250000 NSTEP = 727
 * STEP DOUBLED T = 16.585417 H = .500000 NSTEP = 759

TSEC = 2895.125000 T = 48.095417 H = .500000 NSTEP = 822

X, Y, Z X0, Y0, Z0 X00, Y00, Z00

- .4032 3077577E+07 .321067992127E+04 .233621780400E+01
 .11471337665E+08 -.156926695027E+05 -.660601992485E+01
 .262898693199E+08 -.343549883446E+04 -.15258368317E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 1.67933E+01 2.336218E+00 -6.606020E+00 -1.525837E+01 -1.679033E+01 -1.06376E-02 -1.807568E-07
 ATMOSPHERIC 2.093489E-14 -5.170835E-15 1.969874E-14 4.394857E-15 1.247432E-14 -1.665074E-14 -1.112176E-15
 TOTAL 1.679033E+01 2.336218E+00 -6.606020E+00 -1.525837E+01 -1.679033E+01 -1.06376E-02 -1.807568E-07

STAGE NO. 8 T, ST, STAU H, RHO, MACH, P, VA LAT, LONG, R, V, AA ISP, M, CDAM, CLAW XI, MR, MP, MW

48.095417 .90701690E+07 .65443395E+02 0. -.12685776E+00
 2885.125000 .25697565E-20 .35742859E+03 .10000000E+05 .71809538E+00
 2638.125000 .18424087E+02 .28937958E+08 .19000000E-02 .58357636E+00
 .25564904E-15 .16382031E+05 0. 0.
 .16286782E+05 .14878560E+03 0. 0.

* STEP HALVED T = 58.116667 H = .031250 NSTEP = 843
 * STEP HALVED T = 58.337370 H = .001953 NSTEP = 851
 * STEP DOUBLED T = 58.383198 H = .003906 NSTEP = 875
 * STEP DOUBLED T = 58.452604 H = .007813 NSTEP = 891

ISEC = 3521.687500 T = 58.694792 H = .007813 NSTEP = 922

X,Y,Z X0,Y0,Z0 X00,Y00,Z00

- .166732935561E+07
 .943211344875E+06
 .207907323820E+08
 -.140043390622E+03
 .396515264094E+03
 -.396445296446E+03
 .341867385106E+01
 -.769078914648E+01
 -.27282308426E+02

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK
 GEOPOTENTIAL 3.219367E+01 2.562390E+00 -1.452622E+00 -3.205563E+01 -3.219067E+01 7.51197E-03 5.882027E-03
 ATMOSPHERIC 7.941473E+00 8.562898E-01 -6.239167E+00 4.773390E+00 4.402453E+00 -6.426181E+00 1.325098E+00
 TOTAL 2.855093E+01 3.418680E+00 -7.690789E+00 -2.728223E+01 -2.778822E+01 -6.413667E+00 1.330980E+00

STAGE T,ST,STAU H,RHO,MACH,P,VA LAT, LONG,R,V,AA ISP,M,COAW,CLAW XI,WR,WP,WY
 NO. 8 58.694792 .22711804E+05 .84768075E+02 0. .1266577E+00
 FREE FLIGHT 3521.687500 .11549419E-02 .35743894E+02 .13900000E+03 .71889538E+00
 3274.687500 .63980809E+00 .20878888E+03 .93751835E-03 .68357636E+00
 .80269508E+01 .57793198E+03 0.
 .65624157E+03 .80313335E+02 0.
 0.

* STEP DOUBLED T = 58.905729 H = .015625 NSTEP = 948

*** CRASH *** ALTITUDE = -73.7 TIME = 59.26510

TSEC = 3555.906250 T = 59.265104 H = .015625 NSTEP = 971

X, Y, Z X0, Y0, Z0 X00, Y00, Z00

-.167028474648E+07
 .952864961547E+06
 .297672681792E+08

-.445051684661E+02
 .469037333572E+02
 -.799623060046E+03

.155285287701E+01
 -.837465445471E+01
 .60656' 861740E+00

FORCES MAGNITUDE X Y Z (EXTERNAL UNITS) RADIAL IN-TRACK CROSS-TRACK

GEOPOTENTIAL 3.226082E+01 2.575318E+00 -1.469169E+00 -3.212428E+01 -3.226081E+01 9.535701E-03 1.316452E-03

ATMOSPHERIC 3.346699E+01 -1.022455E+00 -6.905486E+00 3.273084E+01 3.235781E+01 -6.378252E+00 5.685078E+00

TOTAL 8.538977E+00 1.552863E+00 -8.374654E+00 6.065609E-01 9.699672E-02 -6.368716E+00 5.687195E+00

STAGE T, ST, STAL H, RHO, MACH, P, VA LAT, LONG, R, V, AA ISP, W, COAM, CLAW XI, WR, WP, WY

NO. 8 59.265104 -.73664165E+02 .84744933E+02 0. -.12665776E+00

FREE FLIGHT 3555.906250 .23820223E-02 .35445970E+02 .19000000E+05 .71880538E+00

3398.90250 .73214290E+00 .20856108E+08 .13064915E-02 .68357636E+00

.14735135E+02 .80223295E+03 0. 0.
 .81760725E+03 .12160724E+03 0. 0.

*** VEHICLE CRASHED

*** THIS CASE TOOK 2.008 SECONDS TO INTEGRATE A SPAN OF 59.2651 MINUTES ***

*** FROM 0.000 TO 59.265 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 50 AT 14.9 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 2.0 CP SECS


```
*** TRACE66 EPHemeris OUTPUT KEY ***
```

[illegible]

*** CASE 1

*** STAGE NO. 1 POWERED FLIGHT.

*** EPOCH PRINT

DATE,...	ME,MN,ST,DT,..	X,XD	X,XD - BF	ADBARV	LAT,.. BF	REV,...
71/ 1/ 1	0.0000	-363129650E+07	.209257380E+08	99.99327240	0.00000000	.50000
0/ 0	0.0000	.206082555E+08	-.148686311E-06	0.00000000	360.00000000	0.00000
0.00000	0.0000	0.	0.	90.00000000	-.00000000	0.00000
	.01563	-150277774E+04	-.121001230E-10	90.00000000	0.00000000	0.00000
IT	0.0000	-.264798324E+03	.953505100E-05	.20925738E+08	.00000070	
	0.0000	-.134595352E-10	-.134595352E-10	.15255289E+04	180.00000000	
A =	.10481007E+08	MEAN ANOM =	.18000000E+03	APOGEE =	.34439336E+14	
E =	.99653893E+00	ECCENTRIC =	.18000000E+03	HEIGHT =	-.72759576E-14	
I =	.50538039E-12	TRUE ANOM =	.18000000E+03	PERIGEE =	.59701863E+11	
O =	.27999327E+03	KEPL PER =	.29947727E+02	HEIGHT =	-.34379634E+04	
U =	.36000000E+03	ANOM PER =	.29923367E+02	O-DOT =	-.23468143E+17	
TAU =	-.14973864E+02	NCOL PER =	-.80903654E+04	U-DOT =	.46936206E+07	

*** REQUESTED PRINTS

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,...
71/ 1/ 1	0.0000	.363129650E+07	.209257380E+08	99.99327240	0.00000000	.50000 DSC NODE
0/ 0	0.0000	.206082555E+08	-.148686311E-06	0.00000000	360.00000000	0.00000
0.0000	0.0000	0.	0.	90.00000000	-.00000000	0.00000
	.01563	.150277774E+04	-.121001230E-10	90.00000000	0.00000000	0.00000
IT	0.0000	-.264798324E+03	.953505180E-05	.20925738E+08	.00000914	0.00000
	0.0000	-.134595352E-10	-.134595352E-10	.15255289E+04	180.00000000	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,...
71/ 1/ 1	0.0000	.363129650E+07	.209257380E+08	99.99327240	0.00000000	.50000
0/ 0	0.0000	.206082555E+08	-.148686311E-06	0.00000000	360.00000000	0.00000
0.0000	0.0000	0.	0.	90.00000000	-.00000000	0.00000
	.01563	.150277774E+04	-.121001230E-10	90.00000000	0.00000000	0.00000
IT	0.0000	-.264798324E+03	.953505180E-05	.20925738E+08	.00000914	
	0.0000	-.134595352E-10	-.134595352E-10	.15255289E+04	180.00000000	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,...
71/ 1/ 1	0.0000	.363129650E+07	.209257380E+08	99.99327240	0.00000000	.50000 BETA =90
0/ 0	0.0000	.206082555E+08	-.148686311E-06	0.00000000	360.00000000	0.00000
0.0000	0.0000	0.	0.	90.00000000	-.00000000	0.00000
	.01563	.150277774E+04	-.121001230E-10	90.00000000	0.00000000	0.00000
IT	0.0000	-.264798324E+03	.953505180E-05	.20925738E+08	.00000914	
	0.0000	-.134595352E-10	-.134595352E-10	.15255289E+04	180.00000000	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,...
71/ 1/ 1	0.0000	.363129650E+07	.209257380E+08	99.99327240	0.00000000	.50012 PRE-EVNT
0/ 0	0.0000	.206082555E+08	-.148686311E-06	0.00000000	350.99939712	0.00000
0.0000	0.0000	0.	0.	90.00000000	-.00000000	0.00000
	.01563	.150277774E+04	-.121001230E-10	90.00000000	0.00000000	0.00000
IT	0.0000	-.264798324E+03	.953505180E-05	.20925738E+08	.00000914	
	0.0000	-.134595352E-10	-.129721395E-02	.15371184E+04	170.97909818	

STAGE N02 POWERED FLIGHT

DATE, ... 71/ 1/ 1 0/ 0 10.00000
IT
ME,MM,ST,DT, ...
1.1667
1.1667
1.00000
0.00195
0.00090
0.00000
X, XD
-364648055E+07
-206064967E+06
-648979944E-02
-153455604E+04
-815150274E+02
-129721395E-02
X, XD - BF
-209268438E+08
-105198329E+01
-648979944E-02
-187208831E+03
-319594589E+00
-129721395E-02
ADBARV
100.03505026
-0.00000002
355.99999712
0.14949128
-0.00000012
0.00004871
179.97909915
REV, ...
50012 PST-EVNT
0.00000
0.00000
0.00000

DATE, ... 71/ 1/ 1 0/ 0 9.65268
IT
ME,MM,ST,DT, ...
1.16088
1.16088
9.65268
0.00195
0.00000
0.00000
X, XD
-364594764E+07
-216165262E+06
-380570178E-01
-153374241E+04
-884386592E+02
-275116281E+00
X, XD - BF
-209268438E+08
-94488991E+00
-380570178E-01
-180131102E+03
-297220364E+00
-275116281E+00
ADBARV
100.03359944
-0.00000010
355.99999741
0.13899276
-0.00000010
0.00468976
0.0127042
REV, ...
1.00000 ASC MODE
0.00000
0.00000
0.00000

DATE, ... 71/ 1/ 1 0/ 0 11.00000
IT
ME,MM,ST,DT, ...
1.18333
1.18333
11.00000
0.00195
0.00000
0.00000
X, XD
-364801727E+07
-206064253E+06
-759617574E+00
-153848227E+04
-61313300E+02
-230317253E+01
X, XD - BF
-209268438E+08
-148552410E+01
-759617574E+00
-20779937E+03
-388646428E+00
-230317250E+01
ADBARV
100.03922736
0.00000209
355.99999615
0.18199226
0.00000029
0.08649693
359.99851851
REV, ...
1.00002 PRE-EVNT
0.00000
0.00000
0.00000

STAGE N03 POWERED FLIGHT

DATE, ... 71/ 1/ 1 0/ 0 11.00000
IT
ME,MM,ST,DT, ...
1.18333
1.18333
11.00000
0.00195
0.00000
0.00000
X, XD
-364801727E+07
-206064253E+06
-759617574E+00
-153848227E+04
-61313300E+02
-230317253E+01
X, XD - BF
-209268438E+08
-148552410E+01
-759617574E+00
-20779937E+03
-388646428E+00
-230317250E+01
ADBARV
100.03922736
0.00000209
355.99999615
0.18199226
0.00000029
0.08649693
359.99851851
REV, ...
1.00002 PST-EVNT
0.00000
0.00000
0.00000

DATE, ... 71/ 1/ 1 0/ 0 15.65080
IT
ME,MM,ST,DT, ...
1.27751
1.27751
15.65080
0.00195
0.00000
0.00000
X, XD
-365676934E+07
-206064129E+06
-885024035E+02
-155951933E+04
-59081819E+02
-299248459E+02
X, XD - BF
-209268438E+08
-497880143E+01
-885024035E+02
-330671819E+03
-91579785E+00
-299248459E+02
ADBARV
100.06282704
0.0000024333
355.999998637
0.43136952
0.00024333
1.08678265
359.98721473
REV, ...
1.00008 PRE-EVNT
0.00000
0.00000
0.00000

** STAGE N04 POWERED FLIGHT

DATE,...	ME,MM,ST,DT,...	X,XU	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	.27751	-365676934E+07	.209283591E+08	100.06282704	.00024393	1.00008 PSI-EVNT
0/ 0	.27751	.21664129E+08	-.497880143E+01	.00024229	359.99938637	0.00000
16.65080	16.65080	.89502435E+02	.89502435E+02	77.76944063	.43136952	0.00000
IT	.00049	-.155551933E+04	.330671819E+03	88.91321737	.00024393	0.00000
	.00000	.590891819E+02	-.915797851E+00	.20923359E+08	1.08678265	
	.00000	.299348458E+02	.239348450E+02	.15639766E+04	359.98731403	

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	1.83333	-.382962957E+07	.211194722E+08	100.44733648	.36051912	1.00152 PRE-EVNT
0/ 1	1.83333	.217693536E+08	-.233619817E+04	.35810607	359.9947592	0.00000
50.00000	11.00000	.132001167E+06	.132001167E+06	44.39255546	31.95291160	0.00000
IT	.01563	-.23052233E+04	.471172581E+04	18.60042295	.360-9673	0.00000
	.00000	.36610387E+04	-.652191264E+02	.21119885E+08	71.39995367	
	.00000	.441316756E+04	.441316756E+04	.66221561E+04	359.87395734	

** STAGE N05 POWERED FLIGHT

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	1.83333	-.382962957E+07	.211194722E+08	100.44733648	.36051912	1.00152 PSI-EVNT
0/ 1	1.83333	.207693536E+08	-.203619817E+04	.35810607	359.9947592	0.00000
50.00000	11.00000	.132001167E+06	.132001167E+06	44.39255546	31.95291160	0.00000
IT	.00195	-.23052233E+04	.471172581E+04	18.60042295	.360-9673	0.00000
	.00000	.36610387E+04	-.652191264E+02	.21119885E+08	71.39995367	
	.00000	.441316756E+04	.441316756E+04	.66221561E+04	359.87395734	

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...
71/ 1/ 1	1.84333	-.383101277E+07	.211222999E+08	100.44973745	.36771767	1.00154 PRE-EVNT
0/ 1	1.84333	.207719735E+08	-.207550356E+04	.36525644	359.99477005	0.00000
50.60000	11.60000	.134654957E+06	.134654957E+06	44.39599709	32.4215625	0.00000
IT	.00195	-.23054513E+04	.471396926E+04	18.52105861	.36769451	0.00000
	.00000	.36827993E+04	-.657995004E+02	.21122729E+08	71.47933142	
	.00000	.443285238E+04	.443285238E+04	.66368030E+04	359.87210867	

** STAGE NO8
 FREE FLIGHT

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,....
71/ 1/ 1	4.11667	-420902756E+07	.221502326E+08	100.95404915	3.54305730	1.001010 PS1-EVNT
0/ 4	4.11667	.217466699E+08	-.275284719E+05	3.51947193	355.92879242	0.000000
7.00000	247.10300	.136229621E+07	.136229621E+07	46.33324252	208.46052340	0.000000
	91391	-.19508973E+04	.153296421E+05	4.01471358	3.54159824	0.000000
IT	0.00000	.148326689E+05	-.430311423E+03	.221921035+08	85.3928826	
	0.00000	.181294576E+05	.131294576E+05	.23772689E+05	355.68194109	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,....
71/ 1/ 1	1.00000	-.535725302E+07	.260410757E+08	101.87111104	16.27262178	1.04520
0/10	1.00000	.254566666E+08	-.285898245E+06	16.16941149	355.37039410	0.000000
0.00000	60.00000	.755101321E+07	.755101321E+07	50.30392444	1019.56372963	0.000000
	.25000	-.250593693E+04	.730032520E+04	4.17329854	16.24813785	0.000000
IT	0.00000	.694337280E+04	-.955244985E+03	.271152575+08	86.00253432	
	0.00000	.167316140E+05	.167316140E+05	.18287620E+05	358.20997309	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,....
71/ 1/ 1	20.00000	-.626639555E+07	.276216555E+08	103.10523879	31.01306034	1.08606
0/20	20.00000	.269170814E+08	-.917136080E+06	30.84341104	351.09927732	0.000000
0.00000	120.00000	.165032787E+08	.165032787E+08	65.13077807	1856.80055039	0.000000
	.50000	-.63123950E+03	-.137313681E+04	4.67151321	30.95377740	0.000000
IT	0.00000	-.152293522E+04	-.10535374E+04	.321893655+08	85.98811216	
	0.00000	.129543823E+05	.129543823E+05	.13059101E+05	355.69736548	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,....
71/ 1/ 1	31.00000	-.620301387E+07	.248964075E+08	104.40571346	42.81896468	1.11891
0/30	31.00000	.241491464E+08	-.135186798E+07	42.62707544	356.89190746	0.000000
0.00000	180.00000	.229489003E+08	.229489000E+08	88.80033478	2138.41488247	0.000000
	.50000	.897797859E+03	-.744067525E+04	5.45554743	42.74530274	0.000000
IT	0.00000	-.744407440E+04	-.345639678E+03	.33886733E+08	85.97824063	
	0.00000	.839962769E+04	.839962769E+04	.11252579E+05	353.18151679	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,....
71/ 1/ 1	30.46080	-.617982377E+07	.246872878E+08	104.47423928	43.34255508	1.12037 BETA =90
0/30	30.46080	.239400043E+08	-.136080205E+07	43.15051870	356.84491671	0.000000
27.64828	1827.64828	.231779503E+08	.231779503E+08	89.59999998	2139.05679986	0.000000
	.50000	.869667865E+03	-.768607748E+04	5.50227972	43.26388890	0.000000
IT	0.00000	-.768434860E+04	-.301786151E+03	.33889991E+08	85.50722200	
	0.00000	.816887289E+04	.816887289E+04	.11248823E+05	352.99876142	

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,... BF	REV,...
71/ 1/ 1	40.0000	-532247715E+07	.189215416E+08	106.30196864	54.46367021	1.15147
0/43	4..0000	.18191311E+08	-.122979671E+07	54.28147881	356.28131809	0.00000
0.00000	2400.0000	.263696781E+08	-.263696781E+08	113.01680808	1909.07518547	0.00000
		.212152567E+04	-.123394318E+05	6.88478785	54.39869198	0.00000
	0.0000	-.122645884E+05	.82578879E+03	.32475179E+08	85.97384661	
IT	.09000	.275350575E+04	.275350575E+04	.12747658E+05	350.66392397	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,... BF	REV,...
71/ 1/ 1	51.33000	-.364770982E+07	.102241106E+08	110.89338712	68.49981177	1.19104
0/50	51.00000	.955571695E+07	-.291676494E+06	68.36754050	358.36589204	0.00000
0.00000	3000.0000	.257909635E+08	-.257909635E+08	128.77783877	1132.30783299	0.00000
	.50000	.348247104E+04	-.165352809E+05	16.94809311	68.46658268	0.00000
IT	0.00000	-.164337566E+05	.233391386E+04	.27745113E+08	85.97558601	
	.00000	-.228348324E+04	-.528348324E+04	.17609973E+05	348.14763412	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,... BF	REV,...
71/ 1/ 1	57.73839	-.176316903E+07	.194796138E+07	142.80980743	84.06308754	1.23782
0/57	57.73839	.133784248E+07	.105073019E+07	84.82337916	28.342+1935	0.00000
44.30322	3464.30322	.211408933E+08	.211408933E+08	133.94875247	65.83955548	0.00000
	.50000	.465090148E+04	-.189284286E+05	42.27186987	84.06234386	0.00000
IT	0.00000	-.186539368E+05	.335071274E+04	.21256394E+08	85.97660146	
	0.00000	-.157932975E+05	-.157932975E+05	.24880283E+15	346.132+2812	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,... BF	REV,...
71/ 1/ 1	71.52121	-.512405122E+16	.198675710E+17	104.41408869	40.82340990	1.11341
1/10	71.52121	.195474318E+17	-.355285070E+16	40.63314858	349.86113391	BETA = 90
31.27278	4231.27278	.173189692E+17	.173189692E+17	.00001183	320587.5312570	0.00000
	.03125	-.337717893E+14	.133550268E+15	1.58747422	40.63314858	0.00000
IT	0.00000	.131398287E+15	-.238824198E+14	.26594922E+17	41.77011922	
	.00000	.116418561E+15	.116418560E+15	.17877171E+15	275.96732891	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,... BF	REV,...
71/ 1/ 1	58.49359	-.166539023E+07	.154898731E+07	150.56035928	84.78039672	1.24073
0/58	58.49359	.939917806E+06	.112143772E+07	84.74542953	35.90365360	BETA = 90
29.61531	3509.61531	.257633952E+08	.207933952E+08	89.59999768	4.11932927	0.00000
	.00781	-.18113069E+03	.592691162E+03	219.68206520	84.78035423	0.00000
IT	0.00000	.478851345E+03	-.147758025E+03	.21881146E+08	93.34636740	
	0.00000	-.361831513E+02	-.361831513E+02	.51337591E+03	176.42546380	
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	A0BARV	LAT,... BF	REV,...
71/ 1/ 1	59.26355	-.167028059E+07	.156655643E+07	150.29613526	84.74496754	1.24061
0/59	59.26355	.952860555E+06	.111520467E+07	84.70975662	35.44641190	*CRASH*
15.81307	3555.81307	.207673427E+08	.207673427E+08	170.15115798	-00000000	0.00000
	.01563	-.446501753E+02	.143355999E+03	188.08189942	84.74496659	0.00000
IT	0.00000	-.76852404E+02	-.937581765E+02	.20856181E+08	90.72249595	
	0.00000	-.799678312E+03	-.799678312E+03	.80234215E+03	207.61895725	

DATE,...	ME,MM,ST,OT,...	X,XO	X,XO - BF	A0BARV	LAT,... BF	REV,...
71/ 1/ 1	59.26510	-1.167028475E+07	.156656975E+07	150.29609254	84.74433305	1.24061 PRE-EVNT
0/59	59.26510	.952864962E+06	.111519594E+07	84.70972190	35.44536389	0.00000
15.90625	3555.90625	.207672682E+08	.207672682E+08	170.19291151	-0.1212356	0.00000
	.01563	-4.45151685E+02	.142585416E+03	187.86028726	84.74493222	0.00000
IT	0.00000	.469037336E+02	-.935627250E+02	.20856108E+08	90.72247930	
	0.00000	-.799623060E+03	-.799623060E+03	.80223295E+03	207.61874875	

** VEHICLE CRASHED

DATE,...	ME,MM,ST,OT,...	X,XO	X,XO - BF	A0BARV	LAT,... BF	REV,...
71/ 1/ 1	59.26510	-1.167028475E+07	.156656975E+07	150.29609254	84.74433305	1.24061 PRE-EVNT
0/59	59.26510	.952864962E+06	.111519594E+07	84.70972190	35.44536389	0.00000
15.90625	3555.90625	.207672682E+08	.207672682E+08	170.19291151	-0.1212356	0.00000
	.01563	-4.45151685E+02	.142585416E+03	187.86028726	84.74493222	0.00000
IT	0.00000	.469037336E+02	-.935627250E+02	.20856108E+08	90.72247930	
	0.00000	-.799623060E+03	-.799623060E+03	.80223295E+03	207.61874875	

A =	.10433128E+03	MEAN ANOM =	.184939510E+03	APOGEE =	.34340636E+04
E =	.93997235E+00	ECCENTRIC =	.18246567E+03	HEIGHT =	.15781792E+01
I =	.90722479E+02	TRUE ANOM =	.18000917E+03	PERIGEE =	.47475385E-01
O =	.32246886E+03	KEPL PER =	.29742324E+02	HEIGHT =	-.34324379E+04
U =	.27523168E+03	ANOM PER =	.29790353E+02	U-OOT =	.46957538E+09
TAU =	.43986596E+02	NCOL PER =	.31748549E+08	U-OOT =	-.18605385E+11

*** END OF TRAJECTORY ***

EXIT SEGMENT 50 AT 15.3 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS .4 CP SECS.

TRACE-66 (AD184A)

```

      AA
      AAA
      AA A
      AA AA
      AA AAAAAA
      AAAAAAAAAA
      AAAAAAAAAA
      AA AA
      AA AA
      AA
      VERSION 7.27
      19/31/73

```

THE UNIVERSITY OF CHICAGO

(02/21/74)

MODEL DATA
H SCF MODEL
INFORM1

0	02,0
0	03,0
0	04,0
0	05,0
0	06,0
0	07,0
0	08,0
0	09,0
0	10,0
0	11,0
0	12,0
0	13,0
0	14,0
0	15,0
0	16,0
0	17,0
0	18,0
0	19,0
0	20,0
0	21,0
0	22,0
0	23,0
0	24,0
0	25,0
0	26,0
0	27,0
0	28,0
0	29,0
0	30,0
0	31,0
0	32,0
0	33,0
0	34,0
0	35,0
0	36,0
0	37,0
0	38,0
0	39,0
0	40,0

INTERM41

-1.0827E-3
2.676E-6
1.4E-6
2.8E-8
-3.7E-7
5.93E-7
-7.0E-8
1.537069E-6
1.951856E-6
4.162717E-7
9.20555E-8
-5.344208E-7
9.32884E-8
5.056823E-8
-4.432373E-9
1.168464E-7
4.3475E-8
3.028423E-9
-3.801453E-9
-8.3892E-11
-2.746737E-13
-2.000628E-8
1.097921E-8
-1.158042E-9
-1.424538E-10
3.199373E-12
9.22674E-8
4.56422E-8
5.55012E-9
-2.9678E-10
-2.003164E-11
-3.1557E-11
1.625731E-12
-1.013559E-7
7.74717E-9
-5.548191E-10
-8.95364E-11
1.458971E-11

INTERMS04, 60

0.
0.
0.
0.
0.
0.
0.
0.
-7.73576E-7
2.309483E-7
-2.318633E-7
1.36433E-7
-4.181365E-7
9.90846E-8
4.23345E-10
4.033772E-9
-1.42087E-7
-5.45143E-8
3.45103E-9
-2.025287E-9
-1.648367E-9
7.8695E-8
-1.927374E-8
1.057274E-9
-1.922802E-9
-4.115213E-10
-5.391516E-11
6.81522E-8
6.000909E-9
-2.905979E-9
-2.030027E-15
-6.59091E-11
5.2549E-11
-2.675614E-12
-3.29912E-8
-3.09899E-9
2.184649E-9
4.924497E-11
-3.107689E-13

CARD	1
CARD	2
CARD	3
CARD	4
CARD	5
CARD	6
CARD	7
CARD	8
CARD	9
CARD	10
CARD	11
CARD	12
CARD	13
CARD	14
CARD	15
CARD	16
CARD	17
CARD	18
CARD	19
CARD	20
CARD	21
CARD	22
CARD	23
CARD	24
CARD	25
CARD	26
CARD	27
CARD	28
CARD	29
CARD	30
CARD	31
CARD	32
CARD	33
CARD	34
CARD	35
CARD	36
CARD	37
CARD	38
CARD	39
CARD	40

①
CONT'D

ITEM	DESCRIPTION	REFERENCE SECTION
1	<p>Card images of the input <u>MODEL</u> data. Emphasis is given to the variables associated with an SLS run (MULTV=2), the others having been discussed earlier:</p> <p>MULTV, LPACK PANDR, PATA, GPLØT, SSPR, MVET ELEDD, KEDIT, FEDIT, NEDIT JSGLS GMKM, ERKM, F, ØMEGE, ØMEGA, GSUBØ, FTNM, FTKM, SLT, PI, DGREE MSGLS, FREQ, CNTI, ISGLS, PSGLS D1, D2 CLASS LGT UTD, LEMSP ACØN, RCØN</p>	<p>2.2.11 2.2.11.1 2.2.11.3 2.2.11.4 2.1.1 2.2.9 2.1.2.4.1 2.2.1 2.2.5 2.1.4 2.2.2</p>

0 08.06
 0 08.07
 0 08.08
 0 08.09
 0 08.10
 0 08.11
 0 08.12
 0 08.13
 0 08.14
 0 08.15
 0 08.16
 0 08.17
 0 08.18
 0 08.19
 0 08.20
 0 08.21
 0 08.22
 0 08.23
 0 08.24
 0 08.25
 0 08.26
 0 08.27
 0 08.28
 0 08.29
 0 08.30
 0 08.31
 0 08.32
 0 08.33
 0 08.34
 0 08.35
 0 08.36
 0 08.37
 0 08.38
 0 08.39
 0 08.40
 0 08.41
 0 08.42
 0 08.43
 0 08.44
 0 08.45
 0 08.46
 0 08.47
 0 08.48
 0 08.49
 0 08.50
 0 08.51
 0 08.52
 0 08.53
 0 08.54
 0 08.55
 0 08.56
 0 08.57
 0 08.58
 0 08.59
 0 08.60
 0 08.61
 0 08.62

1.058450E-11
 -3.505277E-13
 1.202444E-13
 .3352991869E-2
 GSUB0.3208766404E+2
 SLT 2620.105179
 1.047197551216
 CNT1 1040754.
 IPSGLS2
 ILGT -1
 RCON 1.E-3
 DITIN 2
 LEMS+3
 FLUX 0.
 IKSIG 1
 14 37
 3 0
 ELED00
 KEDIT.5

-6.224239E-13
 0.65730E-13
 -1.058297E-13
 ERKM -6378.145
 OMEGA.4375269088E-2
 FTKM 3280.839895
 DGRE57.295779512
 FREQ 1.779736E9
 IJSGLS6
 CLASS1
 ACON 0.
 PATA 3
 DOP30X4001
 02 -15.738
 DSSPR XX
 13 10
 3 3
 2 0
 ILPACK1
 FEOTIS

0 08.06
 0 08.07
 0 08.08
 0 08.09
 0 08.10
 0 08.11
 0 08.12
 0 08.13
 0 08.14
 0 08.15
 0 08.16
 0 08.17
 0 08.18
 0 08.19
 0 08.20
 0 08.21
 0 08.22
 0 08.23
 0 08.24
 0 08.25
 0 08.26
 0 08.27
 0 08.28
 0 08.29
 0 08.30
 0 08.31
 0 08.32
 0 08.33
 0 08.34
 0 08.35
 0 08.36
 0 08.37
 0 08.38
 0 08.39
 0 08.40
 0 08.41
 0 08.42
 0 08.43
 0 08.44
 0 08.45
 0 08.46
 0 08.47
 0 08.48
 0 08.49
 0 08.50
 0 08.51
 0 08.52
 0 08.53
 0 08.54
 0 08.55
 0 08.56
 0 08.57
 0 08.58
 0 08.59
 0 08.60
 0 08.61
 0 08.62

***** GRAVITY MODEL *****

GM = .5530417752E-02 ER**3/MIN**2 = .1407646853E+17 FT**3/SEC**2 = .390601200E+15 M**3/SEC**2

NO NORMALIZATION WITH 41 TERMS.

N	M	CM	SNM	**	N	M	CM	SNM
2	0	-.108270E-02	0.	**	4	3	.50568230E-07	.42338450E-09
3	0	.267600E-05	0.	**	5	3	.30204230E-08	.34510300E-00
4	0	.140003E-05	0.	**	6	3	.10979210E-07	.10572740E-00
5	0	.280000E-07	0.	**	7	3	.55550120E-08	-.29059790E-00
6	0	-.370000E-06	0.	**	8	3	-.55491810E-09	.21046490E-00
7	0	.593000E-06	0.	**	4	4	-.4323730E-08	.40337720E-00
8	0	-.700000E-07	0.	**	5	4	-.3014530E-08	-.20252070E-00
3	1	.19918560E-05	.23094831E-06	**	6	4	-.1150420E-08	-.19228020E-00
4	1	-.5344200E-06	-.41813650E-06	**	7	4	-.29178000E-09	-.20300270E-14
5	1	.11684640E-06	-.14240870E-06	**	8	4	-.89537400E-10	.49244970E-10
6	1	-.2746237E-12	.7869500E-07	**	5	5	-.83992000E-10	-.16433670E-00
7	1	.9220740E-07	.68152200E-07	**	6	5	-.14245380E-09	-.41152130E-09
8	1	-.1013590E-06	-.3299120E-07	**	7	5	-.20031640E-10	-.65909100E-10
2	2	.15370680E-05	-.77367600E-06	**	8	5	.14589710E-10	-.3102690E-12
3	2	.4162717E-06	-.23186330E-06	**	6	6	.31993730E-11	-.53915160E-10
4	2	.9320840E-07	.9904660E-07	**	7	6	-.31557700E-10	.72599000E-10
5	2	.437501E-07	-.5451433E-07	**	8	6	-.62242390E-12	.18584500E-10
6	2	-.2000620E-07	-.1927374E-07	**	7	7	.16257310E-11	-.76756140E-11
7	2	.4564422E-07	.6000919E-08	**	8	7	.86573800E-12	-.35052770E-12
8	2	.774717E-08	-.3099990E-08	**	0	8	-.18582970E-12	.12024440E-12
3	3	.9205550E-07	.1364030E-06	**				

***** GENERAL PERTURBATIONS GRAVITY MODEL *****
 GM = .553041774E-32 ER**3/MIN**2 = .1407646851E+17 FT**3/SEC**2 = .3986011994E+15 M**3/SEC**2

*** ZONAL HARMONICS ***

EJ2 = .1082549000E-02 EJ3 = -.2435000000E-05 EJ4 = -.1232000000E-05

***** PHYSICAL CONSTANTS *****
 GM(ER**3/MIN**2) = .553041775E-02 OMEGA(RAD/MIN) = .437526909E-02 GMLAT(DEG) = .783000000E+02
 GMK(M(KM**2/SEC**2)) = .398601200E+06 OMEGA(RAD/MIN) = .437526909E-02 GMLNG(DEG) = .291000000E+03
 SGM(ER**3/MIN**2) = .680232650E-04 OMEGL(RAD/MIN) = 0. AM(ER) = .272506277E+00
 ERFT(FT/ER) = .209256726E+08 ERKM(KM/ER) = .637014500E+04 ERNM(NM/ER) = .344392279E+04
 FTKM(FT/KM) = .328063589E+04 FTNM(FT/NM) = .607611549E+04 AE(ER) = .100000000E+01
 GSUB0(FT/SEC**2) = .32876640E+02 DGREE(DEG) = .572557795E+02 SLT(ER/MIN) = .282018318E+04
 CKEP = .10000000E-10 F = .335289187E-02 PI = .314159265E+01

***** INPUT/OUTPUT CONVERSION FACTORS *****
 DF(I/O-ER) = .20925673E+08 VF(I/O-ER/MIN) = .34076121E+06 AF(I/O-ER/MIN**2) = .58126868E+04

***** INTEGRATION INPUTS *****
 NPCHP = 0 ICENT = 1 NSTEP = 2
 HMIN = .15625000E-01 IR = 8 ER = .10000000E-09
 HMAX = .64000000E+02 H0 = .10000000E+01

***** SPECIAL OPTIONS *****
 TAPE2 = 0 TAPE7 = 0 TELEM = 0 PTAPE = 0 NPDOT = 0
 PRMD = 0 NODPR = 0 CLASS = 1 LEMSP = 3 PTNS = 1010"

***** CRASH ALTITUDE TABLE *****
 (IN FT)

ECI CRASH ALTITUDE = .300000000E+06 MCI CRASH ALTITUDE = .300000000E+04

***** INTERPLANETARY CRASH ALTITUDES TABLE *****
 (IN FT)

BODY(1) CRASH ALTITUDE = .300000000E+06 BODY(2) CRASH ALTITUDE = 0.
 BODY(3) CRASH ALTITUDE = .300000000E+04 BODY(4) CRASH ALTITUDE = 0.
 BODY(5) CRASH ALTITUDE = 0 BODY(6) CRASH ALTITUDE = 0.
 BODY(7) CRASH ALTITUDE = 0.

***** STATION LOCATIONS *****
 STATION SIG REF RA-RBF DATUM TYPE LATITUDE X LONGITUDE Y HEIGHT Z P Q
 313 -0 -0 -0 -0 -0 -0 -0 -0
 343 -0 -0 -0 -0 -0 -0 -0 -0
 353 -0 -0 -0 -0 -0 -0 -0 -0
 363 -0 -0 -0 -0 -0 -0 -0 -0
 377 -0 -0 -0 -0 -0 -0 -0 -0
 393 -0 -0 -0 -0 -0 -0 -0 -0
 ***** ATA INPUT *****

 AT4 6.64827257E+4 2 1.68260013E+4 3 4.72859549E+4 CARD 1
 4 5.61307652E+4 5 5.46561358E+3 6 5.75322855E+4 CARD 2
 7 1.41434853E+2 8 4.24344483E+1 9 1.11908631E+2 CARD 3
 10 3.04659113E-1 11 3.45640484E+1 12 6.18612704E+1 CARD 4
 13 2.05906071E+1 14 7.94214544E-2 15 8.79832056E-2 CARD 5
 16 6.77190160E+1 17 4.31726187 18 6.12078389E+1 CARD 6
 19 1.42139627E-1 20 1.78260973E-2 21 7.63605610E-2 CARD 7
 22 -4.67529268E-2 23 -1.03299161E-2 24 -2.65828841E-2 CARD 8
 25 -9.57123720E-5 26 -2.29471783E-5 27 -2.82007265E-5 CARD 9
 28 2.69009967E-7 28 CARD 10
 END CARD 11

ITEM	DESCRIPTION	REFERENCE SECTION
2	<u>Printout of the station locations as input.</u> If CLASS# 0, the actual locations are left blank	4
3	<u>Card images of the input $A^T A$ matrix data.</u> In this case, $(A^T A)^{-1}$ is input because $\Phi P B \Phi X(A)=4$	6

***** DEMO INPUT *****

MDMT 0
ADMT 2
SDRG .0355
PSISD28.CE-5
KORS .3017
END

PIYP 1
SDCG .0346
DPH 5.0
KOTS .3017

OSDEWTVES
FERI 89.5
PRES00
KOCs .3017

CARD 1
CARD 2
CARD 3
CARD 4
CARD 5
CARD 6

ENTER SEGMENT 01 AT 1.5 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS 1.5 CP SECS.

***** VEHICLE DATA FOR CASE 1 *****

MVPRAM04,6-

0 X

0 Y

0 Z

0 DX

0 DY

0 DZ

0 DRAG

IIDRAG1

START1970

4 0

4 12

IVEHID6820

IOAY 26

MIN 1

IC 270.7883984

4 198.847449630

FTIN 0.

4 7.

INPKCK1

3 -.15717854

ONODE20.

4 48611.259

7 64809.871

10 80953.858

13 10693.093

16 26827.276

19 42956.330

22 59080.318

END

20.

20.

20.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

1.

CARD 1

CARD 2

CARD 3

CARD 4

CARD 5

CARD 6

CARD 7

CARD 8

CARD 9

CARD 10

CARD 11

CARD 12

CARD 13

CARD 14

CARD 15

CARD 16

CARD 17

CARD 18

CARD 19

CARD 20

CARD 21

CARD 22

CARD 23

CARD 24

CARD 25

CARD 26

CARD 27

CARD 28

CARD 29

CARD 30

ITEM	DESCRIPTION	REFERENCE SECTION
4	Card images of the deweighting inputs	7
5	Card images of the input VEHICLE data. Emphasis is on the variables <u>associated with an SLS run (MULTV=2)</u> , the others having been discussed earlier: START NCDRAW NPKCK, PKCK DNØDE	11.2.2 11.1.9 11.1.11 11.2.3

EPOCH
YR/MO/DAY
TZNE,HR,MIN,SEC
1970/ 6/26
0.
.12000000000E+02
.10000000000E+01
.17165020000E+02

INITIAL CONDITIONS
A,D,B,A,R,V
.53370435033E+01
-.55147600000E-03
.88946165659E+02
.19884744963E+03
.21561464324E+08
.25690559481E+05

A,E,I,O,U,TAU
.21400276170E+08
.21406144937E-01
.10284744963E+03
.18530723175E+03
.11572153345E+03
.70477056628E+03

AF,AG,N,L,CHI,PSI
.12286662127E-01
-.17528721006E-01
.66784616507E-01
.31944959249E+01
-.12931050634E+00
-.13929146541E+01

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

THESE ARE THE 13 PARAMETERS IN THE PARAM MATRIX. 7 ARE P PARAMETERS AND 6 ARE Q PARAMETERS

NAME	P/Q	CURRENT VALUE	BOUND	SIGMA	CONVERSION
6820 X	P	.214690338E+08	.20000000E+02	0.	.20925673E+08
6820 Y	P	.19942844E+07	.20000000E+02	0.	.20925673E+08
6820 Z	P	-.20753065E+03	.20000000E+02	0.	.20925673E+08
6820 DX	P	.12377378E+04	.10000000E+01	0.	.34876121E+06
6820 OY	P	-.82186686E+04	.10000000E+01	0.	.34876121E+06
6820 DZ	P	-.24308976E+05	.10000000E+01	0.	.34876121E+06
6820 ORAG	P	.92174627E-02	.10000000E+00	0.	.10000000E+01
393 RBIA	Q	.12000000E+04	.10000000E+05	.50000000E+02	.20925673E+08
377 RBIA	Q	.14000000E+04	.10000000E+05	.50000000E+02	.20925673E+08
363 RBIA	Q	.12000000E+04	.10000000E+05	.50000000E+02	.20925673E+08
353 RBIA	Q	.12000000E+04	.10000000E+05	.50000000E+02	.20925673E+08
343 RBIA	Q	.14000000E+04	.10000000E+05	.50000000E+02	.20925673E+08
313 RBIA	Q	.12000000E+04	.10000000E+05	.50000000E+02	.20925673E+08

ENTER SEGMENT 02 AT 1.6 SECONDS. EXECUTION TIME FOR SEGMENT 1 WAS .1 CP SECS.

** DATA STAGING INPUT **

LS/F	NDELTA	DELTA	T	D	YR	MO	DY	TSTART			SEC	YR	MO	DY	HR	MN	SEC	TUPDATE			SEC		
								HR	MO	DY								HR	MO	DY		HR	MO
-0.	-0.	-0.000	1	0	3	0	0	0	0	0.0000	0	0	0	0	0	0	0.0000	70	6	26	13	31	0.0000
-0.	-0.	-0.000	0	0	0	0	0	0	0	0.0000	0	0	0	0	0	0	0.0000	70	6	26	14	39	0.0000
-0.	-0.	-0.000	1	0	0	0	0	0	0	0.0000	0	0	0	0	0	0	0.0000	70	6	26	15	0	0.0000
-0.	-0.	-0.000	1	0	0	0	0	0	0	0.0000	0	0	0	0	0	0	0.0000	70	6	26	16	30	0.0000
-0.	-0.	-0.000	0	0	0	0	0	0	0	0.0000	0	0	0	0	0	0	0.0000	70	6	26	17	43	0.0000
-0.	-0.	-0.000	1	0	0	0	0	0	0	0.0000	0	0	0	0	0	0	0.0000	70	6	26	18	0	0.0000

** OBSERVATIONS FOR CASE 1 **

** STAGE 1 **
 ** STAGE 2 **
 ** STAGE 3 **

STAPASS	YR	MO	DY	HR	MN	SECONDS	T	C	FIELD 1			FIELD 2			FIELD 3			HJD	ST	VEHID	MESSAGE
									1	2	3	1	2	3	1	2	3				
393	16	70	6	26	14	39	20.0000	1	0	0	1.11338000E+02	1.11338000E+02	4.07000000E+00	40763	52760.000	6820					
393	16	70	6	26	14	39	20.0000	0	0	0	1.66357133E+04	0	0	40763	52760.000	6820					
393	16	70	6	26	14	39	36.0000	1	0	0	1.17219000E+02	1.17219000E+02	5.00400000E+00	40763	52776.000	6820					
393	16	70	6	26	14	39	36.0000	0	0	0	1.46059925E+04	0	0	40763	52776.000	6820					
393	16	70	6	26	14	40	28.0000	1	0	0	2.65523622E+06	1.42646000E+02	7.14700000E+00	40763	52828.000	6820					
393	16	70	6	26	14	40	28.0000	0	0	0	4.42319886E+03	0	0	40763	52828.000	6820					
393	16	70	6	26	14	41	12.0000	1	0	0	2.71175853E+06	1.67016000E+02	6.69300000E+00	40763	52972.000	6820					
393	16	70	6	26	14	41	12.0000	0	0	0	6.51818603E+03	0	0	40763	52972.000	6820					
393	16	70	6	26	14	41	24.0000	1	0	0	2.90812864E+06	1.74087000E+02	6.17200000E+00	40763	52984.000	6820					
393	16	70	6	26	14	41	24.0000	0	0	0	9.16173820E+03	0	0	40763	52984.000	6820					
313	16	70	6	26	14	51	12.0000	1	0	0	1.54888790E+06	5.20920000E+01	1.51500000E+01	40763	53472.000	6820					
313	16	70	6	26	14	51	12.0000	0	0	0	2.20899318E+04	0	0	40763	53472.000	6820					
313	16	70	6	26	14	51	44.0000	1	0	0	9.57660763E+05	8.00630000E+01	2.76470000E+01	40763	53504.000	6820					
313	16	70	6	26	14	51	44.0000	0	0	0	1.31763271E+04	0	0	40763	53504.000	6820					
313	16	70	6	26	14	52	40.0000	1	0	0	1.29941929E+06	1.69412000E+02	1.96350000E+01	40763	53560.000	6820					
313	16	70	6	26	14	52	40.0000	0	0	0	1.9833706E+04	0	0	40763	53560.000	6820					
313	16	70	6	26	14	53	4.0000	1	0	0	1.82430118E+06	1.81266000E+02	1.27740000E+01	40763	53584.000	6820					
313	16	70	6	26	14	53	4.0000	0	0	0	2.31371122E+04	0	0	40763	53584.000	6820					
313	16	70	6	26	14	54	4.0000	1	0	0	3.29320539E+06	1.92343000E+02	4.29900000E+00	40763	53644.000	6820					
313	16	70	6	26	14	54	4.0000	0	0	0	2.51645637E+04	0	0	40763	53644.000	6820					

CONT'D

ITEM	DESCRIPTION	REFERENCE SECTION
6	Printout of the input STAGE data LS/F = M	14
7	Observations. The observation printout is fully explained in <u>Case B, Item 3</u>	11.2.1 15 11.1.2

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7

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** STAGE 4 **
STAPASS YR MO DY HR MN SECONDS T C FIELD 1 FIELD 2 FIELD 3 ST VEHID MESSAGE
393 17 70 6 26 16 7 20.0000 1 0 0 1.15749000E+02 1.67500000E+00
393 17 70 6 26 16 7 20.0000 1 0 0 1.13349341E+04 0.
393 17 70 6 26 16 8 4.0000 1 0 2.78503609E+06 1.29323000E+02 7.10300000E+00
393 17 70 6 26 16 8 4.0000 1 0 1.74967044E+04 0.
393 17 70 6 26 16 8 28.0000 1 0 2.41137139E+06 1.40589000E+02 5.15200000E+00
393 17 70 6 26 16 8 28.0000 1 0 1.36219328E+04 0.
393 17 70 6 26 16 9 0.0000 1 0 2.10335958E+06 1.60903000E+02 1.11460000E+01
393 17 70 6 26 16 9 0.0000 1 0 5.46453380E+03 0.
393 17 70 6 26 16 10 4.0000 1 0 2.40362008E+06 2.05002000E+02 6.68500000E+00
393 17 70 6 26 16 10 4.0000 1 0 1.31430709E+04 0.

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** STAGE 5 **
STAPASS YR MO DY HR MN SECONDS T C FIELD 1 FIELD 2 FIELD 3 ST VEHID MESSAGE
343 18 70 6 26 17 44 20.0000 1 0 2.72901903E+06 6.66380000E+01 5.88300000E+00
343 18 70 6 26 17 44 20.0000 1 0 2.1676518E+04 0.
343 18 70 6 26 17 44 40.0000 1 0 2.33840223E+06 7.44520000E+01 7.92400000E+00
343 18 70 6 26 17 44 40.0000 1 0 1.83778783E+04 0.
343 18 70 6 26 17 45 56.0000 1 0 1.70083990E+06 1.32517000E+02 1.27960000E+01
343 18 70 6 26 17 45 56.0000 1 0 4.32450460E+03 0.
343 18 70 6 26 17 46 36.0000 1 0 2.16558399E+06 1.61521000E+02 8.87400000E+00
343 18 70 6 26 17 46 36.0000 1 0 1.64988081E+04 0.
343 18 70 6 26 17 47 32.0000 1 0 3.20381890E+06 1.81541000E+02 3.41400000E+00
343 18 70 6 26 17 47 32.0000 1 0 2.23990942E+04 0.

```


ENTER SEGMENT 10 AT 1.7 SECONDS. EXECUTION TIME FOR SEGMENT 2 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME(MME) TYPE ASSOCIATED QUANTITIES
721.2864 TZERO
1000.0000 TSTOP

*** TRAJECTORY STAFF

```

*****
* PREDETERMINED EVENT TABLE *
*****
*** TRAJECTORY STAFF
*****
SEG11 ENTRY TIME IS 1.76800
* STEP DOUBLED
* STEP DOUBLED
* NODE T = .767215124957E+03 T = 725.161417 H = .250000 NSTEP = 30
* NODE DT = .50301000000E+00 T = 729.411417 H = .500000 NSTEP = 46
* NODE T = .811021379897E+03 T = 729.957797174E+03 H = -.206721431610E+07 -.596669999758E-02
* NODE DT = .50000000000E+00 T = 730.4626327053E+03 H = -.814209479171E+04 -.238278350350E+05
* NODE T = .356943296633E+03 T = 730.9126203942993E+03 H = -.213361809193E+07 -.15672048110E-02
* NODE DT = .50000000000E+00 T = 731.4196203942993E+03 H = -.821494114192E+04 -.243083525139E+05
* NODE T = .903745995142E+03 T = 731.9196203942993E+03 H = -.213361809193E+07 -.105460622573E-02
* NODE DT = .50000000000E+00 T = 732.4196203942993E+03 H = -.814209479171E+04 -.238298363451E+05
* NODE T = .903745995142E+03 T = 732.9196203942993E+03 H = -.213361809193E+07 -.102826795647E-01
* NODE DT = .50000000000E+00 T = 733.4196203942993E+03 H = -.821494114192E+04 -.243076958174E+05
* STEP DOUBLED
* STEP DOUBLED
* NODE T = .946662334323E+03 T = 733.9196203942993E+03 H = -.220038223137E+07 -.920682420941E-02
* NODE DT = .10300000000E+01 T = 734.4196203942993E+03 H = -.814209479171E+04 -.238319337227E+05
* NODE T = .990460717663E+03 T = 734.9196203942993E+03 H = -.219336484338E+07 -.183453992340E+00
* NODE DT = .10000000000E+01 T = 735.4196203942993E+03 H = -.820236695990E+04 -.243069111568E+05
*****

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*** TRAJECTORY TERMINATION

*** THIS CASE TOOK 1.404 SECONDS TO INTEGRATE A SPAN OF 279.6250 MINUTES ***

*** FROM 721.286 TO 1000.911 MINUTES FROM MIDNIGHT OF EPDCH ***

ENTER SEGMENT 81 AT 3.2 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 1.4 CP SECS.

ENTER SEGMENT 82 AT 3.2 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
8	<p data-bbox="419 470 477 1672">Predetermined event table indicating the first integration time span. This time span covers all stages</p> <p data-bbox="502 1391 535 1672">TSTART, TSTOP</p>	11.2.2

***** STAGE 1 *****

STAPASS YEAR MO DY HR MN SEC RESIDUALS - EXTERNAL UNITS MME

SUMMARY OF PREDICTED STATISTICS

STA TYP RMS TYP RMS TYP RMS

PREDICTED RESIDUAL RMS = 0.

ENTER SEGMENT 83 AT 3.2 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS 0. GP SECS.

ITERATION NUMBER 1
0 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820 X	.2146907555645E+03	-0.	.2146907555645E+03	0.	.25784244E+03
6820 Y	.15942847794999E+07	-0.	.15942847794999E+07	0.	.21745334E+03
6820 Z	-.20753754537446E+03	-0.	-.20753754537446E+03	0.	.23985989E+03
6820 OX	.12377377639201E+04	-0.	.12377377639201E+04	0.	.55195925E+03
6820 OY	-.92186686159199E+04	-0.	-.92186686159199E+04	0.	.29661963E+03
6820 OZ	-.24308970466797E+05	-0.	-.24308970466797E+05	0.	.27633415E+03
6820 DRAG	.9217442938252E-02	-0.	.9217442938252E-02	0.	.51866171E-03

NAME	SIGMA ZERO	SIGMA DENT	TOTAL CORR.	I.C./SIGMA	T.C./SIGMA
6820 X	0.	.25784244E+03	0.	0.	0.
6820 Y	0.	.21745334E+03	0.	0.	0.
6820 Z	0.	.23985989E+03	0.	0.	0.
6820 OX	0.	.55195925E+03	0.	0.	0.
6820 OY	0.	.29661963E+03	0.	0.	0.
6820 OZ	0.	.27633415E+03	0.	0.	0.
6820 DRAG	0.	.51866171E-03	0.	0.	0.

RESIDUAL RMS = 0.
RESIDUAL SOS = 0.
APRIORI RMS = 0.
APRIORI SOS = 0.
TOTAL SOS = 0.
PREDICTED SOS = 0.

ITEM	DESCRIPTION	REFERENCE SECTION
	<p>The current solution is shown for one parameter per line, starting with the name (Test Case B, Item 4)</p> <p>The current value is the parameter value used in the iteration, partial derivatives, and residuals computation are computed. For the first iteration, it is the input value of the parameter. If an iteration is bad, the value is replaced for the best RMS is recovered from memory and is printed as the current value</p> <p>The correction is the least squares correction to be applied to the current value for the next iteration</p> <p>The new value is the sum of the current value plus the correction. This value will be used on convergence of this stage and will be applied to the next stage for all available parameters. The current value is used for the vehicle parameters</p> <p>The total correction is the value used to correct the parameters at this stage. This value includes the current prediction</p> <p>SIGMA is the square root of the diagonal elements of the covariance matrix $(A^T A)^{-1}$ for the parameters at the end of this iteration</p> <p>SIGMA ZERO is the square root of the diagonal elements of the initial $(A^T A)^{-1}$ before deweighting for this stage</p> <p>SIGMA DEWT is the square root of the diagonal elements of the deweighted $(A^T A)^{-1}$ at the start of this iteration</p> <p>T.C./SIGMA0 is the total correction/SIGMA ZERO</p> <p>T.C./SIGMA0 is the total correction/SIGMA DEWT</p> <p>The current value, current mean value, total correction, and SIGMA are normal least squares output. SIGMA ZERO, SIGMA DEWT, T.C./SIGMA0, and T.C./SIGMA0 are extended least squares output and are obtained when PANDR1570</p> <p>Residual RMS is the weighted root mean square residuals for the current iteration</p> <p>Residual SCS is the sum of squares of the normalized measurement residuals for the current iteration</p> <p>A priori RMS is the weighted root mean square total of the parameter corrections for the previous iterations for the current stage</p> <p>A priori SCS is the sum of the squares of the total parameter corrections for the previous iterations for the current stage</p> <p>Total SCS is the sum of the residual SCS + a priori SCS</p> <p>Predicted SCS is the predicted sum of the normalized measurement residuals squared</p>	<p>2.2.3</p> <p>2.2.4</p> <p>2.2.4</p> <p>2.2.2</p>

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

6020 X	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.27234E-02	.27234E-02	.92365E-03	.45841E-03	.44390E+03	.42806E+03	.41722E+03	.10966E+04
.17085E-03	.17085E-03	.16370E-03	.35395E+02	.84265E+02	.21921E+05	.64479E+05	.93397E+07
6020 Z	6020 Z	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
-.65588E-03	-.65588E-03	.35921E-02	-.20210E+01	-.84265E+02	.42806E+03	.41722E+03	.10966E+04
6020 DX	6020 DX	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
-.84361E+00	-.84361E+00	-.43786E+00	-.21456E+00	-.84265E+02	.42806E+03	.41722E+03	.10966E+04
6020 DY	6020 DY	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
-.20527E+00	-.20527E+00	-.43786E+00	-.21456E+00	-.84265E+02	.42806E+03	.41722E+03	.10966E+04
6020 DZ	6020 DZ	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
-.25873E+00	-.25873E+00	-.43786E+00	-.21456E+00	-.84265E+02	.42806E+03	.41722E+03	.10966E+04
6020 DRAG	6020 DRAG	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.70757E+02	.70757E+02	.79235E+01	.42212E+01	.34712E+04	-.21921E+05	.64479E+05	.93397E+07
ATA	ATA	ATA	ATA	ATA	ATA	ATA	ATA
-0.	-0.	-0.	-0.	-0.	-0.	-0.	-0.

ATA INVERSE

6020 X	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.66483E+05	.66483E+05	.47296E+05	.57532E+05	.30466E+00	.79421E-01	.87983E-01	.76361E-01
6020 Y	6020 Y	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.16826E+05	.16826E+05	.54656E+04	.42434E+02	.11191E+03	.14214E+00	.17826E-01	.23209E-04
6020 Z	6020 Z	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.56131E+05	.56131E+05	.42434E+02	.11191E+03	.14214E+00	.17826E-01	.23209E-04	.26901E-06
6020 DX	6020 DX	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.14043E+03	.14043E+03	.42434E+02	.11191E+03	.14214E+00	.17826E-01	.23209E-04	.26901E-06
6020 DY	6020 DY	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.34564E+02	.34564E+02	.42434E+02	.11191E+03	.14214E+00	.17826E-01	.23209E-04	.26901E-06
6020 DZ	6020 DZ	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.67719E+02	.67719E+02	.42434E+02	.11191E+03	.14214E+00	.17826E-01	.23209E-04	.26901E-06
6020 DRAG	6020 DRAG	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
-.66753E-01	-.66753E-01	.10330E-01	-.26583E-01	-.95712E-04	-.22947E-04	-.23209E-04	.26901E-06

CORRELATION MATRIX

6020 X	1.00000
6020 Y	.30010 1.00000
6020 Z	.90759 .10479 1.00000
6020 DX	.20676 .35355 .84528 1.00000
6020 DY	.45193 .95914 .28941 .49510 1.00000
6020 DZ	.95043 .67185 .92346 .93191 .21748 1.00000
6020 DRAG	-.34960 -.09159 -.21366 -.33433 -.14916 -.19676 1.00000

ENTER SEGMENT 84 AT 1.3 SECONDS EXECUTION TIME FOR SEGMENT 84 WAS 1.3 CP SECS.
ATA INVERSE UPDATED TO 811.22 MINUTES FROM MIDNIGHT OF EPOCH

6020 X	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.55687E+05	.55687E+05	.21730E+06	.14791E+07	.32479E+01	.44207E+00	.13083E+01	.76683E-01
6020 Y	6020 Y	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.67521E+05	.67521E+05	.49044E+06	.21726E+03	.28152E+03	.32502E+00	.35508E-01	.25901E-06
6020 Z	6020 Z	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.20658E+06	.20658E+06	.75470E+03	.21726E+03	.28152E+03	.32502E+00	.35508E-01	.25901E-06
6020 DX	6020 DX	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.32434E+03	.32434E+03	.15119E+03	.20548E+03	.20548E+03	.32502E+00	.35508E-01	.25901E-06
6020 DY	6020 DY	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.50349E+02	.50349E+02	.53597E+02	-.45517E+01	-.66394E-03	-.77576E-04	-.39061E-04	.25901E-06
6020 DZ	6020 DZ	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.62601E+02	.62601E+02	-.15668E+01	-.45517E+01	-.66394E-03	-.77576E-04	-.39061E-04	.25901E-06
6020 DRAG	6020 DRAG	6020 Z	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
-.5564E-01	-.5564E-01	-.15668E+01	-.45517E+01	-.66394E-03	-.77576E-04	-.39061E-04	.25901E-06

ITEM	DESCRIPTION	REFERENCE SECTION
10	<p data-bbox="376 906 409 1704"><u>$A^T A$</u> is the current $A^T A$ matrix for this iteration</p> <p data-bbox="434 459 533 1704"><u>$A^T B$</u> is the right-hand side of the normal matrix equation for the generalized least squares (GLS) problem when a priori statistics are included in the GLS solution of the linear system. The equation to be solved is</p> $(C_0^{-1} + A^T W A) \Delta P = A^T W B$ <p data-bbox="657 1608 690 1704">where</p> $A = \frac{\partial O_c}{\partial P}$ <p data-bbox="781 1066 814 1598">W = observation weighting matrix</p> <p data-bbox="827 1012 860 1598">P = vector of parameter corrections</p> <p data-bbox="868 757 910 1598">B = residual vector ($A^T W O_{mc}$) for the last iteration</p>	<p data-bbox="935 480 1017 1704"><u>$A^T A$ inverse</u> is the covariance for the parameter set at this iteration. It is the inverse of the $A^T A$ matrix above</p> <p data-bbox="1050 555 1108 1704"><u>Correlation matrix</u>, the correlation coefficients for the parameter set. These values are computed directly from the covariance matrix</p> <p data-bbox="1133 544 1199 1704"><u>$A^T A$ inverse updated</u> is the covariance for the parameter set updated to the time of the next iteration</p>

G AND G DEWEIGHTING MATRICES FOR VEHICLE 6320

ORBIT PLANE COORDINATE SYSTEM

.33140E+05
 -.29250E-18
 0.
 .39760E+06
 .31491E+05
 .63892E-10
 -.39775E+03
 0.
 -.38775E+02
 .33054E-21
 0.
 .60694E-10
 .40832E+00
 -.74757E-13
 .45369E-01
 0.
 .43098E-01

PARAMETER SET COORDINATE SYSTEM

.76445E-11
 -.79472E-11
 -.24449E-10
 -.17971E-11
 .15439E-11
 .50051E-11
 .15841E-09
 .25451E-09
 .82090E-09
 .53052E-10
 .48041E-11
 .14962E-14
 .33296E-11
 .28538E-12
 .38366E-12
 .56905E-14
 .37105E-12
 *** ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ***

YEAR/MC/DY	X	Y	Z	XR0T	YR0T	ZR0T	HEIGHT	ALPHA	DELTA	BETA	AZIMUTH	RADIUS	VELOCITY	A	E	I	O	U	TAU	AF	AG	N	L	CHI	PSI	MEAN ANOMALY	ECCENTRIC ANOM	TRUE ANOMALY	KEPLERIAN PER	ANOMALY PER	NODAL PERIOD	APOGEE RADIUS	APOGEE HEIGHT	PERIGEE RADIUS	PERIGEE HEIGHT	O-DOT	U-DOT				
1970/ 6/26	21462602.415							5.482511795	21798793.913	-.0122905196989	58.21461818	3664.19737																													
13/31	2060702.054							.071549899	.02134291985	-.0174559177234	59.2355346	228.10753																													
1.2588030	593.249							88.948443245	108.847926486	.0667914375674	60.35334034	3511.04979																													
.0015603	1262.7637296							198.847926491	185.481982716	3.371622844	89.8318739	74.95996																													
248.4688068	-8214.9716254							21561236.311	119.645021943	-.1335668939	89.5929426	2.7925652809																													
104.6003	-24308.3525001							25689.9725442	736.4870267	-1.35162602397	89.7251141	-2.0666905725																													

LEAST SQUARES PROCESS CONVERGED.

EXIT SEGMENT 94 AT 3.3 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CN SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
11	<u>Deweighting matrix</u> in the orbit plane coordinate system (RTC). The values in this matrix are used to deweight the $A^T A$ matrix. This deweighting allows for the uncertainty in the unmodeled parameters. Units are external	
12	<u>Parameter set coordinate system</u> is the RTC deweighting matrix converted to the parameter set coordinate system (ECI). This converted matrix is added to the updated $A^T A$ inverse matrix. Units are external	

ENTER SEGMENT 16 AT 3.3 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME (MME)	TYPE	ASSOCIATED QUANTITIES	* PREDETERMINED EVENT TABLE *
------------	------	-----------------------	-------------------------------

811.0210 TZERO
892.0000 TSTOP

892.0300 TSTOP

TRAJECTORY START

SEG11 ENTRY TIME IS 3.36790

```

NODE T = .811021379896E+03
DT = .12500000000000E+00

```

$$0T = .12500000 - C3DE+9C$$

STEP 037AND00

STEP TWO

```

NODE      T =      .35694329636503
          OT =      .50000000000000

```

OT = 10 .50000002376E+05.

TRAJECTORY TERMINATION

*** THIS CASE TOOK .483 SECONDS TO INTEGRATE A SPAN OF 71.1250 MINUTES ***

*** FROM 811.021 TO 882.146 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 3.9 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .5 CP SCS.

ENTER SEGMENT 82 AT 3.9 SECONDS. EXECUTION TIME FOR SEGMENT #1 WAS .1 CP SECS.

***** STAGE 2 *****

STAPASS YEAR MO DY HR MN SEC RESIDUALS - EXTERNAL UNITS MME

SUMMARY OF PREDICTED STATISTICS

TYP RMS TYP RMS TYP RMS

PREDICTED RESIDUAL RMS = 0.

ENTER SEGMENT 83 AT 3.9 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .0 CP SECS.

ITERATION NUMBER 1
0 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820 X	.2146267415330E+08	-6.	.2146267415330E+08	0.	.29859908E+03
6820 Y	.2060002544027E+07	-0.	.2060002544027E+07	0.	.53540718E+03
6820 Z	.58324941054139E+03	-0.	.58324941054139E+03	0.	.13559432E+04
6820 DX	.12627637289684E+04	-0.	.12627637289684E+04	0.	.19112453E+01
6820 DY	-.02148716253522E+04	-0.	-.02148716253522E+04	0.	.42129759E+00
6820 DZ	-.24308352500073E+05	-0.	-.24308352500073E+05	0.	.34901981E+01
6820 DRAG	.92174626938252E+02	-0.	.92174626938252E+02	0.	.58941494E+03

NAME	SIGMA ZERO	SIGMA DEWT	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMAD
6820 X	.23558149E+03	.29859908E+03	0.	0.	0.
6820 Y	.46615033E+03	.53540718E+03	0.	0.	0.
6820 Z	.12161926E+04	.13559432E+04	0.	0.	0.
6820 DX	.18021846E+01	.19112453E+01	0.	0.	0.
6820 DY	.36169753E+00	.42129759E+00	0.	0.	0.
6820 DZ	.27691647E+00	.34901981E+00	0.	0.	0.
6820 DRAG	.51866371E-03	.58941494E+03	0.	0.	0.

RESIDUAL RMS = 0.
RESIDUAL SOS = 0.
APRIORI RMS = 0.
APRIORI SOS = 0.
TOTAL SOS = C.
PREDICTED SOS = 0.

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

	6820 X	682 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.16114E-02						
6820 Y	.16088E-03	.36029E-04					
6820 Z	.87962E-05	.51395E-06	.14741E-04				
6820 DX	.32316E-02	-.35608E-02	-.10851E-01	.96554E+01			
6820 DY	-.43220E+02	-.51557E-01	-.97442E-04	-.20794E+01	.12850E+03		
6820 DZ	-.12593E+01	-.12158E+00	-.33604E-02	-.73308E+01	.33698E+03	.99553E+03	
6820 DRAG	.93853E+02	.80826E+01	-.27226E+01	.18668E+04	-.25541E+05	-.75004E+05	.10104E+08
ATA	-0.	-0.	-0.	-0.	-0.	-0.	0.

ATA INVERSE

	6820 X	682 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.89161E+05						
6820 Y	.64041E+05	.28666E+06					
6820 Z	.19587E+06	.60989E+06	.18386E+07				
6820 DX	.31122E+03	.07971E+03	.25379E+04	.36529E+01			
6820 DY	.61616E+02	.16430E+03	.31659E+03	.47678E+00	.17749E+03		
6820 DZ	.99219E+02	.57766E+02	.20549E+03	.32496E+00	.36601E-01	.12181E+00	
6820 DRAG	-.45064E-01	-.15666E+01	-.45517E+01	-.66094E-03	-.77576E-04	-.30061E-04	.34741E-06

CORRELATION MATRIX

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	1.00000						
6820 Y	.40058	1.00000					
6820 Z	.46277	.84009	1.00000				
6820 DX	.54534	.85871	.97929	1.00000			
6820 DY	.48980	.72839	.55419	.59212	1.00000		
6820 DZ	.95204	.30538	.43422	.48716	.24891	1.00000	
6820 DRAG	-.25605	-.49643	-.56953	-.58671	-.31241	-.14613	1.00000

ENTER SEGMENT 84 AT 4.0 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.

ATA INVERSE UPDATED TO 879.00 MINUTES FROM MIDNIGHT OF EPOCH

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.95809E+07						
6820 Y	.10097E+07	.18607E+06					
6820 Z	.13755E+06	.15107E+05	.88340E+05				
6820 DX	-.71989E+02	-.32306E+02	-.95064E+02	.11142E+00			
6820 DY	-.37018E+04	-.44852E+03	-.62902E+02	.49529E-01	.15454E+01		
6820 DZ	-.10980E+05	-.11553E+04	-.20265E+03	.13719E+00	.42122E+01	.12469E+02	
6820 DRAG	.12151E+01	.13110E+00	-.41728E-02	.10330E-04	-.49906E-03	-.14747E-02	.34741E-06

G AND G DEWEIGHTING MATRICES FOR VEHICLE 6820

ORBIT PLANE COORDINATE SYSTEM

.26229E+05			
-.79673E+04	.38750E+06		
0.	0.	.24916E+05	
.15384E+02	-.37474E+03	0.	.37047E+00
-.30689E+02	.93222E+01	0.	-.18000E-01
0.	0.	.57586E+01	0.
			.31734E-01

PARAMETER SET COORDINATE SYSTEM

.87797E-09			
.77093E-10	.64413E-10		
-.10427E-10	-.10049E-12	.59356E-10	
.34815E-11	-.11055E-11	-.39878E-11	.31126E-12
-.16180E-10	-.84678E-12	-.13394E-12	-.79310E-13
-.47865E-10	-.44451E-11	.15397E-11	-.24524E-12
			.53885E-12
			.83169E-12
			.27518E-11

**** ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ****

YEAR/MO/OY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADIUS
HR/MIN	Y	DELTA	E	AG	ECCENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMALY	PERIGEE RADIUS
LATITUDE	XOOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YOOT	RADIUS	U	CHI	ANOMALY PER	O-DOT
HEIGHT	ZOOT	VELOCITY	TAU	PSI	NODAL PERIOD	U-DOT
1970/ 6/26	-861872.839	97.158392672	21737616.110	.0115440762591	330.12379221	3647.59745
14/39	6862499.928	71.116301417	.01957929700	-.015140182847	329.55535415	211.36878
0.0003000	2.220527.828	50.568518390	108.876805463	.0670736009855	328.98203717	3507.50556
71.2343408	25757.4037672	271.463539434	185.611644975	276.252955068	89.4539728	71.27589
323.1034043	2520.8380076	21370691.970	120.517427874	-.13677847464	89.6928160	2.8239257559
83.5838	-29.3564957	25880.4313975	796.9697671	-1.38206143348	89.7249242	-2.000000599

LEAST SQUARES PROCESS CONVERGED.

EXIT SEGMENT 84 AT 4.0 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.

ENTER SEGMENT 10 AT 4.0 SECONDS. EXECUTION TIME FOR SEGMENT 04 WAS .1 CP SECS.
 ***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME(MME) TYPE ASSOCIATED QUANTITIES
 079.0000 TZERO
 903.7449 TSTOP

*** TRAJECTORY START

***** PREDETERMINED EVENT TABLE *****
 * * * * *
 SEG11 ENTRY TIME IS 4.04300 T = 882.250000 H = .250000 NSTEP = 25
 * STEP DOUBLED T = 889.250000 H = .500000 NSTEP = 52
 * NODE T = .900745995138E+03 .214559397444E+08 .212517332371E+07 -.122432195041E-04
 DT = .500000000000E+00 .128685767449E+04 -.021173714214E+04 -.243076958233E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .253 SECONDS TO INTEGRATE A SPAN OF 24.7500 MINUTES ***

*** FROM 879.000 TO 903.750 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 4.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .3 CP SECS.

ENTER SEGMENT 82 AT 4.4 SECONDS. EXECUTION TIME FOR SEGMENT 01 WAS .1 CP SECS.

***** STAGE 3 *****

STAPASS	YEAR	MO	DY	HR	MM	SEC	RESIDUALS - EXTERNAL UNITS	MME
393 16	1970	6	26	14	39	21.0000	0.	879.333
						PREDICTED RESIDUALS	0.	
393 16	1970	6	26	14	39	19.2503	0.	879.321
						PREDICTED RESIDUALS	0.	
393 16	1970	6	26	14	39	36.0000	0.	879.600
						PREDICTED RESIDUALS	0.	
393 16	1970	6	26	14	39	35.2492	0.	879.587
						PREDICTED RESIDUALS	0.	
393 16	1970	6	26	14	40	29.0000	0.	880.467
						PREDICTED RESIDUALS	0.	
393 16	1970	6	26	14	40	27.2438	0.	880.454
						PREDICTED RESIDUALS	0.	
393 16	1970	6	26	14	41	12.0000	0.	881.200
						PREDICTED RESIDUALS	0.	
393 16	1970	6	26	14	41	11.2384	0.	881.187
						PREDICTED RESIDUALS	0.	
393 16	1970	6	26	14	41	24.0000	0.	881.400
						PREDICTED RESIDUALS	0.	
393 16	1970	6	26	14	41	23.2371	0.	881.387
						PREDICTED RESIDUALS	0.	
313 16	1970	6	26	14	51	12.0000	0.	891.200
						PREDICTED RESIDUALS	0.	
313 16	1970	6	26	14	51	11.2533	0.	891.188
						PREDICTED RESIDUALS	0.	
313 16	1970	6	26	14	51	44.0000	0.	891.733
						PREDICTED RESIDUALS	0.	
313 16	1970	6	26	14	51	43.2484	0.	891.721
						PREDICTED RESIDUALS	0.	
313 16	1970	6	26	14	52	43.0000	0.	892.667
						PREDICTED RESIDUALS	0.	
313 16	1970	6	26	14	52	39.2320	0.	892.654
						PREDICTED RESIDUALS	0.	
313 16	1970	6	26	14	53	4.0000	0.	893.067
						PREDICTED RESIDUALS	0.	
313 16	1970	6	26	14	53	3.2305	0.	893.054
						PREDICTED RESIDUALS	0.	
313 16	1970	6	26	14	54	4.0000	0.	894.067
						PREDICTED RESIDUALS	0.	
313 16	1970	6	26	14	54	3.2296	0.	894.054
						PREDICTED RESIDUALS	0.	

REFERENCE
SECTION

ITEM

DESCRIPTION

13 Residuals - External Units. Each line corresponds to one input observation set or card and contains the station-pass identification in year, month, day, hour, minute, and second; three pairs of measurement residuals and identification; and the time in MME

The residuals are the unnormalized differences between the input measurements (modified by bias and/or refraction corrections) and the corresponding values for the same measured types computed from the integrated trajectory position at the observation time. The observation names are abbreviated as follows:

RNG	Range	CM3	Three-way cumulative doppler
AZ	Azimuth	DOP	Doppler
EL	Elevation	TWD	Two-way doppler
TRA	Topocentric right ascension	SRR	SGLS range rate
TD	Topocentric declination	AX	X-antenna
THA	Topocentric hour angle	AY	Y-antenna
GRA	Geocentric right ascension	CC3	JPL two- or three-way doppler
GD	Geocentric declination	TNT	Tranet doppler
U	u	GCR	Geoeiver range difference
V	v	V2	Vehicle-vehicle range
H	Height	V2D	Vehicle-vehicle range rate
X		S2	Station-vehicle-vehicle range
Y		S2D	Station-vehicle-vehicle range rate
Z		S3	Station-vehicle-vehicle-vehicle range
P	P	S3D	Station-vehicle-vehicle-vehicle range rate
Q	Q	V3	Vehicle-vehicle-vehicle range
RD	Range rate	TDA	Time differences of arrival
PD	P rate	TDA	Time of arrival
QD	Q rate	N	Time-of-arrival counter
CM1	One-way cumulative doppler	ACC	Accelerometer

Predicted residuals for each observation $(\hat{\phi}) = \hat{r} + [C_0] \hat{r}$ where $C_0 = (A^T A)^{-1}$ for this iteration

$$\hat{r} = \frac{\partial \hat{\phi}}{\partial \hat{p}}$$

\hat{p} = parameter set

SUMMARY OF PREDICTED STATISTICS

STA	TYP	RMS	TYP	RMS	TYP	RMS
313	RNG	.246498E+04	SFR	.311255E+02		
393	SRR	.234402E+02	RNG	.915407E+03		

PREDICTED RESIDUAL RMS = .2162231161E+03 (15)

ENTER SEGMENT 83 AT 4.5 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .1 CP SECS.

ITERATION NUMBER 1
 18 MEASUREMENTS WERE USED IN THIS SOLUTION
 CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820 X	-.86187283924646E+06	-.26946076E+04	-.85917823167636E+06	.26946076E+04	.86664237E+11
6820 Y	.68624999275575E+07	.15963546E+03	.68626595639133E+07	.15963546E+03	.12336910E+12
6820 Z	.25220327327524E+08	.85484888E+03	.25221382676088E+08	.85484888E+03	.38966545E+12
6820 DX	.25737403767231E+05	-.87179446E+00	.25736532062771E+05	-.87179446E+00	.41930156E+11
6820 DY	.25208181106158E+04	-.10258623E+01	.25198121452701E+04	-.10258623E+01	.41057022E+11
6820 DZ	-.29056495734126E+02	-.31997651E+01	-.32256260837096E+02	-.31997651E+01	.85279079E+11
6820 DRAG	.92174626938252E-02	.24751907E-03	.94649817670362E-02	.24751907E-03	.41172570E+13

NAME	SIGMA ZERO	SIGMA DENT	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMA0
6820 X	.30953062E+04	.31567975E+04	.26946076E+04	.87054636E+00	.35358898E+00
6820 Y	.43136142E+03	.46290205E+03	.15963546E+03	.37007322E+00	.74495796E+00
6820 Z	.29722097E+03	.33812934E+03	.85484888E+03	.29761339E+01	.25201713E+01
6820 DX	.33379987E+00	.38637129E+00	-.87179446E+00	-.26111339E+01	-.22563316E+01
6820 DY	.12431271E+01	.12692153E+01	-.10258623E+01	-.82922727E+00	-.80826505E+00
6820 DZ	.35311126E+01	.35782622E+01	-.31997651E+01	-.90614546E+00	-.89422321E+00
6820 DRAG	.58941497E-03	.58941494E-03	.24751907E-03	.41994028E+00	.41994028E+00

RESIDUAL RMS =	.1334096648E+03
RESIDUAL SDS =	.3203164959E+06
APRIORI RMS =	0.
APRIORI SOS =	0.
TOTAL SOS =	.32031664959E+06
PREDICTED SOS =	.1510667690E+02

ITEM	DESCRIPTION	REFERENCE SECTION
14	<u>Summary of predicted statistics</u> contains the station data type and the RMS value for each data type	Item 9
15	<u>Predicted residual RMS</u> is the resulting RMS value calculated from the RMS values of each data type	Item 14

ATA

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
6020 X	.46287E-01						
6020 Y	.12552E-01	.35232E-01					
6020 Z	-.10536E-01	.2825E-01	.67521E-01				
6020 DX	.19273E+02	.37392E+01	-.16916E+02	.20191E+05			
6020 DY	.16679E+02	.20377E+02	.15566E+02	.90214E+04	.17560E+05		
6020 DZ	-.76409E+01	.13403E+02	.37019E+02	-.13102E+05	.61963E+04	.21591E+05	
6020 DRAG	-.42191E+03	.16306E+03	.99403E+03	-.44431E+06	-.57531E+05	.56580E+06	.29194E+08
ATA	.10877E+03	-.3656E+01	-.95625E+02	.53025E+05	.14167E+05	-.50686E+05	-.16180E+07

.32037E+06

ATA INVERSE

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
6020 X	.75107E+02						
6020 Y	.50115E+01	.15220E+03					
6020 Z	.20719E+03	-.82866E+02	.15184E+04				
6020 DX	-.11061E+00	.25883E+00	-.10674E+01	.17581E-02			
6020 DY	-.84013E-01	.37172E+00	.16065E+00	-.12867E-02	.16857E-02		
6020 DZ	-.34376E+00	.35833E+00	-.30233E+01	.31680E-02	-.16098E-02	.72725E-02	
6020 DRAG	-.11839E-02	-.16032E-02	-.54738E-02	-.38768E-05	.10328E-04	.23858E-06	.16952E-06

CORRELATION MATRIX

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
6020 X	1.00000						
6020 Y	.04687	1.00000					
6020 Z	.61354	-.17446	1.00000				
6020 DX	-.30438	.50037	-.65329	1.00000			
6020 DY	-.23611	-.73388	.10041	-.74742	1.00000		
6020 DZ	-.46512	.34059	-.91132	.88597	-.45970	1.00000	
6020 DRAG	-.33180	-.32684	-.34118	-.22456	.61885	.00679	1.00000

ENTER SEGMENT 84 AT 4.15 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.

*** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 2. ***

YEAR/MC/DY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RAOTUS
HR/MIN	Y	DELTA	E	AG	ECCENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE NCALY	PERIGEE RADIUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	O-POT
HEIGHT	ZDOT	VELOCITY	TAU	PSI	NODAL PERIOD	U-POT
1970/ 6/26	-859170.232	57.136J7908C	21737496.946	.C115444705030	330.05894482	3647.45825
14/39	6862659.563	71.117991789	.C1954597749	-.C15724523242	329.49039975	211.21026
0.0J0C000	20221382.676	9C.5E8645043	188.875801391	.C670741516302	328.91695641	3507.68554
71.2355249	25756.532C62A	271.442104951	185.611994282	276.260879867	85.4532373	71.36555
323.0810907	2519.8121453	21371443.584	12C.599870828	-.13678442616	89.5921573	2.823827869
83.7077	-32.2562608	25879.5177238	796.9865525	-1.35203486846	85.7241692	-2.080357473

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
313	5 RNG	1.2E+33	5.8E+01	4.3E+02	5 AZ	2.4E-02	0.	3.1E-03	5 EL	1.9E-02	0.	7.4E-03
313	5 SRR	1.6E+31	1.6E+02	1.1E+31	5 EL	1.7E-02	0.	3.4E-03	5 SRR	1.9E+01	1.9E+02	1.8E+01
393	5 AZ	1.4E-01	0.	1.3E-31								
393	3 RNG	6.1E+02	3.8E+31	2.2E+32								

EXIT SEGMENT 84 AT 4.5 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.
 ENTER SEGMENT 10 AT 4.5 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME (HME) TYPE ASSOCIATED QUANTITIES
 879.3300 TZERO
 923.7449 TSTOP

*** TRAJECTORY START

***** PREDETERMINED EVENT TABLE *****

SEG	ENTRY	TIME	IS	4.57170	T	=	382.250000	H	=	.253000	NSTED	=	25
+	STEP	COUPLED			T	=	889.250000	H	=	.500000	NSTED	=	52
+	NODE	T =	.903745091723E+03				.214557299934E+08			.212528979768E+07			-0.144713230605E-04
	OT =	.500000000000E+00					.128581890605E+04			-.82114667770E+04			-.243780029595E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .253 SECONDS TO INTEGRATE A SPAN OF 24.750 MINUTES ***

*** FROM 879.330 TO 903.750 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 4.8 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .3 CP SECS.

ENTER SEGMENT 82 AT 4.9 SECONDS. EXECUTION TIME FOR SEGMENT 21 WAS .1 CP SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
16	<u>Total edit summary</u> is fully explained in Case B, Item 7.	2.2.4

***** STAGE 3 *****

STAPASS	YEAR	MO	DAY	HR	MM	SEC	RESIDUALS - EXTERNAL UNITS	MME
393	16	1970	6	26	14	39	27.0000	0.
393	16	1970	6	26	14	39	19.2503	0.
393	16	1970	6	26	14	39	36.0700	0.
393	16	1970	6	26	14	39	35.1692	0.
393	16	1970	6	26	14	40	28.0000	0.
393	16	1970	6	26	14	40	27.2438	0.
393	16	1970	6	26	14	41	12.0000	0.
393	16	1970	6	26	14	41	11.2384	0.
393	16	1970	6	26	14	41	24.0000	0.
393	16	1970	6	26	14	41	23.2371	0.
393	16	1970	6	26	14	51	12.0000	0.
393	16	1970	6	26	14	51	11.2533	0.
393	16	1970	6	26	14	51	44.0000	0.
393	16	1970	6	26	14	51	43.2484	0.
393	16	1970	6	26	14	52	40.0000	0.
393	16	1970	6	26	14	52	39.2320	0.
393	16	1970	6	26	14	53	4.0000	0.
393	16	1970	6	26	14	53	3.2365	0.
393	16	1970	6	26	14	54	4.0000	0.
393	16	1970	6	26	14	54	3.2296	0.

ENTER SEGMENT 83 AT 5.0 SECONDS. EXECUTION TIME FOR SEGMENT #2 WAS .1 CP SECS.

ITERATION NUMBER 2
16 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	X	Y	Z	DX	DY	DZ	DRAW	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820	X							-.85917823	.35999910E+00	-.85917781	.26949676E+04	.86647990E+01
6820	Y							-.68626595	.630133E+07	-.15450372E+01	.15809042E+03	.12332311E+02
6820	Z							.20221382	.678408E+08	.87685625E+00	.85572574E+03	.38971069E+02
6820	DX							.25756932	.762771E+05	.40341242E-03	.87137135E+00	.41930178E-01
6820	DY							.25198121	.452701E+04	-.33434910E-02	-.10292058E+01	.41030290E-01
6820	DZ							-.32256260	.830496E+02	.18162331E-02	-.31979499E+01	.85289058E-01
6820	DRAW							.94649817	.670862E-02	-.43065814E-05	-.24345649E-03	.41173917E-03

NAME	SIGMA ZERO	SIGMA LEWT	TOTAL CORR.	T.C./SIGMA	T.C./SIGMA
6820 X	.30953062E+04	.31567975E+04	.26949676E+04	.87066266E+04	.85370302E+00
6820 Y	.43136102E+03	.46290205E+03	.15009042E+03	.36649145E+03	.34152024E+00
6820 Z	.2972209 E+03	.33812934E+03	.85572574E+03	.28790901E+01	.25307645E+01
6820 DX	.3337990 E+00	.38637129E+00	-.87130105E+00	-.26102503E+01	-.22590875E+01
6820 DY	.12431127E+01	.12692153E+01	-.10292058E+01	-.82791685E+01	-.91089935E+00
6820 DZ	.35311826E+01	.35782622E+01	-.31979409E+01	-.99563112E+01	-.99371563E+00
6820 DRAG	.58941494E-03	.58941494E-03	.24345049E-03	.41303753E+00	.41303753E+00

RESIDUAL	RMS
RESIDUAL	.6734020011E+00
SOS	.8162485924E+01
APRIORI	.9997706082E+00
APRIORI	.695678883E+01
TOTAL	.1515927484E+02
PREDICTED	.1487141259E+02

ATA	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.46320E-01	.35183E-01	.67555E-01	.20240E+05	.17517E+05	.21619E+05	.28914E+06
6820 Y	.12520E-01	.27983E-01	-.16989E+02	.90207E+04	.61704E+04	.56051E+05	.13779E+04
6820 Z	-.10610E-01	.37246E+01	-.15509E+02	-.13147E+05	-.57035E+05	.29092E+02	.81625E+1
6820 DX	.19313E+02	.23327E+02	.37054E+02	-.43967E+06	-.55513E+02		
6820 DY	.16069E+02	.13387E+02	.98556E+03				
6820 DZ	-.76831E+01	.16168E+03	.16760E-01				
6820 DRAG	-.41838E+03	.16118E-01					
ATB	-.70171E-01						

ATA INVERSE

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.75179E+02	.15209E+03	.15107E+04	.17501E-02	.16835E-02	.72742E-02
6820 Y	.48999E+01	-.84416E+02	-.10677E+01	-.12873E-02	-.16091E-02	.30184E-06
6820 Z	.20715E+03	.25994E+00	.16293E+03	-.31672E-02	.10285E-05	.16953E-06
6820 DX	-.11670E+00	-.37126E+00	-.30310E+01			
6820 DY	-.83529E-01	.35854E+00	-.54754E-02			
6820 DZ	-.34426E+00	-.16532E-02				
6820 DRAG	-.11803E-02					

CORRELATION MATRIX

```

6820 X 1.00000
6820 Y .04585
6820 Z .61344
6820 DX -.30470
6820 DY -.23495
6820 DZ -.46584
6820 DRAG -.33084
1.00000
-.17565
.61344
.50075
-.73372
.34088
-.32558
1.00000
-.65340
1.00000
.10189
-.91189
-.34123
-.74823
.00860
1.00000
1.00000
-.45982
.60903
.00860
1.00000

```

ENTER SEGMENT 84 AT 5.0 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS
 *** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 3. ***

.0 CP SECS.

YEAR/MO/DY	X	Y	Z	XDOT	YDOT	ZDOT	ALPHA	DELTA	BETA	AZIMUTH	RADIUS	VELOCITY	TAU	AF	AG	N	L	CHI	PSI	MEAN ANOMALY	ECCENTRIC ANOM	TRUE ANOMALY	KEPLERIAN PER	ANOMALY PER	NODAL PERIOD	APOGEE RADIUS	APOGEE HEIGHT	PERIGEE RADIUS	PERIGEE HEIGHT	O-DOT	U-DOT	
1970/ 6/26	-859177.872	6862658.018	20221383.553	25756.5324662	2519.8088018	-32.2544446	97.136377710	71.117996552	96.568643087	271.442112057	21371443.903	25879.5177974	21737497.734	.0115444430051	330.05906030	329.49050718	328.91777581	89.4532421	89.692622	89.7241741	330.05906030	329.49050718	328.91777581	89.4532421	89.692622	89.7241741	3647.45839	211.21842	3587.61666	71.36669	2.823826735	-2.080358339
14/39	6862658.018	20221383.553	25756.5324662	2519.8088018	-32.2544446		71.117996552	96.568643087	271.442112057	21371443.903	25879.5177974																					
0.0000000																																
71.2355296																																
323.0810893																																
83.7077																																

EXIT SEGMENT 84 AT 5.0 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.

ENTER SEGMENT 10 AT 5.0 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.
 ***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME (MM) TYPE ASSOCIATED QUANTITIES
 879.0000 TZERO
 903.7449 TSTOP

*** TRAJECTORY START

***** PREDETERMINED EVENT TABLE *****
 *
 SEG11 ENTRY TIME IS 5.07700
 * STEP DOUBLED T = 882.250000 H = .250000 NSTEP = 25
 * STEP DOUBLED T = 889.250000 H = .500000 NSTEP = 52
 * NODE T = .900745093793E+03 .214557320665E+08 .212527764462E+07 -.729249300990E-05
 * DT = .000000000000E+00 .128580828105E+04 -.621146372638E+04 -.243780023900E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .255 SECONDS TO INTEGRATE A SPAN OF 24.7500 MINUTES ***

*** FROM 879.000 TO 903.750 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 5.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .3 CP SECS.

ENTER SEGMENT 82 AT 5.4 SECONDS. EXECUTION TIME FOR SEGMENT 61 WAS .1 CP SECS.

***** STAGE 3 *****

STAPASS	YEAR	MO	DAY	HR	MIN	SEC	RESIDUALS - EXTERNAL UNITS	MME
393 16	1970	6	26	14	39	20.0000	0.	879.333
393 16	1970	6	26	14	39	19.2503	-.362891E-01 SRR	879.321
393 16	1970	6	26	14	39	36.0000	0.	879.600
393 16	1970	6	26	14	39	35.2492	.368371E-01 SRR	879.507
393 16	1970	6	26	14	40	28.0000	-.127559E+02 RNG	880.467
393 16	1970	6	26	14	40	27.2438	-.275882E-01 SRR	880.454
393 16	1970	6	26	14	41	12.0000	-.221059E+01 RNG	881.200
393 16	1970	6	26	14	41	11.2384	-.311691E-02 SRR	881.107
393 16	1970	6	26	14	41	24.0000	-.543241E+01 RNG	881.400
393 16	1970	6	26	14	41	23.5371	-.438627E-01 SRR	881.387
313 16	1970	6	26	14	51	12.0000	-.231003E+02 RNG	891.200
313 16	1970	6	26	14	51	11.2533	-.473738E-01 SRR	891.188
313 16	1970	6	26	14	51	44.0000	-.264175E+02 RNG	891.733
313 16	1970	6	26	14	51	43.2484	-.734340E-01 SRR	891.721
313 16	1970	6	26	14	52	40.0000	-.170611E+02 RNG	892.667
313 16	1970	6	26	14	52	39.2320	-.002365E-01 SRR	892.654
313 16	1970	6	26	14	53	4.0000	-.185782E+02 RNG	893.067
313 16	1970	6	26	14	53	3.2305	-.338924E-03 SRR	893.054
313 16	1970	6	26	14	54	4.0000	-.171638E+02 RNG	894.067
313 16	1970	6	26	14	54	3.2296	-.344210E-02 SRR	894.054

ENTER SEGMENT 83 AT 5.5 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .1 CP SECS.

ITERATION NUMBER 3
16 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820 X	-.85917787167725E+06	.47835554E-03	-.85917787119919E+06	.26949680E+04	.86647932E-01
6820 Y	.6862658179761E+07	-.15530498E-03	.68626580178207E+07	.15809026E+03	.12332326E-02
6820 Z	.20221383553264E+08	.37430598E-02	.20221383557007E+08	.85572948E+03	.36971070E-02
6820 DX	.25756532466183E+05	-.39323101E-05	.25756532462351E+05	-.87131488E+00	.41930145E-01
6820 DY	.25198088017790E+04	-.81119420E-07	.25198088016979E+04	-.10292059E+01	.41030546E-01
6820 DZ	-.3225444597435E+02	-.81730286E-05	-.32254445276746E+02	-.31973570E+01	.85289692E-01
6820 DRAG	.94609131858769E-02	-.552555057E-08	.94609076601712E-02	.24344497E-03	.41173920E-03

NAME	SIGMA ZERO	SIGMA DENT	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMA0
6820 X	.30953062E+04	.31567975E+04	.26949680E+04	.87066282E+00	.35370317E+00
6820 Y	.4313612E+03	.46290205E+03	.15809026E+03	.36649109E+00	.34151991E+00
6820 Z	.2972209 E+03	.33812934E+03	.85572948E+03	.28791027E+01	.25307756E+01
6820 DX	.333799E+00	.38637129E+00	-.87130488E+00	-.26102618E+01	-.22550974E+01
6820 DY	.12431271E+01	.12692153E+01	-.10292059E+01	-.82791691E+00	-.81089941E+00
6820 DZ	.35311826E+01	.35782622E+01	-.31979570E+01	-.91563343E+00	-.89371791E+00
6820 DRAG	.58941494E-03	.58941494E-03	.24344497E-03	.41302816E+00	.41302816E+00
RESIDUAL RMS =	.667756855E+00				
RESIDUAL SOS =	.785924119E+01				
APRIORI RMS =	.100389503E+01				
APRIORI SOS =	.701293610E+01				
TOTAL SOS =	.148717722E+02				
PREDICTED SOS =	.148717717E+02				

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.46320E-01						
6820 Y	.12528E-01	.35143E-01					
6820 Z	-.10609E-01	.27983E-01	.67555E-01				
6820 DX	.19313E+02	.37247E+01	-.16989E+02	.20240E+05			
6820 DY	.16069E+02	.21328E+02	.15809E+02	.90208E+04	.17517E+05		
6820 DZ	-.76830E+01	.13397E+02	.37054E+02	-.13147E+05	.61704E+04	.21619E+05	
6820 DRAG	-.41838E+03	.16167E+03	.98555E+03	-.43966E+06	-.57036E+05	.56050E+06	.28914E+08
ATB	-.29748E-04	-.20918E-04	-.88262E-05	-.23391E-01	-.23512E-01	.30988E-02	.41490E+00

ATA INVERSE

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.75079E+02						
6820 Y	.49000E+01	.15209E+03					
6820 Z	.20715E+03	-.84417E+02	.15187E+04				
6820 DX	-.11070E+00	.25894E+00	-.10677E+01	.17581E-02			
6820 DY	-.83529E-01	-.37120E+00	.16293E+00	-.12873E-02	.10839E-02		
6820 DZ	-.34426E+00	.35854E+00	-.30310E+01	.31672E-02	-.16091E-02	.72742E-02	
6820 DRAG	-.11803E-02	-.16532E-02	-.54754E-02	-.38723E-05	.10289E-04	.30196E-06	.16953E-06

CORRELATION MATRIX

6820 X 1.00000
 6820 Y .04586 1.00000
 6820 Z .61344 -.17565 1.00000
 6820 DX -.30469 .50075 -.65340 1.00000
 6820 DY -.23495 -.73372 .11198 -.74823 1.00000
 6820 DZ -.46594 .34688 -.01189 .88565 -.45982 1.00000
 6820 DRAG -.33084 -.32558 -.34123 -.22430 .60902 .00860 1.00000

ENTER SEGMENT 04 AT 5.5 SECONDS. EXECUTION TIME FOR SEGMENT #3 WAS .0 CP SECS.

A7A INVERSE UPDATED TO 500.74 MINUTES FROM MIDNIGHT OF EPOCH

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.75352E+04	.48176E+03	.56034E+04	.23166E-01	.65730E-03	.52821E-02	.16953E-06
-.14908E+04	-.14064E+04	.10604E+02	.15167E+01	.33877E-02	.12298E-02	-.54047E-05
.60784E+04	-.25608E+01	.10604E+02	.15167E+01	.33877E-02	.12298E-02	-.54047E-05
.13201E+02	-.26673E+00	.15167E+01	.33877E-02	.12298E-02	.12298E-02	-.54047E-05
.19277E+01	-.13525E+01	.52459E+01	.92051E-02	-.59657E-05	-.54047E-05	.16953E-06
.51825E+01	-.13525E+01	.52459E+01	.92051E-02	-.59657E-05	-.54047E-05	.16953E-06
-.23175E-01	.66550E-02	-.11955E-01	-.15155E-04	-.59657E-05	-.54047E-05	.16953E-06

G AND G DEWEIGHTING MATRICES FOR VEHICLE 6820

ORBIT PLANE COORDINATE SYSTEM

.78246E+04	.13243E+05	74329E+04	.41201E-01
-.96415E+04	0.	0.	-.20402E-01
0.	0.	0.	0.
.17437E+02	-.20776E+02	0.	.10712E-01
-.91552E+01	.11281E+02	0.	0.
0.	0.	.58474E+01	.19176E-01

PARAMETER SET COORDINATE SYSTEM

```

.16473E-11
.69271E-11
.21336E-10
.22445E-11
.54055E-12
.11590E-11
.19750E-10
.61505E-11
.11550E-11
.10236E-11
.34357E-12
.14631E-11
.32562E-12
.76111E-13
.97225E-13
.16903E-13
.17612E-13
    
```

*** ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ***

YEAR/MO/DY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADIUS
HP/MIN	Y	DELTA	E	AG	ECCENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMALY	PERIGEE RADIUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	O-DOT
HEIGHT	ZDOT	VELOCITY	TAU	PSI	NODAL PERIOD	U-DOT
1970/ 6/26	21455717.114	5.657163506	21797285.075	.0123957499983	58.21076095	3663.69744
15/ 0	2125373.124	.030751110	.02127520963	-.0173693664702	59.32922068	227.68446
44.694.030	282.643	88.951419980	118.840776953	.0667983727789	60.33345092	3511.44667
.0067562	1286.1091971	198.848776950	185.656927894	3.553413457	89.3225473	74.96429
226.151867	-8211.4289637	21560728.370	119.615715412	-.13733735945	29.6836302	2.7933472359
104.5167	-24304.0023914	25639.7112610	886.2034378	-1.39123356209	89.7157996	-2.0669831941

LEAST SQUARES PROCESS CONVERGED.

TOTAL ECIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
313	5 RNG	2.1E+01	1.0E+00	-6.6E-01	5 EL	8.9E-03	0.	-5.5E-03
313	5 SRR	5.3E-02	5.3E-01	2.1E-02	5 SRR	3.3E-02	3.3E-01	-3.4E-03
393	5 AZ	9.1E-02	0.	9.1E-02				
393	3 RNG	8.1E+00	4.1E-01	-3.2E+00				

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TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM
RNG	0	-.422278908+2	.03141500E+00	-.6571398E+00	.40913610E+02
AZ	1	-.42256725E-1	.2093823E-03	-.3175314E-01	-.21256903E-01
EL	2	-.19483211E-1	.2788169E-03	-.5542366E-02	.83984781E-02
SRR	3	-.77414358E-1	.19583505E-02	.23503126E-01	.11842065E+00

TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM
53472.*	
53482.*	
53492.*	
53502.*	
53512.*	
53522.*	
53532.*	
53542.*	
53552.*	
53562.*	
53572.*	
53582.*	
53592.*	
53602.*	
53612.*	
53622.*	
53632.*	
53642.*	

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TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM
AZ	0	.65166516E-1	.50850711E-03	.93591862E-01	.11601722E+00
EL	1	-.53078909E-1	.79851344E-03	-.13133237E-01	.26812435E-01
SRR	2	-.69479148E-1	.13222093E-02	-.33688846E-02	.62741779E-01
RNG	3	-.18091632E-2	.29827194E+00	-.31790344E+01	.11735563E+02

TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM
52760.*	
52770.*	
52780.*	
52790.*	
52800.*	
52810.*	
52820.*	
52830.*	
52840.*	
52850.*	
52860.*	
52870.*	
52880.*	

EXIT SEGMENT 84 AT 5.6 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .1 CP SECS.

ITEM	DESCRIPTION	REFERENCE SECTION
17	An example of the printer plot of the measurement residuals for the <u>last iteration (see Case B, Item 20, for a full explanation)</u>	2.2.1 11.1.2 15

ENTER SEGMENT 10 AT 5.6 SECONDS. EXECUTION TIME FOR SEGMENT 04 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME(MME) TYPE ASSOCIATED QUANTITIES
879.0000 IZERO
1621.2182 ISTOP

*** TRAJECTORY START

***** PREDETERMINED EVENT TABLE *****

SEG11 ENTRY TIME IS	STEP	T	H	ECI	NSSTEP	NSSTEP
5.64200	000000	982.250000	0.250000	0.250000	25	25
5.64200	000000	809.250000	0.500000	0.500000	52	52
5.64200	000000	214557320668E+08	212527764464E+07	212527764464E+07	163423225258E+04	163423225258E+04
5.64200	000000	128581028242E+04	0.21146372635E+04	0.21146372635E+04	14398023999E+05	14398023999E+05
5.64200	000000	944.750000	1.000000	1.000000	162	162
5.64200	000000	218803714357E+08	0.22005023323E+07	0.22005023323E+07	125779257434E+01	125779257434E+01
5.64200	000000	345907455384E+03	0.14265712192E+04	0.14265712192E+04	38120373837E+05	38120373837E+05
5.64200	000000	214489766159E+08	0.21904653327E+07	0.21904653327E+07	203249489554E+00	203249489554E+00
5.64200	000000	131064337857E+04	0.202010237125E+04	0.202010237125E+04	24372204050E+05	24372204050E+05
5.64200	000000	218706977640E+08	0.22669543461E+07	0.22669543461E+07	58991176111E+01	58991176111E+01
5.64200	000000	371226613584E+03	0.814293763106E+04	0.814293763106E+04	238341151012E+05	238341151012E+05
5.64200	000000	214421025123E+08	0.225584277690E+07	0.225584277690E+07	863067201429E+01	863067201429E+01
5.64200	000000	133502110587E+04	0.820410225153E+04	0.820410225153E+04	243065075938E+05	243065075938E+05
5.64200	000000	21860898722E+08	0.233339315702E+07	0.233339315702E+07	101487221398E+00	101487221398E+00
5.64200	000000	336803041540E+03	0.814285997901E+04	0.814285997901E+04	238364978998E+05	238364978998E+05
5.64200	000000	21435461178E+08	0.232115326113E+07	0.232115326113E+07	183242366425E+01	183242366425E+01
5.64200	000000	135985239073E+04	0.819580465312E+04	0.819580465312E+04	243754490028E+05	243754490028E+05
5.64200	000000	218505799153E+08	0.239962253565E+07	0.239962253565E+07	349275773535E+03	349275773535E+03
5.64200	000000	421904305512E+03	0.814166299668E+04	0.814166299668E+04	238391830641E+05	238391830641E+05
5.64200	000000	214287958496E+08	0.23867293595E+07	0.23867293595E+07	141720489610E+00	141720489610E+00
5.64200	000000	138359662734E+04	0.819456210999E+04	0.819456210999E+04	243743612622E+05	243743612622E+05
5.64200	000000	218400481221E+08	0.246518206583E+07	0.246518206583E+07	153969776460E+01	153969776460E+01
5.64200	000000	447494361867E+03	0.814101306780E+04	0.814101306780E+04	23819324156E+05	23819324156E+05
5.64200	000000	214216538875E+08	0.245314069009E+07	0.245314069009E+07	134185454353E+00	134185454353E+00
5.64200	000000	140705124634E+04	0.81808296350E+04	0.81808296350E+04	243733393389E+05	243733393389E+05
5.64200	000000	218293481956E+08	0.25315839874E+07	0.25315839874E+07	190257516319E+00	190257516319E+00
5.64200	000000	473738187344E+03	0.8135980303347E+04	0.8135980303347E+04	234448042444E+05	234448042444E+05

NODE T = .143889773764E+04
 DT = .100000000000E+01
 NODE T = .148477523587E+04
 DT = .100000000000E+01
 NODE T = .152855981410E+04
 DT = .100000000000E+01
 NODE T = .157443233333E+04
 DT = .100000000000E+01
 NODE T = .161821345867E+04
 DT = .100000000000E+01

.214142223518E+06
 .143188662466E+04
 -.218185158357E+08
 -.499282763766E+03
 .152855981410E+04
 .145653788076E+04
 -.218172374883E+08
 -.52411908623E+03
 .213994585329E+08
 .148056649020E+04

.251756189895E+07
 -.818469744155E+04
 -.259856294727E+07
 .812348091137E+04
 .256374667414E+07
 -.817537123394E+04
 -.266469893192E+07
 .813783967267E+04
 .264837440794E+07
 -.817509952422E+04

.238869289165E-01
 -.243722798899E+05
 -.426712096486E-02
 .238474219867E+05
 -.139505778299E+00
 -.243710299133E+05
 -.178961111444E-01
 .239502272862E+05
 -.124191763445E+00
 -.242996054642E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .915 SECONDS TO INTEGRATE A SPAN OF 742.750 MINUTES ***

*** FROM 879.030 TO 1621.750 MINUTES FROM MIDNIGHT OF EPOCH ***
 *** TRACE56 EPHMERIS OUTPUT KEY ***

DATE,...	ME,MM,ST,DT	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...	REMARK
YR/MO/DAY	MIN FROM EPOCH	X (FT)	X (FT)	ALPHA (DEG)	LATITUDE (DEG)	REV COUNT	.
HR/MIN	MIN FROM MIDNIGHT	Y (FT)	Y (FT)	DELTA (DEG)	LONGITUDE (DEG)	PERIOD	.
SEC	SEC FROM MIDNIGHT	Z (FT)	Z (FT)	BETA (DEG)	ALTITUDE (NM)	PERIOD-DECAY	.
	STEP SIZE (MIN)	XO (FT/SEC)	XO (FT/SEC)	AZIMUTH (DEG)	S-VEH-LAT (DEG)	MOD-REG	.
IT	UTC - IT	YO (FT/SEC)	YO (FT/SEC)	R (FT)	I (DEG)		
	UT1 - IT	ZO (FT/SEC)	ZO (FT/SEC)	V (FT/SEC)	O (DEG)		

* * * * * ECI TRAJECTORY * * *

*** CASE 1

*** EPOCH PRINT

DATE,...	ME,MM,ST,DT,...	X,XC	X,XD - BF	ADBARV	LAT,... BF	REV,...
70/ 6/26	0.00300	-0.59177872E+06	.552943353E+07	97.13607771	71.23532964	.24863
14/39	879.00000	.56265812E+07	-.415447366E+07	71.11799655	323.08108931	0.00000
0.00000	52740.00000	.232213836E+08	.232213936E+08	90.56864399	83.70774013	0.00000
		.257565325E+05	-.164017950E+05	271.44211206	71.23274551	0.00000
IT		.251981887E+04	-.236658767E+05	.21371444E+08	108.87579657	
		-.322144446E+02	-.322254444E+02	.25879518E+05	51.55699698	
A =	.21737498E+08	MEAN ANCM =	.33005906E+03	APOGEE =	.36474584E+04	
E =	.19545978E-01	ECCENTRIC =	.32949051E+03	HEIGHT =	.21121842E+03	
I =	.10887580E+03	TAUE ANOM =	.32891708E+03	PERIGEE =	.35076057E+04	
O =	.18561199E+03	KEEL PER =	.9453242E+02	HEIGHT =	.71365690E+02	
U =	.12358975E+03	ANCM PER =	.89692362E+02	O-DOT =	.28238268E+01	
TAU =	.79699652E+03	NCOL PER =	.19724174E+02	U-DOT =	-.20003583E+01	

*** REQUESTED PRINTS

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,...
70/ 6/26	21.74509	.214557321E+08	-.149366771E+08	5.65692696	-.00000039	.50000 DSC NODE
15/ 0	90.74509	.212527759E+07	-.155480551E+08	-.00000039	226.15078160	0.00000
44.70563	54044.70563	-.147473157E+00	-.147473157E+00	88.95141266	104.51754274	0.00000
		.128561810E+04	-.744391549E+04	198.84877695	-.00000039	0.00000
IT		-.821146374E+04	.649884239E+04	.21560734E+08	108.84667950	
		-.243800224E+05	-.243800224E+05	.25689695E+05	46.15078174	

DELTA NODE = .013 DELTA V = -89.7141

(18)

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,...
70/ 6/26	111.45900	.214489767E+08	-.137216942E+08	5.93139148	-.00000693	1.50000 DSC NODE
16/30	990.45900	.219146382E+07	-.871272125E+07	-.00000699	203.8355595	0.00000
27.53971	59427.53971	-.259150197E+01	-.259150197E+01	88.55178468	104.48516846	0.00000
		.131664551E+04	-.441879149E+04	198.85054353	-.00000693	0.00000
IT		-.326811268E+04	.833922557E+04	.21561537E+08	108.85038759	
		-.243072214E+05	-.243072214E+05	.25689136E+05	23.83555921	

ITEM	DESCRIPTION	REFERENCE SECTION
18	<p data-bbox="386 635 451 1742"><u>Delta Node</u> is the difference between the predicted node time and the <u>input node time</u></p> <p data-bbox="475 554 516 1742"><u>Delta V</u> is the difference in velocity at the predicted and input node times</p>	2.2.11.1

DELTA NODE = -.011 DELTA V = -.0002									
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	BF	REV,...	OSC	MODE
70/ 6/26	201.16392	.214421628E+08	-.215528327E+08	6.00577563	..00001374		2.50000		
19/29	1080.16392	.22558411E+07	-.572707417E+06	-.00001295	181.52212002		89.70841		
3.33519	04859.83519	-.487416521E+01	-.437416521E+01	88.95319054	104.46935725		0.10000		
IT	1.00000	.133501531E+04	-.731338886E+03	198.85099714	-.00001394		.17480		
	.00000	-.820410289E+04	.985501748E+04	.21560443E+08	186.8475333				
	.00000	-.243065077E+05	-.243065077E+05	.256843439E+05	1.52212444				
DELTA NODE = -.036 DELTA V = -.0005									
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	BF	REV,...	OSC	MODE
70/ 6/26	29.85963	.214354463E+08	-.211570499E+08	6.18023193	..00000957		3.50000		
19/29	1163.85963	.232115205E+07	-.765241429E+07	-.00001951	159.21125520		89.69853		
51.57806	70191.57806	-.35766384E+01	-.357806384E+01	88.95336690	104.52073191		-.00988		
IT	1.00000	.135984799E+04	.376464178E+04	198.85099939	-.00000957		.17487		
	0.00000	-.819960514E+04	.939449343E+04	.21560754E+08	186.84140924				
	0.00000	.243065490E+05	-.243065490E+05	.25687374E+05	339.21125844				
DELTA NODE = -.073 DELTA V = -.0012									
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	BF	REV,...	OSC	MODE
70/ 6/26	38.54792	.214287958E+08	-.215743469E+08	6.135351092	..00000043		4.50000		
20/59	1253.54792	.238602036E+07	-.147319236E+08	-.00000943	136.90177593		89.69101		
32.87528	75572.87528	-.159996576E+00	-.159996576E+00	88.955541135	104.59832840		-.00752		
IT	1.00100	.138359652E+04	.64015954E+04	198.84955597	-.00000043		.17449		
	.00000	-.819456211E+04	.752649396E+04	.21561224E+08	108.83051044				
	.00000	-.243064361E+05	-.243064361E+05	.25685933E+05	316.90177517				
DELTA NODE = -.123 DELTA V = -.0020									
DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,...	BF	REV,...	OSC	MODE
70/ 6/26	470.22819	.214216533E+08	-.213738337E+07	6.52865239	..00000493		5.50000		
22/29	1349.22819	.245154134E+07	-.196052934E+08	-.00000480	114.59676720		89.68198		
13.69145	9093.69145	.190533638E+01	-.190533638E+01	88.95876518	104.64370017		-.00912		
IT	1.00000	.140705351E+04	.877935830E+04	198.84899737	..00000493		.17288		
	.00000	-.818562935E+05	.453105004E+04	.21561477E+08	108.81533541				
	.00000	-.243063393E+05	-.243063393E+05	.25684782E+05	294.59476556				
70/ 6/26	559.89774	.214142223E+08	-.215444451E+08	6.77513675	..00000142		6.50000		
23/58	1438.89774	.251756217E+07	-.215444451E+08	-.00000141	92.29255036		89.67197		
53.86424	86333.86424	.511300907E+00	.934165049E+04	198.848938690	104.67714663		-.00991		
IT	1.00000	.143185722E+04	.860814736E+03	.21561703E+08	108.79783419		.17518		
	.00000	-.818409737E+04	-.860814736E+03	.256873465E+05	272.29254597				
	.00000	-.243062799E+05	-.243062799E+05						

DELTA NODE = -.203 DELTA V = -.0034

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBRV	LAT,... BF	REV,...	DSC MODE
70/ 6/27	649.55881	.21406907E+08	.737797002E+07	6.88029536	-.00010358	7.50000	
1/28	1528.55881	.258304619E+07	.202606282E+08	-.00073366	69.99075998	89.66484	
33.58090	5313.58990	-.137648336E+01	-.137648336E+01	88.59986531	104.75522760	-.00713	
	1.07000	.145653643E+04	.943119771E+04	198.84691289	-.00000368	.17673	
IT	0.00000	-.017937142E+04	-.293925337E+04	.21562177E+08	108.84712996		
	0.00000	-.243010299E+05	-.243010299E+05	.25681972E+05	249.99075133		

DELTA NODE = -.233 DELTA V = -.0039

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBRV	LAT,... BF	REV,...	DSC MODE
70/ 6/27	739.21396	.213994588E+08	.145146072E+08	7.05498926	-.0001259	8.50000	
2/58	1618.21396	.264837286E+07	.159460620E+08	-.00071251	47.69055222	89.65710	
12.83771	10692.83771	-.70774157E+01	-.470774157E+01	88.56197226	104.84384478	-.00775	
	1.00000	.148356096E+04	.751035070E+04	198.84814915	-.0001259	.17475	
IT	0.00000	-.817510032E+04	-.629802904E+04	.21562716E+08	126.84563644		
	0.00000	-.242596055E+05	-.242596055E+05	.25680638E+05	227.69055648		

DELTA NODE = -.255 DELTA V = -.0043

TRAJECTORY TERMINATION

A =	.21783497E+08	MEAN ANCH	=	.69639794E+02	APOGEE	=	.36587057E+04
E =	.20530278E+01	ECCENTRIC	=	.70750326E+02	HEIGHT	=	.22279347E+03
I =	.10884909E+03	TRUE ANOM	=	.71364713E+02	PERIGEE	=	.35114994E+04
O =	.18705511E+03	KEPL PER	=	.89737334E+02	HEIGHT	=	.75587163E+02
U =	.11848199E+03	ANCH PER	=	.89611976E+02	O-DOT	=	.27994103E+01
TAU =	.16033909E+04	MODL PER	=	.99644152E+02	U-DOT	=	-.20713653E+01

END OF TRAJECTORY ***

EXIT SEGMENT 50 AT 6.8 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS .2 CP SECS.

TRAJECTORY INTEGRATION FOR CASE 1 *****

ASSOCIATED QUANTITIES

TIME(MME)	TYPE
900.7449	TZERO
993.4592	TSTOP

TRAJECTORY START

[illegible]

TRAJECTORY TERMINATION

*** THIS CASE TOOK .473 SECONDS TO INTEGRATE A SPAN OF 93.2500 MINUTES ***

```
*** FROM 500.745 TO 993.995 MINUTES FROM MIDNIGHT OF EPOCH ***
```

ENTER SEGMENT 81 AT 7.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .5 CP SECS.

ENTER SEGMENT 82 AT 7.4 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SEC.

***** STAGE 4 *****

STAPASS	YEAR	MO	DAY	HR	MIN	SEC	RESIDUALS - EXTERNAL UNITS			MME
							TYP	RMS	TYP	RMS
393 17	1970	6	26	16	7	20.0000	0.	.778958E-01	AZ	967.333
						PREDICTED RESIDUALS	0.	0.	0.	
393 17	1970	6	26	16	7	19.2528	.519859E+00	0.	SRR	967.321
						PREDICTED RESIDUALS	.22250E+01	0.	0.	
393 17	1970	6	26	16	8	4.0000	.448224E+03	.747379E-01	AZ	968.067
						PREDICTED RESIDUALS	.679392E+03	0.	0.	
393 17	1970	6	26	16	8	3.2507	.140701E+00	0.	SRR	968.054
						PREDICTED RESIDUALS	.501885E+01	0.	0.	
393 17	1970	6	26	16	8	28.0000	.431812E+03	.927567E-01	AZ	968.467
						PREDICTED RESIDUALS	.528062E+03	0.	0.	
393 17	1970	6	26	16	8	27.2486	.624195E+00	0.	SRR	968.454
						PREDICTED RESIDUALS	.775019E+01	0.	0.	
393 17	1970	6	26	16	9	0.0000	.363979E+03	.756500E-01	AZ	969.000
						PREDICTED RESIDUALS	.221027E+03	0.	0.	
393 17	1970	6	26	16	8	59.2444	.334749E+01	0.	SRR	968.587
						PREDICTED RESIDUALS	.117638E+02	0.	0.	
393 17	1970	6	26	16	10	4.0000	.673896E+02	.113288E+00	AZ	970.067
						PREDICTED RESIDUALS	.516391E+03	0.	0.	
393 17	1970	6	26	16	10	3.2352	.449521E+01	0.	SRR	970.054
						PREDICTED RESIDUALS	.804813E+01	0.	0.	

STA TYP RMS TYP RMS TYP RMS

393 SRR .765986E+01 RNG .513694E+03

PREDICTED RESIDUAL RMS = .5960568927E+02

ENTER SEGMENT 83 AT 7.4 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .1 CP SECS.

ITERATION NUMBER 1
9 MEASUREMENTS WERE USED IN THIS SOLUTION

CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820 X	.2145517113563E+08	-.46831199E+02	.21455670282464E+08	-.46831099E+02	.78929819E+02
6820 Y	.21253731238283E+07	-.2086587E+03	.2125164729618E+07	-.20865807E+03	.76947084E+02
6820 Z	.2826431437326E+03	.15964563E+01	.2842396005202E+03	.15964563E+01	.11451517E+03
6820 DX	.1286159197693E+04	-.19195345E+00	.12859673436397E+04	-.19185345E+00	.14809437E+00
6820 OY	-.8211428963711E+04	-.36894704E+00	-.82117975107534E+04	-.3688474E+00	.44335061E+01
6820 OZ	-.24318072381429E+05	-.1831393E-02	-.24308004212928E+05	-.1831393E-02	.93765791E+01
6820 DRAG	.94609075661712E-02	-.24678299E-03	.92141242731143E-02	-.24673299E-03	.32835328E-03

NAME	SIGMA ZERO	SIGMA OENT	TOTAL CORR.	T.C./SIGMA	T.C./SIGMA
6820 X	.86805251E+02	.12145175E+03	-.46831099E+02	-.53949616E+00	-.30559428E+00
6820 Y	.21949089E+02	.9551248E+02	-.2086587E+03	-.95061286E+01	-.21836540E+01
6820 Z	.74856045E+02	.13505311E+03	.15964563E+01	.21327019E-01	.11820952E-01
6820 DX	.15220332E+06	.25044331E+00	-.19185345E+00	-.12605076E+01	-.76574965E+00
6820 OY	.25647653E-01	.11173154E+00	-.36884704E+00	-.14381317E+02	-.3012195E+01
6820 OZ	.72678355E-01	.12624497E+00	-.1831393E-02	-.25198699E-01	-.14576251E-01
6820 DRAG	.4117392E-03	.49792486E-03	-.24678299E-03	-.59936724E+00	-.9562295E+00

RESIDUAL RMS = .2241036669E+02
 PRIORI SOS = .4520020810E+04
 PRIORI SOS = 0.
 PRIORI SOS = 0.
 TOTAL SOS = .4520020810E+04
 PREDICTED SOS = .3056764551E+02

ATA

	6820 X	6820 Y	6820 Z	6820 OX	6820 OY	6820 OZ	6820 DRAG
6820 X	.87892E+01						
6820 Y	.65287E+00	.49508E-01					
6820 Z	-.47921E+00	-.33768E-01	.00680E-01				
6820 OX	.12797E+04	.93528E+02	-.73920E+02	.18992E+06			
6820 OY	-.25357E+04	-.19105E+03	.13254E+03	-.36483E+06	.74119E+06		
6820 OZ	-.79119E+04	-.58664E+03	.43293E+03	-.11551E+07	.22793E+07	.71263E+07	
6820 DRAG	-.18049E+05	-.13479E+04	.98224E+03	-.26334E+07	.52186E+07	.16291E+08	.46454E+08
ATA	.16012E+03	.12971E+02	-.63761E+01	.21334E+05	-.50032E+05	-.14254E+06	-.33427E+06

.45200E+04

ATA INVERSE

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.62259E+04						
.15792E+04	.59259E+04					
.872.7E+04	.20195E+04	.13114E+05				
.11196E+02	.42725E+01	.16196E+02	.21932E-01			
.30804E+01	.16927E+01	.45008E+01	.55049E-02	.19656E-02		
.73431E+01	.22693E+01	.10233E+02	.13585E-01	.35492E-02	.87808E-02	
.14115E-02	.42814E-04	.19356E-02	.32074E-05	.12856E-05	.16789E-05	.1782E-06

CORRELATION MATRIX

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
1.00000						
.2602	1.00000					
.96483	.22903	1.00000				
.95780	.37493	.95498	1.00000			
.88028	.49620	.8651	.83843	1.00000		
.93282	.31472	.95359	.97892	.85432	1.00000	
.05446	-.00169	.05149	.06596	.39803	.05457	1.00000

ENTER SEGMENT 84 AT 7.5 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS
 *** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 2. ***

.9 CP SECS.

YEAR/NO/DY	X	Y	Z	ALPHA	BETA	AZIMUTH	RADIUS	VELOCITY	TAU	CHI	PSI	MEAN ANOMALY	ECCENTRIC ANOM	TRUE ANOMALY	KEPLERIAN PER	ANOMALY PER	MODAL PERIOD	APOGEE RADIUS	APOGEE HEIGHT	PERIGEE RADIUS	PERIGEE HEIGHT	O-DOT	U-DOT
1970/ 6/26	21455670.282	2125164.473	21277338.583	5.656644001	.010755345	88.951761166	198.849501195	21560661.200	119.636955905	-.13779605544	-.139125344564	58.25819728	59.37827585	60.35227594	85.9228781	89.6839588	89.7161255	3663.69455	227.80501	3511.06657	74.97784	2.7934261179	-2.0667979488
15/ 0																							
44.6940090																							
.0007604																							
226.1505472																							
104.5057																							

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
393	5 A2	8.8E-02	0.	8.7E-02	5 EL	2.0E-02	0.	-1.4E-03	5 SRR	2.5E+00	2.5E+01	-1.3E+00
393	4 RVG	3.6E+02	1.8E+11	3.3E+12								

EXIT SEGMENT 94 AT 7.5 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .9 CP SECS.

ENTER SEGMENT 10 AT 7.5 SECONDS. EXECUTION TIME FOR SEGMENT 14 WAS .1 CP SECS.

TRAJECTORY INTEGRATION FOR CASE 1

TIME (H:MM)	TYPE	ASSOCIATED QUANTITIES	* PREDETERMINED EVENT TABLE *
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TRAJECTORY START

[illegible]

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .474 SECONDS TO INTEGRATE A SPAN OF 93.250 MINUTES ***

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*** FROM 966.745 TO 993.995 MINUTES FROM MIDNIGHT OF EPOCH ***

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ENTER SEGMENT 81 AT 8.0 SECONDS. EXECUTION TIME FOR SEGMENT 19 WAS .5 CP SECS.

ENTER SEGMENT 82 AT 8.1 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .1 CP SECS.

***** STAGE 4 *****

STAPASS	YEAR	MO	DY	HR	MM	SEC	RESIDUALS - EXTERNAL UNITS				MME		
393 17	1970	6	26	16	7	20.0000	0.	.765619E-01	AZ	-.119794E-01	EL	967.333	
393 17	1970	6	26	16	7	19.2528	-.507401E-01	SRR	0.	0.		967.321	
393 17	1970	6	26	16	8	4.0000	.425502E+01	RNG	.753160E-01	AZ	-.291289E-01	EL	968.067
393 17	1970	6	26	16	8	3.2507	-.113955E+00	SRR	0.	0.		968.054	
393 17	1970	6	26	16	8	29.0000	-.374171E+00	RNG	.955793E-01	AZ	.285608E-02	EL	968.467
393 17	1970	6	26	16	8	27.2486	.341970E+00	SRR	0.	0.		968.454	
393 17	1970	6	26	16	9	0.0000	-.265366E+01	RNG	.828947E-01	AZ	-.988464E-02	EL	969.000
393 17	1970	6	26	16	8	59.2444	-.455000E+00	SRR	0.	0.		968.987	
393 17	1970	6	26	16	10	4.0000	-.701144E+01	RNG	.123622E+00	AZ	.301353E-01	EL	970.067
393 17	1970	6	26	16	10	3.2352	-.466441E-02	SRR	0.	0.		970.054	

ENTER SEGMENT 83 AT 841 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .1 CP SECS.

ITERATION NUMBER 2
9 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	X	Y	Z	DX	DY	DZ	DRAG	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820	X							.2145567282464E+08	.92491652E-01	.21455670374955E+08	-0.46736603E+02	.78930351E+02
6820	Y							.2125164729018E+07	.16091504E-01	.21251644890533E+07	-0.20861470E+03	.76946620E+02
6820	Z							.2842396105002E+03	.87796232E-01	.28432739828369E+03	.16825261E+01	.11451511E+03
6820	DX							.12859673436397E+04	.24579873E-03	.12859675094304E+04	-0.19161785E+00	.14009628E+00
6820	DY							-0.02117978107534E+04	.50299954E-04	-0.0211797804534E+04	-0.36873674E+00	.44335549E-01
6820	DZ							-0.24308004217828E+05	.12568941E-03	-0.24308004087139E+05	-0.17057099E-02	.93704034E-01
6820	DRAG							.92141246731143E-02	.88942603E-07	.92142136157169E-02	-0.24669404E-03	.32034745E-03

NAME	X	Y	Z	DX	DY	DZ	DRAG	SIGMA ZERO	SIGMA DENT	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMA0
6820	X							.86805251E+02	.12145175E+03	-0.46736608E+02	-0.53043065E+00	-0.18433273E+00
6820	Y							.21949089E+02	.95551248E+02	-0.20861478E+03	-0.95053955E+01	-0.21634856E+01
6820	Z							.74956045E+02	.13505311E+03	.16842526E+01	.224997607E-01	.12471039E-01
6820	DX							.15220332E+00	.25054331E+00	-0.19160785E+00	-0.12588927E+01	-0.76476859E+00
6820	DY							.25647653E-01	.11173154E+00	-0.36879674E+00	-0.14379356E+02	-0.33007693E+01
6820	DZ							.72678355E-01	.12624897E+00	-0.17057099E-02	-0.23469297E-01	-0.13510684E-01
6820	DRAG							.4173920E-03	.49792486E-03	-0.24669404E-03	-0.59915122E+00	-0.49544432E+00


```

RESIDUAL RMS = .1324313099E+01
RESIDUAL SDS = .1578424666E+02
PRIORI RMS = .1453812521E+01
PRIORI SOS = .1479499593E+02
TOTAL SDS = .3657124259E+02
PREDICTED SDS = .3057910301E+02

```

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
6020 X	.87868E+01						
6020 Y	.65260E+00	.49481E-01					
6020 Z	-.47907E+00	-.3752E-01	.30672E-01				
6020 DX	.12793E+04	.93493E+02	-.72996E+02	.18985E+06			
6020 DY	-.25351E+04	-.19098E+03	.13251E+03	-.36473E+06	.74107E+06		
6020 DZ	-.79097E+04	-.18639E+03	.43280E+03	-.11547E+07	.22788E+07	.71243E+07	
6020 DRAG	-.18059E+05	-.13415E+04	.98279E+03	-.26348E+07	.52219E+07	.16261E+08	.46508E+08
ATA	-.27693E-01	-.22579E-02	.10408E-02	-.36341E+01	.85895E+01	.24675E+02	.57351E+02

.15784E+02

ATA INVERSE

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
6020 X	.62300E+04						
6020 Y	.15792E+04	.59208E+04					
6020 Z	.87208E+04	.20185E+04	.13114E+05				
6020 DX	.11196E+02	.42725E+01	.16196E+02	.21932E-01			
6020 DY	.30804E+01	.16927E+01	.45008E+01	.55048E-02	.19656E-02		
6020 DZ	.73431E+01	.22692E+01	.10233E+02	.13585E-01	.35491E-02	.87806E-02	
6020 DRAG	.14102E-02	-.43631E-04	.19339E-02	.32044E-05	.12792E-06	.16770E-05	.10781E-06

CORRELATION MATRIX

	6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
6020 X	1.00000						
6020 Y	.26003	1.00000					
6020 Z	.96483	.22907	1.00000				
6020 DX	.95780	.37484	.95498	1.00000			
6020 DY	.88027	.49619	.8658	.83841	1.00000		
6020 DZ	.99282	.31472	.97831	.35429	.35429	1.00000	
6020 DRAG	.05441	-.00173	.05143	.00879	.05451	1.00000	

ENTER SEGMENT 84 AT 8.2 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .9 CP SECS.

ATA INVERSE UPDATED TO 990.46 MINUTES FROM MIDNIGHT OF EPOCH

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.64488E+04						
6820 Y	.22545E+04	.70603E+04					
6820 Z	.10446E+05	.51398E+04	.21586E+05				
6820 DX	.14193E+02	.76367E+01	.25567E+02	.33597E-01			
6820 DY	.33610E+01	.25718E+01	.69484E+01	.85926E-02	.24916E-02		
6820 DZ	.71493E+01	.29442E+01	.12150E+02	.15859E-01	.38137E-02	.87277E-02	
6820 DRAG	-.67963E-02	-.14985E-02	-.27622E-03	-.13003E-04	-.15558E-05	.92745E-06	.10781E-06

G AND G DEWEIGHTING MATRICES FOR VEHICLE 6820

ORBIT PLANE COORDINATE SYSTEM

.33140E+05			
-.28250E-18	.39768E+06		
0.	0.	.31481E+05	
.53892E-10	-.38775E+03	0.	.40832E+00
-.38775E+02	.33054E-21	0.	-.74757E-13
0.	0.	.60694E-10	0.
			.45369E-01
			0.
			.43090E-01

PARAMETER SET COORDINATE SYSTEM

.76544E-10			
-.84431E-11	.15836E-09		
-.25985E-10	.25440E-09	.82087E-09	
-.19090E-11	.16972E-10	.50821E-10	.33260E-11
.15218E-11	.19085E-11	.51080E-11	.30326E-12
.50021E-11	.51099E-12	.47902E-15	-.55433E-15
			.38724E-12
			.56820E-14
			.37185E-12

*** ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ***

YEAR/MC/OY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADIUS
HR/MIN	Y	DELTA	E	AG	ECCENTRIC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMALY	PERIGEE RADIUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	O-DOT
HEIGHT	ZDOT	VELOCITY	TAU	PSI	NOODAL PERIOD	U-DOT
1970/ 6/26	21448940.285	5.836716977	21796005.085	.0122908967746	58.37509577	3663.35866
16/30	2190322.224	.000496226	.02124174705	-.0173247199113	59.42292033	227.28738
27.5520000	186.731	88.952055837	108.851268834	.0668042571570	60.47652666	3513.96353
.0004996	1310.7168068	198.851268834	185.830547549	3.728592319	89.8146355	74.89225
203.8346400	-8208.4446951	21560405.867	119.522948988	-.14202932182	89.6757341	2.7942694148
104.4768	-24307.2205315	25689.2489736	975.8954835	-1.35087350274	89.7078954	-2.0868271786

LEAST SQUARES PROCESS CONVERGED.

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
393	5 AZ	8.8E-02	0.	8.7E-02	5 EL	2.0E-02	0.	-1.4E-03
393	4 RNG	3.6E+02	1.8E+01	3.3E+02	5 SRR	2.5E+00	2.5E+01	-1.6E+00

TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM
AZ	0	.57387975E+01	.58955203E-03	.86865617E-01	.11634326E+00
EL	1	-.42231769E-01	.81594036E-03	-.14347512E-02	.39362287E-01
SRR	2	-.55172833E+01	.77994378E-01	-.16175644E+01	.22821505E+01
RNG	3	.20522198E+02	.61460753E+01	.32782596E+03	.63512972E+03

TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM
58040	3
58050	*
58060	*
58070	*
58080	*
58090	*
58100	*
58110	*
58120	*
58130	*
58140	*
58150	*
58160	*
58170	*
58180	*
58190	*
58200	*

EXIT SEGMENT 84 AT 6.2 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

◆◆ PREDETERMINED EVENT TABLE ◆◆

ASSOCIATED QUANTITIES

TIME (HME)	TYPE
900.7449	TZERO
1710.8623	TSTOP

*** TRAJECTORY START

[illegible]

NODE T = .1438903341775E+04
 DT = .100000000000E+01
 NODE T = .148478197219E+04
 DT = .100000000000E+01
 NODE T = .15285573776E+04
 DT = .100000000000E+01
 NODE T = .157444108760E+04
 DT = .100000000000E+01
 NODE T = .161822351636E+04
 DT = .100000000000E+01
 NODE T = .16640595975E+04
 DT = .100000000000E+01
 NODE T = .17078692196E+04
 DT = .100000000000E+01

.214143730173E+08
 .143197618436E+04
 .21819767521E+08
 .499183945199E+03
 .214073028286E+08
 .14565933864E+04
 .218179394785E+08
 .524274479972E+03
 .213995838503E+08
 .148065841045E+04
 .217962812645E+08
 .550156266870E+03
 .21391762930E+08
 .150503006250E+04

.251737365455E+07
 .818504397135E+04
 .259842659783E+07
 .813865422107E+04
 .258286156986E+07
 .817571391562E+04
 .266457146476E+07
 .813890329923E+04
 .264819264741E+07
 .817543636605E+04
 .273067911266E+07
 .813757464437E+04
 .271341376866E+07
 .817111856521E+04

-.83251352040E-01
 -.243722684018E+05
 .184823510083E-01
 .238469054249E+05
 .192848794083E+00
 -.243710155487E+05
 -.166571505548E+00
 .238496698736E+05
 .190298708107E-01
 -.242995880307E+05
 -.46055256516E-01
 .23525181497E+05
 -.79343391331E-01
 -.242982759545E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .965 SECONDS TO INTEGRATE A SPAN OF 810.250° MINUTES ***

*** FROM 500.745 TO 1710.995 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 50 AT 9.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS 1.0 CP SECS

*** TRACE66 EPHEMERIS OUTPUT KEY ***

DATE,...	HE,MM,SS,DT	X,XD	X,XD - BF	ADBARV	LAT,...	REV,...	REMARK
YR/MO/DAY	MIN FROM EPOCH	X (FT)	X (FT)	ALPHA (DEG)	LATITUDE (DEG)	REV COUNT	.
HR/MIN	MIN FROM MIDNIGHT	Y (FT)	Y (FT)	DELTA (DEG)	LONGITUDE (DEG)	PERIOD	.
SEC	SEC FROM MIDNIGHT	Z (FT)	Z (FT)	BETA (DEG)	ALTITUDE (N°)	PERIOD-DECAY	.
IT	STEP SIZE (MIN)	XD (FT/SEC)	XD (FT/SEC)	AZIMUTH (DEG)	S-VEH-LAT (DEG)	MOD-REG	.
	UTC - IT	YD (FT/SEC)	YD (FT/SEC)	R (FT)	I (DEG)		
	UT1 - IT	ZD (FT/SEC)	ZD (FT/SEC)	V (FT/SEC)	O (DEG)		

*** ECI TRAJECTORY ***

*** CASE 1

*** EPOCH PRINT

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADBARV	LAT,.. BF	REV,...
70/ 6/26	0.00000	.214556703E+08	-.149364904E+08	5.55664410	.00076044	.50000
15/ 0	900.74490	.212516447E+07	-.155687417E+08	.00075574	226.15054724	0.00000
44.69400	54044.65400	.284239600E+03	.284239600E+03	86.55176117	104.50566791	0.00000
IT	.12500	.128596734E+04	-.744424983E+04	198.84950120	.00076028	0.00000
	.00000	-.821179781E+04	.649898865E+04	.21560661E+08	108.84950120	
	.00000	-.243080042E+05	-.243080042E+05	.25668581E+05	46.15024052	
A =	.21797339E+08	MEAN ANOM =	.58260157E+02	APOGEE =	.36636945E+04	
E =	.21272900E-01	ECENTRIC =	.59382726E+02	HEIGHT =	.22760581E+03	
I =	.10884950E+03	TRUE ANCP =	.60362206E+02	PERIGEE =	.35110666E+04	
O =	.18565639E+03	KEPL PER =	.89822878E+02	HEIGHT =	.74977836E+02	
U =	.11963700E+03	ANOM PER =	.89883959E+02	O-DCT =	.27934261E+01	
TAU =	.89621852E+03	NODL PER =	.89716126E+02	U-DCT =	-.20667979E+01	

*** REQUESTED PRINTS

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADBARV	LAT,.. BF	REV,...
70/ 6/26	0.00019	.214556853E+08	-.149365774E+08	5.65639613	.00000000	.50000
15/ 0	900.74509	.212506845E+07	-.155686657E+08	.00000000	226.15024052	0.00000
44.70569	54044.70569	.249001808E+04	.249685575E-04	88.95175381	104.50659261	0.00000
IT	.12500	.128561444E+04	-.744424894E+04	198.84950119	.00000000	0.00000
	.00000	-.921183277E+04	.649898959E+04	.21560667E+08	108.84953488	
	.00000	-.243080042E+05	-.243080042E+05	.256685805E+05	46.15024052	
DELTA NODE =	.013	DELTA V =	-.89.7141			

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADBARV	LAT,.. BF	REV,...
70/ 6/26	89.71443	.214489506E+08	-.197217459E+08	5.83054327	.00001264	1.50000
16/30	990.45333	.219025757E+07	-.871248832E+07	.00001255	203.83443330	0.00000
27.55988	59427.55988	.472287522E+01	-.472287522E+01	88.95205994	104.47743549	0.00000
IT	1.00000	.131047915E+04	-.441872337E+04	198.85125894	-.0001263	0.00000
	.00000	-.820846896E+04	.83963313E+04	.21563490E+08	108.8487665	
	.00000	-.243072205E+05	-.243072205E+05	.256685245E+05	23.834-.3767	

DELTA NODE = .009 DELTA V = -89.7052

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,... DSC NODE
73/ 6/26	179.4.1993	.21420973E+08	-.215528130E+08	6.00524419	-.00001096	2.50000
18/ 0	1088.16483	.225563953E+07	-.572420969E+06	-.00001088	181.52136040	89.70894
9.88981	64803.88981	-.479559499E+01	-.479559499E+01	88.55338154	104.46438428	0.00000
IT	1.00000	.133489282E+04	-.731134537E+03	198.85171352	-.00011996	.17481
	0.00000	-.821446546E+04	.985537073E+04	.21560414E+08	108.84372393	
	0.00000	-.243165057E+05	-.243065057E+05	.25688546E+05	1.52136411	

DELTA NODE = .019 DELTA V = -89.6963

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,... DSC NODE
70/ 6/20	269.11646	.214354620E+08	-.201569164E+08	6.17970566	-.00000244	3.50000
19/29	1169.86136	.232195455E+07	-.765274995E+07	-.00000242	159.21023533	89.69931
51.68184	70191.68184	-.912413357E+00	-.912413357E+00	88.5534062	104.51999436	-.00964
IT	1.00000	.135976345E+04	-.316496424E+04	198.85161678	-.00000244	.17488
	0.00000	-.819596379E+04	.939474680E+04	.21560749E+08	108.83489710	
	0.00000	-.243354449E+05	-.243054449E+05	.25687410E+05	335.21029616	

DELTA NODE = .031 DELTA V = -89.6886

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,... DSC NODE
70/ 6/26	358.80582	.214288330E+08	-.157431650E+08	6.35290695	.00000435	4.50000
20/59	1259.55072	.238582606E+07	-.147322709E+08	.00000433	136.89984942	89.69293
33.04319	75573.04319	.162767580E+01	.162767580E+01	88.55544874	104.60096574	-.00727
IT	1.00000	.138354675E+04	.640200088E+04	198.85028451	.00010435	.17450
	0.00000	-.819491698E+04	.752659943E+04	.21561240E+08	108.82137302	
	0.00000	-.243043549E+05	-.243043549E+05	.25686038E+05	316.89994754	

DELTA NODE = .045 DELTA V = -89.6802

DATE,...	ME,MM,ST,DT,...	X,XD	X,XD - BF	ADBARV	LAT,... BF	REV,... DSC NODE
70/ 6/26	448.48741	.214217126E+08	-.897332123E+07	6.52812349	.00000286	5.50000
22/29	1349.23231	.245134964E+07	.196055704E+08	.00000284	114.59321131	89.68316
13.93845	80953.93845	.106826385E+01	.106826385E+01	88.95872605	104.64674163	-.00887
IT	1.00000	.140703647E+04	.877978738E+04	198.84962701	.00000286	.17280
	0.00000	-.819018042E+04	.453177263E+04	.21561514E+08	108.80471249	
	0.00000	-.243133845E+05	-.243033845E+05	.25684885E+05	294.59321034	

DELTA NODE = .089 DELTA V = -89.6688

DATE,... ME,MM,ST,DT,...
 70/ 6/26 538.15852
 23/58 1438.90342
 54.20508 86334.20508
 1.00000
 6.00000
 IT 0.00000
 .00000
 DELTA NODE = .138
 DELTA V = -89.6603
 X,XD X,XD - BF
 .214143037E+08
 .251737354E+07
 .389226012E+00
 .143190578E+04
 .818104392E+04
 .243022684E+05
 .861778912E+06
 .215445325E+08
 -.339226012E+00
 .994202325E+04
 .860547767E+03
 -.243022684E+05
 AOBARV
 6.70467415
 -.00000103
 88.55926901
 198.84874451
 .21561761E+08
 .25683566E+05
 LAT,... BF
 -.00010104
 92.29030370
 104.68671713
 -.00000104
 108.84898509
 272.29050475
 REV,...
 6.50000 DSC NODE
 89.67349
 -.00966
 .17518

DATE,... ME,MM,ST,DT,...
 70/ 6/27 627.82241
 1/28 1528.56731
 34.03862 5314.03862
 1.00000
 1.00000
 IT .00000
 .00000
 DELTA NODE = .217
 DELTA V = -89.6509
 X,XD X,XD - BF
 .214070031E+08
 .258286027E+07
 .401596464E+01
 .145658878E+04
 .817971359E+04
 .243010156E+05
 .737884687E+07
 .202603940E+08
 -.431596464E+01
 .943143079E+04
 .293868518E+04
 -.243010156E+05
 AOBARV
 6.87976210
 -.00001967
 88.55966903
 198.84764484
 .21562257E+08
 .25682070E+05
 LAT,... BF
 -.0001074
 95.98134783
 104.76139940
 -.0001174
 108.84642285
 245.98835147
 REV,...
 7.50000 DSC NODE
 89.66661
 -.00688
 .17673

DATE,... ME,MM,ST,DT,...
 70/ 6/27 717.47862
 2/58 1618.22352
 13.41117 10693.41117
 1.00000
 0.00000
 IT 0.00000
 .00000
 DELTA NODE = .318
 DELTA V = -89.6388
 X,XD X,XD - BF
 .213595841E+08
 .264819113E+07
 .447732963E+01
 .148165295E+04
 .817543706E+04
 .242995881E+05
 .145154875E+08
 .159453987E+08
 -.447732963E+01
 .761037231E+04
 .629855848E+04
 -.242995881E+05
 AOBARV
 7.05446814
 -.00001198
 47.58753614
 104.88063967
 -.0001197
 108.84221351
 227.68764020
 LAT,... BF
 -.00001198
 47.58753614
 104.88063967
 -.0001197
 108.84221351
 227.68764020
 REV,...
 8.50000 DSC NODE
 89.65912
 -.00750
 .17475

DATE,... ME,MM,ST,DT,...
 70/ 6/27 807.12481
 4/27 1767.86971
 52.18270 16072.18270
 1.00000
 3.00000
 IT .00000
 .00000
 DELTA NODE = .443
 DELTA V = -89.6276
 X,XD X,XD - BF
 .213517630E+08
 .271341346E+07
 .954935475E+00
 .150502887E+04
 .817111871E+04
 .242582755E+05
 .194805004E+08
 .924555265E+07
 -.954935475E+00
 .465699874E+04
 -.871556180E+04
 -.242582755E+05
 AOBARV
 7.22901183
 -.0000266
 25.38927320
 104.91796446
 -.0000266
 108.83369697
 205.38927410
 LAT,... BF
 -.0000266
 25.38927320
 104.91796446
 -.0000266
 108.83369697
 205.38927410
 REV,...
 9.50000 DSC NODE
 89.64951
 -.00961
 .17482

*** TRAJECTORY TERMINATION

```

A = .21784133E+08      MEAN ANOM = .64068895E+02      APOGEE = .36592199E+14
E = .20643742E-01      ECCENTRIC = .65142122E+02      HEIGHT = .22332311E+03
I = .10885036E+03      TRUE ANOM = .66220110E+02      PERIGEE = .35111943E+04
O = .18722902E+03      KEPL PER = .89741261E+02      HEIGHT = .75297496E+02
U = .11837888E+03      ANOM PER = .89605599E+02      O-DCT = .27993325E+01
TAU = .16930237E+04      NODL PER = .89637770E+02      U-DCT = -.240706795E+01
  
```

*** END OF TRAJECTORY ***

```

EXIT SEGMENT 50 AT 9.5 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS .3 CP SECS.
ENTER SEGMENT 10 AT 9.5 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS .3 CP SECS.
  
```

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME(NME) TYPE ASSOCIATED QUANTITIES

```

990.4592 TZERO
1067.0233 TSTOP
  
```

* PREDETERMINED EVENT TABLE *

*** TRAJECTORY START

```

*****
SEG11 ENTRY TIME IS 9.56500
NODE T = .990459328035E+03      .21448950327E+08      .219025916574E+07      .345415535802E-04
DT = .125030000000E+00      .131049502801E+04      -.820846836465E+04      -.24372205316E+05
* STEP DOUBLED T = 994.459200 H = .250000 NSTEP = 31
* STEP DOUBLED T = 998.709200 H = .500000 NSTEP = 47
* STEP DOUBLED T = 1020.209200 H = 1.000000 NSTEP = 89
NODE T = .103636736719E+04      -.218709586538E+08      -.226677558081E+07      -.996434377020E-01
DT = .100000000000E+01      -.371291430118E+03      .814315093846E+04      .238338021858E+05
  
```

*** TRAJECTORY TERMINATION

```

*** THIS CASE TOOK .392 SECONDS TO INTEGRATE A SPAN OF 76.7500 MINUTES ***
  
```

```

*** FROM 990.459 TO 1067.209 MINUTES FROM MIDNIGHT OF EPOCH ***
  
```

```

ENTER SEGMENT 81 AT 10.0 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .4 CP SECS.
  
```

```

ENTER SEGMENT 82 AT 10.0 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.
  
```


***** STAGE 5 *****

STAPASS YEAR MO DY HR MM SEC RESIDUALS - EXTERNAL UNITS HME

SUMMARY OF PREDICTED STATISTICS

STA	TYP	RMS	TYP	RMS	TYP	RMS
-----	-----	-----	-----	-----	-----	-----

PREDICTED RESIDUAL RMS = 0.

ENTER SEGMENT 83 AT 10.0 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .0 CP SECS.

ITERATION NUMBER 1
0 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820 X	.214850284574E+00	-0.	.214850284574E+00	0.	.19991533F+03
6820 Y	.2190322239458E+07	-0.	.2190322239458E+07	0.	.27639606E+03
6820 Z	.18673059803602E+03	-0.	.18673059803602E+03	0.	.61727697F+03
6820 DX	.13107168068238E+04	-0.	.13107168068238E+04	0.	.66193016E+00
6820 DY	-.8208444695180E+04	-0.	-.8208444695180E+04	0.	.22269565E+00
6820 DZ	-.24307220531520E+05	-0.	-.24307220531520E+05	0.	.23287673E+00
6820 DRAG	.92142136157169E-02	-0.	.92142136157169E-02	0.	.43152294E-03

NAME	SIGMA ZERO	SIGMA DENT	TOTAL CORR.	T.C./SIGMA	T.C./SIGMA
6820 X	.80304656E+02	.19991533E+03	0.	0.	0.
6820 Y	.84025871E+02	.27639606E+03	0.	0.	0.
6820 Z	.14692307E+03	.61727697E+03	0.	0.	0.
6820 DX	.1832918E+00	.66193016E+00	0.	0.	0.
6820 DY	.49916415E-01	.22269565E+00	0.	0.	0.
6820 DZ	.93422328E-01	.23287673E+00	0.	0.	0.
6820 DRAG	.32834745E-03	.43152294E-03	0.	0.	0.

RESIDUAL RMS = 0.
RESIDUAL SOS = 0.
APRIORI RMS = 0.
APRIORI SOS = 0.
TOTAL SOS = 0.
PREDICTED SOS = 0.

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.42654E-02	.72200E-04					
.43729E-03	.47189E-05					
.35167E-04	.15421E-03	.31884E-04				
.86672E-01	.12293E+00	.27604E-01	.32051E+02			
.11819E+01	.35443E+00	.12498E-01	.23336E+02	.35021E+03		
.34489E+01	.17261E+03	.27134E-01	.71343E+02	.95440E+03	.28076E+04	
.17261E+03	.17276E+02	.52806E+03	.55206E+04	.47603E+05	.13977E+06	.12492E+08
ATB	-0.	-0.	-0.	-0.	-0.	-0.

ATA INVERSE

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
.39966E+05	.76395E+05					
.14428E+04	.11654E+06	.38103E+06				
.93284E+03	.13180E+03	.39062E+03	.43815E+00			
.26585E+00	.16500E+02	.44227E+02	.45480E-01	.49593E-01		
.14467E+02	.66731E+01	.12154E+02	.15792E-01	.45049E-02	.53860E-01	
.43655E+02	.14995E-02	.27622E-03	.13003E-04	.15558E-05	.92745E-06	.18621E-06
6820 DRAG						

CORRELATION MATRIX

6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
1.00000						
.02611	1.00000					
.00756	.68304	1.00000				
.00197	.72040	.95601	1.00000			
.32496	.26807	.32173	.30253	1.00000		
.94492	.10493	.08484	.10280	.06716	1.00000	
.07878	.01256	.00104	.04552	.01619	.00926	1.00000

ENTER SEGMENT 84 AT 10.1 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.

ATA INVERSE UPDATED TO 1064.92 MINUTES FROM MIDNIGHT OF EPOCH

	6820 X	6820 Y	6820 Z	6820 OX	6820 OY	6820 DZ	6820 DRAG
6820 X	.70452E+06						
6820 Y	-.31155E+05	.33116E+05					
6820 Z	-.29886E+06	-.15288E+05	.16949E+06				
6820 OX	-.29719E+03	.18419E+00	.92422E+02	.16470E+00			
6820 OY	-.28220E+03	.16395E+02	.12679E+03	.11297E+00	.16424E+00		
6820 DZ	-.72510E+03	.38832E+02	.34171E+03	.29466E+00	.29239E+00	.81388E+00	
6820 DRAG	.14836E+00	-.61493E-02	-.63494E-01	-.77262E-04	-.64775E-04	-.15291E-03	.10621E-06

G AND G OWEIGHTING MATRICES FOR VEHICLE 6820

ORBIT PLANE COORDINATE SYSTEM

.29549E+05						
-.30492E+04	.39486E+06					
0.	0.	.28070E+05				
.84176E+01	-.38108E+03	0.	.38510E+00			
-.34574E+02	.35672E+01	0.	-.98430E-02	.40454E-01		
0.	0.	.46071E+01	0.	0.	.32204E-01	

PARAMETER SET COORDINATE SYSTEM

.78319E-09						
-.24473E-10	.55341E-10					
-.29040E-09	.11061E-10	.18480E-09				
-.18272E-10	-.87267E-12	.32239E-11	.63768E-12			
-.16232E-11	.12518E-11	.67533E-11	.32176E-12	.59577E-12		
-.41458E-10	.20712E-11	.19294E-10	.82234E-12	.86483E-12	.25299E-11	

***** ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE *****

YEAR/MC/DY	X	ALPHA DELTA	A E	AF AG	MEAN ANOMALY ECCENTRIC ANOM	APOGEE RADIUS APOGEE HEIGHT
HR/MIN	Y	BETA	I	N	TRUE ANOMALY	PERIGEE RADIUS PERIGEE HEIGHT
SECONDS	Z	12IMUTH KADIUS	O U	L CHI	KEPLERIAN PER ANOMALY PER	0-00Y U-00Y
LATITUDE	XDOT	VELOCITY	TAU	PSI	NODAL PERIOD	
LONGITUDE	YDOT					
HEIGHT	ZDOT					
1370 / 6/26	7592292.341	43.413755895	21743202.958	-0.107332626829	355.7549988	3648.41715
17/4	7183127.603	60.643103119	0.1954638714	-0.0163359596314	355.67040241	212.67459
1.3979200	18581636.620	90.084563566	108.874728438	-0.679477592187	355.58591467	3508.52489
60.8072627	24094.8386435	221.285960530	185.982094698	299.062715447	89.4884613	72.782214
222.9763031	-771.9219982	21319414.735	117.325670862	-0.14577743567	89.6713960	2.8210805775
73.5841	-9593.4692113	25944.8301693	975.5900679	-1.35109474719	69.7913905	-2.9786973148

LEAST SQUARES PROCESS CONVERGED.

```

EXIT SEGMENT 84 AT          10.1 SECONDS.      .0 CP SECS.
ENTER SEGMENT 1. AT        10.1 SECONDS.      .1 CP SECS.
EXECUTION TIME FOR SEGMENT 84 WAS
EXECUTION TIME FOR SEGMENT 84 WAS

```

TRAJECTORY INTEGRATION FOR CASE 1

TIME (MPE)	TYPE	ASSOCIATED QUANTITIES	* PREDETERMINED EVENT TABLE *
------------	------	-----------------------	-------------------------------

*** TRAJECTORY START

```

* * * * *
SEG11 ENTRY TIME IS 10.1493C
* STEP DOUBLED
* STEP DOUBLED
*
* * * * *
T = 1067.273299
T = 1071.523299
*
* * * * *
H = .25000
H = .50000
*
* * * * *
NSTEP = 25
NSTEP = 41
*
* * * * *
NODE T = 1.080164820996E+04
CT = .500000000000E+00
*
* * * * *
- .21420970735E+08
- .133489802319E+04
*
* * * * *
H = .225564037775E+07
- .820446434921E+04
*
* * * * *
NSTEP = 30.951067894E-02
NSTEP = 24.3765058245E+05
*
* * * * *

```

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .213 SECONDS TO INTEGRATE A SPAN OF 19.5000 MINUTES ***

```

*** FROM 1064.C23 TO 1083.523 MINUTES FROM MIDNIGHT OF EPOCH ***

```

ENTER SEGMENT 81 AT 10.4 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .2 CP SECS.

ENTER SEGMENT 82 AT 10.4 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.

***** STAGE 6 *****

STAPASS	YEAR	MO	DAY	HR	MIN	SEC	RESIDUALS - EXTERNAL UNITS				MME		
343 18	1970	6	26	17	44	23.0000	--.101891E+04	RNG	--.753545E-02	AZ	--.124282E-01	EL	1064.333
						PREDICTED RESIDUALS	.872341E+03		0.		0.		
343 18	1970	6	26	17	44	19.2525	.491889E+01	SRR	0.		0.		1064.321
						PREDICTED RESIDUALS	.410377E+01		0.		0.		
343 18	1970	6	26	17	44	43.0000	--.897623E+03	RNG	--.758193E-01	AZ	--.210287E-01	EL	1064.667
						PREDICTED RESIDUALS	.779368E+03		0.		0.		
343 18	1970	6	26	17	44	39.2512	.751119E+01	SRR	0.		0.		1064.654
						PREDICTED RESIDUALS	.637908E+01		0.		0.		
343 18	1970	6	26	17	44	56.0000	.377287E+03	RNG	--.266531E-01	AZ	--.524774E-01	EL	1065.933
						PREDICTED RESIDUALS	.341341E+03		0.		0.		
343 18	1970	6	26	17	45	55.2392	.211965E+02	SRR	0.		0.		1065.921
						PREDICTED RESIDUALS	.163673E+02		0.		0.		
343 18	1970	6	26	17	46	36.0000	.997313E+03	RNG	--.420406E-01	AZ	--.651275E-01	EL	1066.600
						PREDICTED RESIDUALS	.745369E+03		0.		0.		
343 18	1970	6	26	17	46	35.2336	.103505E+02	SRR	0.		0.		1066.587
						PREDICTED RESIDUALS	.809252E+01		0.		0.		
343 18	1970	6	26	17	47	32.0000	.132342E+04	RNG	--.361294E-01	AZ	--.661090E-01	EL	1067.533
						PREDICTED RESIDUALS	.970787E+03		0.		0.		
343 18	1970	6	26	17	47	31.2308	.298569E+01	SRR	0.		0.		1067.521
						PREDICTED RESIDUALS	.244620E+01		0.		0.		

SUMMARY OF PREDICTED STATISTICS

STA	TYP	RMS	TYP	RMS	TYP	RMS
-----	-----	-----	-----	-----	-----	-----

343	RNG	.772325E+03	SRR	.890966E+01		
-----	-----	-------------	-----	-------------	--	--

PREDICTED RESIDUAL RMS =		.6865373079E+02
--------------------------	--	-----------------

ENTER SEGMENT 83 AT	10.5 SECONDS.	EXECUTION TIME FOR SEGMENT 82 WAS	.0 CP SECS.
---------------------	---------------	-----------------------------------	-------------

ITERATION NUMBER	1
10 MEASUREMENTS WERE USED IN THIS SOLUTION	

CURRENT SOLUTION IS

NAME	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
X 6820	.75922423410593E+07	.11517256E+04	.75934430666913E+07	.11507256E+04	.29643735E+32
6820	.7193127632643E+07	-.18282803E+07	.716312517743959E+07	-.18282803E+01	.26396697E+32
6820	.1850163662026E+08	-.83642102E+03	.18506010019004E+08	-.83642102E+03	.39504359E+32
6820	.24094838643523E+05	-.20868619E+00	.24094625957333E+05	-.20868619E+00	.12497134E+09
6820	-.77192159415084E+03	-.47311194E+00	-.77239500006648E+03	-.47301194E+00	.2825926E+32
DZ	-.9590469210553E+04	-.14318469E+01	-.959190000578932E+04	-.14383469E+01	.21595331E+30
DRAG	.92142136151769E-02	.14530978E-02	.936012349400169E-02	.14593479E-03	.60531016E+33

NAME	SIGMA ZBRD	SIGMA DENT	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMA0
X	.8393591E+03	.10234573E+04	.11507256E+04	.13709627E+01	.11243514E+01
Y	.8620	.24845168E+03	.18282803E+01	.19046705E+01	.73537279E+02
Z	.1819789E+03	.50041317E+03	-.83642102E+03	-.20316670E+01	-.16714600E+01
DX	.0583081E+01	.49220179E+00	-.20868619E+00	-.51421968E+01	-.42398563E+00
DY	.40530984E+00	.48656132E+00	-.47361194E+00	-.11670379E+01	-.37215276E+00
DZ	.90251315E+01	.13590583E+01	-.14300979E+01	-.15860355E+01	.13510359E+01
DRAG	.4315229E-03	.43152294E-03	.14508049E-03	.133612755E+01	.133612755E+01

RESIDUAL	RMS	=	.8777435238E+02
RESIDUAL	SOS	=	.7704361927E+05
APRIORI	RMS	=	0.
APRIORI	SOS	=	0.
TOTAL	SOS	=	.7704361827E+05
PREDICTED	SOS	=	.6706987746E+01

ATI

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6920 DRAG
6820 X	.29217E-01						
6820 Y	- .45035E-02	.19858E-01					
6820 Z	- .13208E-01	.50896E-02	.12439E-01				
6820 DX	.47.93E+01	- .77598E+00	.20907E+01	.43095E+04			
6820 DY	.14339E+J1	.15532E+01	- .87915E+00	- .18952E+03	.29645E+03		
6820 DZ	- .25336E+01	.64221E+00	- .59693E+00	- .19689E+04	.82272E+02	.93689E+03	
6820 DRAG	.86219E+J2	.13~25E+C3	.30750E+C3	.25321E+06	- .10100E+05	- .10545E+05	.25437E+08
ATE	.46653E+J2	- .1f948E+02	- .24734E+C2	.57163E+04	.21626E+04	- .34013E+04	- .516995E+05 .77043E+E5

ATA INVERSE

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.87911E+03						
6820 Y	.40469E+03	.80634E+03					
6820 Z	.69344E+03	-.39026E+03	.15006E+04				
6820 DX	-.17610E+01	-.17321E+00	-.26060E+01	.15610E-01			
6820 DY	-.52524E+01	-.76136E+01	.23439E+01	.43912E-02	.79855E-01		
6820 DZ	-.89767E+00	.65437E+00	-.31440E+01	.24655E-01	-.61675E-02	.45636E-01	
6820 DRAG	-.17762E-02	.50442E-03	-.53197E-02	-.13125E-04	-.79211E-05	-.16935E-04	.16428E-06

CORRELATION MATRIX

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	1.00000						
6820 Y	.48066	1.00000					
6820 Z	.59202	-.34789	1.00000				
6820 DX	-.47525	-.04881	-.52785	1.00000			
6820 DY	-.62687	-.94880	.20996	.12434	1.00000		
6820 DZ	-.14020	.10671	-.36853	.91354	-.10106	1.00000	
6820 DRAG	-.14780	.04383	-.33224	-.25912	-.19348	1.00000	

ENTER SEGMENT 84 AT 10.5 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.
 *** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 2. ***

YEAR/MC/DY	HR/MIN	SECONDS	LONGITUDE	HEIGHT	X	Y	Z	XDOT	YDOT	ZDOT	ALPHA	DELTA	BETA	AZIMUTH	RADIUS	VELOCITY	AF	AG	N	L	CHI	PSI	MEAN ANCHALY	ECCENTRC ANOM	TRUE ANOMALY	KEPLERIAN PER	PERIGEE HEIGHT	PERIGEE RADIUS	APOGEE HEIGHT	APOGEE RADIUS		
1970/ 6/26	17/44				7593443.067	7183125.774	60.640045934	43.405413599	21743146.308	.0107339327918	355.77927559	355.63515102	355.61020994	89.0891116	89.6707338	89.7028441	3648.41899															
1.3979200					15580800.199	24.94.6299573	221.280390669	108.875079899	.0670480122506	355.61020994	355.63515102	355.61020994	89.0891116	89.6707338	89.7028441	3648.41899																
60.8042163					222.9715608	-772.3950101	2131094.951	117.304259930	-.14577756705	355.61020994	355.63515102	355.61020994	89.0891116	89.6707338	89.7028441	3648.41899																
73.5339					-9591.9600579		25943.1793895	975.5843667	-1.35110311703																							

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN		
343	5	RNG	9.7E+02	4.9E+01	1.6E+02	5	AZ	4.4E-02	0.	-1.0E-02	5	EL	4.9E-02	0.
343	5	SRR	1.1E+01	1.4E+12	9.5E+00									

EXIT SEGMENT 84 AT 10.5 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .0 CP SECS.

ENTER SEGMENT 10 AT 10.15 SECONDS. EXECUTION TIME FOR SEGMENT 04 WAS .1 CP SECS.

***** TRAJECTORY INTEGRATION FOR CASE 1 *****

TIME(MME) TYPE ASSOCIATED QUANTITIES
1064.0233 TZERO
1083.1645 TSTOP

** TRAJECTORY START

***** * PREDETERMINED EVENT TABLE *

ENTRY TIME	IS	10.57600	T	1067.273299	H	=	.250000	NSTEP	=	25
STEP	DOUBLED		T	1071.523299	H	=	.500000	NSTEP	=	41
NODE	T =	.108016365486E+04		.214420373113E+08		.225573039794E+07				- .303975478830E-02
DT	=	.500000000L00E+00		.133527768483E+04		-.820457575669E+04				-.243964633952E+05

** TRAJECTORY TERMINATION

*** THIS CASE TOOK .214 SECONDS TO INTEGRATE A SPAN OF 19.5000 MINUTES ***

*** FROM 1064.023 TO 1083.523 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 01 AT 10.8 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .2 CP SECS.

ENTER SEGMENT 02 AT 10.9 SECONDS. EXECUTION TIME FOR SEGMENT 01 WAS .1 CP SECS.

***** STAGE 6 *****

STAPASS	YEAR	MO	DY	HR	MN	SEC	RESIDUALS - EXTERNAL UNITS	MME
343 18	1970	6	26	17	44	23.0000	.224450E+02 RNG	-282965E-01 AZ
343 18	1970	6	26	17	44	19.2525	.527920E-01 SRR	0. -106395E-01 EL
343 18	1970	6	26	17	44	43.0000	.157750E+02 RNG	0. -186839E-01 EL
343 18	1970	6	26	17	44	39.2512	-.334204E-01 SRR	0. 1064.654
343 18	1970	6	26	17	45	56.0000	-.684252E+01 RNG	-210743E-01 AZ
343 18	1970	6	26	17	45	55.2392	.457146E-01 SRR	0. 1065.921
343 18	1970	6	26	17	46	36.0000	-.974235E+01 RNG	-154507E-01 AZ
343 18	1970	6	26	17	46	35.2336	.734993E-01 SRR	0. 1066.600
343 18	1970	6	26	17	47	32.0000	-.472401E+01 RNG	-461330E-01 AZ
343 18	1970	6	26	17	47	31.2318	-.582066E-01 SRR	0. 1067.533
343 18	1970	6	26	17	47	31.2318	-.582066E-01 SRR	0. 1067.521

ENTER SEGMENT 83 AT 10.9 SECONDS. EXECUTION TIME FOR SEGMENT 82 WAS .0 CP S=CS.

ITERATION NUMBER 2
10 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	X	Y	Z	DX	DY	DZ	DRAG	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820	X							.7593443666913E+07	-.17473217E+00	.75934428919591E+07	.1150559E+04	.29652415E+02
6820	Y							.71831257743959E+00	-.75528587E+00	.71831250091107E+00	-.25935742E+01	.28380447E+02
6820	Z							.185808 193004E+08	-.22954129E+06	.18580795969463E+08	-.83665056E+03	.39509778E+02
6820	DX							.24994629957333E+05	-.22630740E-02	.24994632229407E+05	-.20642312E+00	.12498010E+09
6820	DY							-.7723950108648E+03	.10204461E-02	-.77239396964038E+03	-.47199149E+00	.28259765E+09
6820	DZ							-.9591901578832E+04	.34716790E-02	-.95918965862341E+04	-.14273752E+01	.21595791E+09
6820	DRAG							.93601234480069E-02	-.76051947E-06	.93593628885378E-02	-.14514927E-03	.40531424E-03

NAME	X	Y	Z	DX	DY	DZ	DRAG	SIGMA ZB50	SIGMA DENT	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMA0
6820	X							.83935591E+03	.11234573E+04	.11505593E+04	.13707545E+01	.11241806E+01
6820	Y							.18197897E+03	.24845163E+03	-.25935742E+01	-.14252760E-01	-.10438948E-01
6820	Z							.41169347E+03	.51041317E+03	-.83665056E+03	-.21322176E+01	-.16719196E+01
6820	DX							.40583091E+00	.49220174E+00	-.20642312E+00	-.50864328E+00	-.41938777E+00
6820	DY							.40530758E+00	.49655137E+00	-.47159149E+00	-.11645202E+01	-.97035550E+00
6820	DZ							.90215315E+00	.11590583E+01	-.14273752E+01	-.15821873E+01	.13477778E+01
6820	DRAG							.43152294E-03	.43152294E-03	.14514927E-03	.33636514E+00	.33636514E+00

RESIDUAL RMS = .6140155352E+00
RESIDUAL SOS = .37701577E+01
APRIORI RMS = .664943878E+00
APRIORI SOS = .309502136E+01
TOTAL SOS = .6865170811E+01
PREDICTED SOS = .6855143305E+01

ATA

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.29190E-01						
6820 Y	-.44992E-02	.19864E-01					
6820 Z	-.13198E-01	.50833E-02	.12434E-01				
6820 DX	.47059E+01	-.37609E+00	.20929E+01	.43090E+04			
6820 DY	.14332E+01	.15533E+01	-.87924E+00	-.18987E+03	.29638E+03		
6820 DZ	-.25322E+01	.64200E+00	-.59786E+03	-.19687E+04	.82292E+02	.93600E+03	
6820 DRAG	.86061E+02	.13439E+03	.30760E+03	.25316E+06	-.10096E+05	-.10543E+06	.25438E+08
ATB	.46266E-02	-.13627E-01	-.29084E-02	.18222E+01	-.10706E+01	-.99047E+00	-.11216E+02

.37792E+1

ATA INVERSE

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.87927E+03						
6820 Y	.40464E+03	.87545E+03					
6820 Z	.69369E+03	-.38972E+03	.15610E+04				
6820 DX	-.17610E+01	-.17305E+00	-.26069E+01	.15620E-01			
6820 DY	-.52532E+01	-.76796E+01	.23425E+01	.43922E-02	.79861E-01		
6820 DZ	-.89736E+00	.65443E+00	-.31448E+01	.24657E-01	-.61666E-02	.46638E-01	
6820 DRAG	-.17784E-02	.58270E-03	-.53233E-02	-.13125E-04	-.79253E-05	-.16948E-04	.16428E-06

CORRELATION MATRIX

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	1.00000						
6820 Y	.48883	1.00000					
6820 Z	.59210	-.34756	1.00000				
6820 DX	-.47519	-.04879	-.52793	1.00000			
6820 DY	-.62689	-.94880	.20980	.12436	1.00000		
6820 DZ	-.14313	.10678	-.36857	.91355	-.10104	1.00000	
6820 DRAG	-.14797	.04370	-.33242	-.2591	-.16919	-.19362	1.00000

ENTER SEGMENT 84 AT 10.9 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS
 *** ORBITAL ELEMENTS FOR VEHICLE 1 FOR ITERATION 3. ***

.0 CP SECS.

YEAR/MO/DY	X	ALPHA	A	AF	MEAN ANOMALY	APOGEE RADTUS
HR/MIN	Y	DELTA	E	AG	ECCENTRC ANOM	APOGEE HEIGHT
SECONDS	Z	BETA	I	N	TRUE ANOMALY	PERIGEE RADTUS
LATITUDE	XDOT	AZIMUTH	O	L	KEPLERIAN PER	PERIGEE HEIGHT
LONGITUDE	YDOT	RADIUS	U	CHI	ANOMALY PER	O-NOT
HEIGHT	ZDOT	VELOCITY	TAU	PSI	NODAL PERIOD	U-NOT
1970/ 6/26	7593442.892	43.489411209	21743146.599	.0107338089766	355.77973727	3648.44912
17/44	7183125.009	60.648047161	.01955756163	-.0163492876864	355.69563177	212.71563
1.3979200	18580799.969	90.084121532	108.875078675	.0670480199052	355.61068986	3508.47429
60.8042175	24094.6322204	221.286989441	185.982347975	299.065864625	89.488134	72.73481
222.9719584	-772.3939896	21319094.431	117.303779372	-.14577752670	89.6773556	2.8211591892
73.5308	-9591.8965862	25945.1801773	975.5842532	-1.39113308952	89.7020459	-2.8786364671

.0 CP SECS.

EXIT SEGMENT 84 AT 10.9 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS

ENTER SEGMENT 10 AT 11.0 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .0 CP SECS.
 ***** TRAJECTORY INTEGRATION FOR CASE 1 *****

* PREDETERMINED EVENT TABLE *

TIME(MME) TYPE
 1064.0233 TZERO
 1083.1645 TSTOP

*** TRAJECTORY START

SEG11 ENTRY TIME IS 10.98900
 STEP DOUBLED
 STEP DOUBLED
 NODE T = .108016365736E+04
 DT = .500000000000E+00
 T = 1067.273299 H = .250000 NSTEP = 25
 T = 1071.523299 H = .500000 NSTEP = 41
 .21420405147E+08 .225573066533E+07 -.303506639194E-02
 .133527982041E+04 -.620457386845E+04 -.243964682024E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .213 SECONDS TO INTEGRATE A SPAN OF 19.5000 MINUTES ***

*** FROM 1064.023 TO 1083.523 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 81 AT 11.2 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .2 CP SECS.

ENTER SEGMENT 82 AT 11.3 SECONDS. EXECUTION TIME FOR SEGMENT 81 WAS .1 CP SECS.

***** STAGE 6 *****

STAPASS	YEAR	MO	DY	HR	MM	SEC	RESIDUALS - INTERNAL UNITS	MME
343 18	1970	6	26	17	46	20.0000	.229047E+02 RNG	1064.333
343 18	1970	6	26	17	46	19.2525	.561860E-01 SRR	1064.321
343 18	1970	6	26	17	46	40.0000	.163067E+02 RNG	1064.667
343 18	1970	6	26	17	46	39.2512	.297533E-01 SRR	1064.654
343 18	1970	6	26	17	45	56.0000	.622021E+01 RNG	1065.933
343 18	1970	6	26	17	45	55.3392	.419391E-01 SRR	1065.921
343 18	1970	6	26	17	46	36.0000	.331809E+01 RNG	1066.600
343 18	1970	6	26	17	46	35.2336	.685414E-01 SRR	1066.587
343 18	1970	6	26	17	47	32.0000	.450345E+01 RNG	1067.533
343 18	1970	6	26	17	47	31.2368	.606420E-01 SRR	1067.521

ENTER SEGMENT 83 AT 11.3 SECONDS. EXECUTION TIME FOR SEGMENT 02 WAS .0 CP SECS.

ITERATION NUMBER 3
10 MEASUREMENTS WERE USED IN THIS SOLUTION
CURRENT SOLUTION IS

NAME	X	Y	Z	DX	DY	DZ	DRAG	CURRENT VALUE	CORRECTION	NEW VALUE	TOTAL CORR.	SIGMA
6820	X							.75934428519591E+07	.60785110E-05	.75934428919652E+07	.11503509E+04	.29652406E+02
6820	Y							.71831251091100E+07	.10559320E-03	.7183125092156E+07	-.25934606E+01	.28380447E+02
6820	Z							.18580759969463E+08	-.26003321E-03	.18580759969203E+08	-.83665082E+03	.39509776E+02
6820	DX							.24094632221407E+05	-.10117911E-05	.24094632219395E+05	-.20642413E+00	.12498001E+00
6820	DY							-.7723939891228E+03	-.85049487E-06	-.77239398949087E+03	-.47199235E+00	.28259768E+00
6820	DZ							-.95915965062041E+04	-.27485479E-05	-.95915965089527E+04	-.14273780E+01	.21595792E+00
6820	DRAG							.93593628805378E-02	.42636614E-09	.93593633149039E-02	.14514970E-03	.40531414E-03

NAME	X	Y	Z	DX	DY	DZ	DRAG	SIGMA ZERO	SIGMA DENT	TOTAL CORR.	T.C./SIGMA0	T.C./SIGMA0
6820	X							.83935591E+03	.10234573E+04	.11505509E+04	.13707545E+01	.11241807E+01
6820	Y							.18197891E+03	.24945168E+03	-.25934606E+01	-.14251480E-01	-.10438523E-01
6820	Z							.41169344E+03	.50041317E+03	-.83665082E+03	-.20322182E+01	-.16719201E+01
6820	DX							.40583081E+00	.49220109E+00	-.20642413E+00	-.50864577E+00	-.41938962E+00
6820	DY							.40530584E+00	.48656132E+00	-.47199235E+00	-.11645223E+01	-.37005727E+00
6820	DZ							.90215315E+00	.10590583E+01	-.14273780E+01	-.15821903E+01	-.13477804E+01
6820	DRAG							.43152294E-03	.43152294E-03	.14514970E-03	.33636613E+00	.33636613E+00

RESIDUAL RMS = .6130680263E+00
RESIDUAL SOS = .3758524040E+01
APRIORI RMS = .6651072091E+00
APRIORI SOS = .3096573196E+01
TOTAL SOS = .6855097244E+01
PREDICTED SOS = .6855097244E+01

***** LEAST SQUARES PROCESS CONVERGED *****

ATA

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.29198E-01						
6820 Y	-.44992E-02	.19864E-01					
6820 Z	-.13198E-01	.50833E-02	.12434E-01				
6820 DX	.47059E+01	-.27679E+00	.20929E+01	.43090E+04			
6820 DY	.14332E+01	.15533E+01	-.87923E+00	-.18967E+03	.29638E+03		
6820 DZ	-.25322E+01	.64200E+00	-.59786E+03	-.19687E+04	.82292E+02	.93680E+03	
6820 DRAG	.86061E+02	.13439E+03	.38760E+03	.25316E+06	-.10096E+05	-.10543E+06	.25438E+08
6820 ATB	.41392E-05	-.15072E-05	-.23650E-05	.72438E-03	.10835E-03	-.49068E-03	-.12140E-01

.37989E+11

ATA INVERSE

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	.87927E+03						
6820 Y	.40464E+03	.60545E+03					
6820 Z	.69369E+03	-.30972E+03	.15610E+04				
6820 DX	-.17610E+01	-.37305E+00	-.26069E+01	.15629E-01			
6820 DY	-.52532E+01	-.76096E+01	.23425E+01	.43922E-02	.79864E-01		
6820 DZ	-.89735E+00	.65443E+00	-.31448E+01	.24657E-01	-.61666E-02	.46638E-01	
6820 DRAG	-.17784E-02	.30270E-03	-.53233E-02	-.13125E-04	-.79253E-05	-.16948E-04	.16428E-06

CORRELATION MATRIX

	6820 X	6820 Y	6820 Z	6820 DX	6820 DY	6820 DZ	6820 DRAG
6820 X	1.00000						
6820 Y	.48083	1.00000					
6820 Z	.59210	-.34756	1.00000				
6820 DX	-.47519	-.04879	-.52793	1.00000			
6820 DY	-.62689	-.94880	.20980	.12436	1.00000		
6820 DZ	-.14013	.10678	-.36857	.91355	-.10104	1.00000	
6820 DRAG	-.14797	.04370	-.33242	-.25910	-.06919	-.19362	1.00000

ENTER SEGMENT 84 AT 11.3 SECONDS. EXECUTION TIME FOR SEGMENT 83 WAS .0 CP SECS.
 ATA INVERSE UPDATED TO 1000.16 MINUTES FROM MIDNIGHT OF EPOCH

6020 X	6020 Y	6020 Z	6020 DX	6020 DY	6020 DZ	6020 DRAG
.35499E+05						
.10500E+05	.45207E+05					
.39262E+05	.56209E+04	.46072E+05				
.72910E+02	.31827E+02	.79375E+02	.15238E+00			
.17093E+02	.35478E+02	.15014E+02	.42516E-01	.30491E-01		
.37517E+02	.63646E+01	.43562E+02	.76353E-01	.14674E-01	.42439E-01	
.33922E-01	-.11780E-01	-.25810E-01	-.67130E-04	-.16543E-04	-.19563E-04	.16428E-06

G AND G DEWEIGHTING MATRICES FOR VEHICLE 6020

ORBIT PLANE COORDINATE SYSTEM

.43466E+04			
-.40126E+04	.40423E+04		
0.	0.	.41290E+04	
.99574E+01	-.86330E+01	0.	.25101E-01
-.50857E+01	.46549E+01	0.	-.11651E-01
0.	0.	.49930E+01	0.
			.59505E-02
			.99104E-02

PARAMETER SET COORDINATE SYSTEM

.93055E-11			
.29501E-11	.10030E-10		
.86308E-11	.84679E-12	.92512E-11	
.12938E-11	.44673E-12	.11146E-11	.19053E-12
.28967E-12	.75130E-12	.10441E-12	.43619E-13
.65715E-12	.56209E-13	.64756E-12	.91182E-13
			.85921E-13
			-.42134E-15
			.52310E-13

**** ORBITAL ELEMENTS FOR VEHICLE 1 FOR NEXT DATA STAGE ****

YEAR/MO/DY	X	Y	Z	HR/MIN	SECONDS	LONGITUDE	HEIGHT	ALPHA	BETA	AZIMUTH	RADIUS	VELOCITY	TAU	AF	AG	AN	LN	CHI	PSI	MEAN ANOMALY	ECCENTRIC ANOM	APOGEE RADIUS	PERIGEE RADIUS	PERIGEE HEIGHT	U-DOT
1970/ 6/26	21442108.010	2255315.104	-1229.335	9.8700000	-0.032009	1333.7543378	101.5205828	6.004383877	-0.03266904	198.852063799	21560398.619	25688.5299652	1065.5699717	0.122634548163	-0.172617768107	0.066108839665	3.908663117	-1.4627750850	-1.39045372068	58.51440816	59.55167132	3662.97539	226.93318	3518.87238	74.8217
18/ 0																				58.51440816	59.55167132	3662.97539	226.93318	3518.87238	74.8217
104.4612																				58.51440816	59.55167132	3662.97539	226.93318	3518.87238	74.8217

LEAST SQUARES PROCESS CONVERGED.

TOTAL EDIT SUMMARY

STA	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN	N TYP	RMS	RMS/SIG	MEAN
343	5 RNG	1.4E+01	6.8E-01	3.9E+00	5 AZ	5.4E-02	0.	-3.7E-02	5 EL	3.9E-02	0.	-3.5E-02
343	5 SRR	5.3E-02	5.3E-01	1.5E-02								

TYPE	SYMB	MINIMUM	DELTA	MEAN	MAXIMUM	STATION	PAGE
RNG	0	-.22439559E+02	.52546681E+00	.38337018E+01	.30107122E+02	1	1
AZ	1	-.11550817E+00	.15718191E-02	-.36917213E-01	.41673742E-01		
EL	2	-.73484652E-01	.71150079E-03	-.34909652E-01	.66539697E-03		
SRR	3	-.86777451E-01	.20406317E-02	.15254093E-01	.11728568E+00		
63860	*******
63870	*******
63880	*******
63890	*******
63900	*******
63910	*******
63920	*******
63930	*******
63940	*******
63950	*******
63960	*******
63970	*******
63980	*******
63990	*******
64000	*******
64010	*******
64020	*******
64030	*******
64040	*******
64050	*******

EXIT SEGMENT 84 AT 11.4 SECONDS. EXECUTION TIME FOR SEGMENT 84 WAS .1 CP SECS.

NODE	T =	.1616216850000000	.213994367270E+08	.264428399292E+07	.243835445813E-01
DT =		.1000000000000000	.14808981692E+04	-.617555867226E+04	-.242995496028E+05
NODE	T =	.166408354981E+04	-.217958962602E+08	-.273074395062E+07	-.212157618508E-01
DT =		.1000000000000000	-.550046114581E+03	.613782797751E+04	.238527373047E+05
NODE	T =	.170786130670E+04	.213915999808E+08	.271350556792E+07	-.114127474058E+00
DT =		.1000000000000000	.150524649161E+04	-.617124063287E+04	-.242982391742E+05
NODE	T =	.175372245239E+04	-.217843490327E+08	-.279665859553E+07	-.932234178636E-02
DT =		.1000000000000000	-.5175642917481E+03	.613756447812E+04	.238552246979E+05
NODE	T =	.179749767323E+04	.213834988072E+08	.277846378426E+07	-.131203734526E+00
DT =		.1000000000000000	.152916060097E+04	-.816674010473E+04	-.242971469914E+05

*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .872 SECONDS TO INTEGRATE A SPAN OF 737.0000 MINUTES ***

*** FROM 1064.023 TO 1801.023 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 50 AT 12.3 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .9 CP SECS

*** TRACE66 EPHEMERIS OUTPUT KEY ***

DATE,...	HE,MM,ST,OT	X,XO	X,XD - BF	ADBRV	LAT,...	REV,...	REMARK
YR/MO/DAY	MIN FROM EPOCH	X (FT)	X (FT)	ALPHA (DEG)	LATITUDE (DEG)	REV COUNT	.
HR/MIN	MIN FROM MIDNIGHT	Y (FT)	Y (FT)	DELTA (DEG)	LONGITUDE (DEG)	PERIOD	.
SEC	SEC FROM MIDNIGHT	Z (FT)	Z (FT)	BETA (DEG)	ALTITUDE (NH)	PERIOD-DECAY	.
	STEP SIZE (MIN)	XD (FT/SEC)	XD (FT/SEC)	AZIMUTH (DEG)	S-VEH-LAT (DEG)	NDD-REG	.
IT	UTC - IT	YD (FT/SEC)	YD (FT/SEC)	R (FT)	I (DEG)		
	UT1 - IT	ZD (FT/SEC)	ZD (FT/SEC)	V (FT/SEC)	O (DEG)		

* * * ECI TRAJECTORY * * *

*** CASE 1

*** EPOCH PRINT

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADBARV	LAT,.. BF	REV,...
70/ 6/26	0.00000	.759344289E+07	-.764806414E+07	43.40 941121	60.80421747	.31365
17/44	1064.02330	-.712312501E+07	-.712494034E+07	60.64004716	222.97195040	0.00000
1.39792	63841.39792	.185808000E+08	.185808000E+08	90.88412153	73.53052355	0.00000
	.12500	.240946322E+05	-.246075916E+05	221.28608944	60.80078090	0.00000
IT	0.00000	-.772393990E+03	.151403765E+04	.2131994E+08	108.87507868	
	0.00000	-.959189659E+04	-.959189659E+04	.25945180E+05	5.54499517	
A =	.21743147E+08	MEAN ANCH =	.35577974E+03	APOGEE =	.36464491E+04	
E =	.19557962E-01	ECCENTRIC =	.35569563E+03	HEIGHT =	.21270963E+03	
I =	.10887508E+03	TRUE ANCH =	.35561069E+03	PERIGEE =	.35084743E+04	
O =	.18598235E+03	KEPL PER =	.89488113E+02	HEIGHT =	.72734801E+02	
U =	.11730378E+03	ANOM PER =	.89670736E+02	O-DOT =	.28211592E+01	
TAU =	.97558425E+03	NODL PER =	.89702846E+02	U-DOT =	-.20786365E+01	

*** REQUESTED PRINTS

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADBARV	LAT,.. BF	REV,...
70/ 6/26	16.14036	.214420405E+08	-.215527613E+08	6.00549935	.30000006	.50000
18/ 9	1080.16366	.225573007E+07	-.572626326E+06	.00000006	181.52190964	0.00000
9.81942	64809.81942	.230045380E-01	.230045380E-01	88.95264149	104.45724719	0.00000
	.50000	.133127985E+04	-.731569387E+03	198.85206376	.00000006	0.00000
IT	0.00000	.620457386E+04	.985550169E+04	.21560367E+08	108.84336396	
	0.00000	-.243306460E+05	-.243306460E+05	.25688558E+05	1.52198952	

DELTA NODE = -.052 DELTA V = -.0009

DATE,...	ME,MM,ST,DT,..	X,XD	X,XD - BF	ADBARV	LAT,.. BF	REV,...
70/ 6/26	105.83642	.14353908E+08	-.201569485E+08	9.17996209	-.00000288	1.50000
19/29	1169.85972	.232104389E+07	.765249304E+07	-.00000236	159.21096388	0.00000
51.58320	70191.58320	-.107809356E+01	-.137809356E+01	88.95279537	104.50992605	0.00000
	1.00000	.136012187E+04	.306461904E+04	.98.85196623	-.00000288	0.00000
IT	0.00000	-.820007404E+04	.939502721E+04	.21560607E+08	108.85222696	
	.00000	-.243354003E+05	-.243354003E+05	.25687422E+05	339.21096495	

DELTA NODE = -.068 DELTA V = -.0011				DELTA NODE = -.092 DELTA V = -.0015				DELTA NODE = -.107 DELTA V = -.0018				DELTA NODE = -.109 DELTA V = -.0018											
DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE	DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE								
70/ 6/26	195.52513	.214287+73E+08	-.157433235E+08	6.35324341	-.0001173	2.50000	0.00000	70/ 6/26	285.28599	.214216120E+08	-.897364123E+07	6.52839148	-.0001158	3.50000	0.00000								
20/ 59	1259.54843	.238591366E+07	-.147319911E+08	-.00001165	136.90068710	89.69142	0.00000	22/ 29	1349.22919	.245143774E+07	-.196053251E+08	114.59425589	114.59425589	89.68236	0.00000								
32.90578	75572.90578	-.438376636E+01	-.438376636E+01	88.55481801	104.58844613	0.00000	0.00000	13.75138	80953.75138	-.432756937E+01	-.432756937E+01	88.55815109	104.63123814	-.00905	0.00000								
IT	1.00000	.138387453E+04	.640178899E+04	198.85063321	-.00001173	.17450	0.00000	IT	1.00000	.140734137E+04	.877973059E+04	198.84997498	-.00011157	.17289	0.00000								
	0.00000	-.8139502954E+04	.752698666E+04	.21567164E+08	106.84898891				0.00000	-.819129459E+04	.453222152E+04	.21561424E+08	106.84274223										
	..00000	-.243043113E+05	-.243043113E+05	.25566050E+05	316.90068477				3.30300	-.243033423E+05	-.243033420E+05	.255684898E+05	294.59425581										
DELTA NODE = -.068 DELTA V = -.0011								DELTA NODE = -.107 DELTA V = -.0018								DELTA NODE = -.109 DELTA V = -.0018							
DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE	DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE								
70/ 6/26	195.52513	.214287+73E+08	-.157433235E+08	6.35324341	-.0001173	2.50000	0.00000	70/ 6/26	374.87599	.214141869E+08	-.862266509E+06	6.70494891	-.00010271	4.50000	0.00000								
20/ 59	1259.54843	.238591366E+07	-.147319911E+08	-.00001165	136.90068710	89.69142	0.00000	23/ 58	1438.89929	.251746366E+07	-.215444081E+08	-.00000269	92.29191156	89.67252	0.00000								
32.90578	75572.90578	-.438376636E+01	-.438376636E+01	88.55481801	104.58844613	0.00000	0.00000	53.95759	86333.95759	-.181202333E+01	-.101202333E+01	88.55875049	104.66947350	-.00984	0.00000								
IT	1.00000	.138387453E+04	.640178899E+04	198.85063321	-.00001173	.17450	0.00000	IT	1.00000	.143219283E+04	.984213692E+04	198.84909180	-.00010271	.17519	0.00000								
	0.00000	-.8139502954E+04	.752698666E+04	.21567164E+08	106.84898891				0.00000	-.818515932E+04	.861069873E+03	.21561656E+08	108.83250828										
	..00000	-.243043113E+05	-.243043113E+05	.25566050E+05	316.90068477				0.00000	-.243022270E+05	-.243022270E+05	.255683579E+05	272.29191248										
DELTA NODE = -.068 DELTA V = -.0011								DELTA NODE = -.107 DELTA V = -.0018								DELTA NODE = -.109 DELTA V = -.0018							
DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE	DATE,...	ME,MM,ST,DT,...	X, XD	X, XD - BF	ADBARV	LAT,...	REV,...	DSC NODE								
70/ 6/27	464.53870	.214068712E+08	.737823384E+07	6.88074863	.00010451	5.50000	0.00000	70/ 6/27	464.53870	.214068712E+08	.737823384E+07	6.88074863	.00010451	5.50000	0.00000								
1/28	1528.56200	.258295298E+07	.232604898E+08	.00000448	69.98936552	89.66746	0.00000	1/28	1528.56200	.258295298E+07	.232604898E+08	.00000448	69.98936552	89.66746	0.00000								
33.72002	5313.72002	.168762171E+01	.168762171E+01	88.55920725	104.74867934	-.00706	0.00000	33.72002	5313.72002	.168762171E+01	.168762171E+01	88.55920725	104.74867934	-.00706	0.00000								
IT	1.00000	.145685981E+04	.943171991E+04	198.84799115	.00010451	.17674	0.00000	IT	1.00000	.145685981E+04	.943171991E+04	198.84799115	.00010451	.17674	0.00000								
	0.00000	-.817983090E+04	-.293826764E+04	.21562139E+08	108.81834109				0.00000	-.817983090E+04	-.293826764E+04	.21562139E+08	108.81834109										
	..00000	-.243043113E+05	-.243043113E+05	.25566050E+05	316.90068477				..00000	-.243043113E+05	-.243043113E+05	.25566050E+05	316.90068477										

DELTA NODE = -.102 DELTA V = -.0017

DATE, ... ME, MM, ST, DT, ...
 70/ 6/27 554.19355
 2/58 1618.21685
 13.01102 10693.01102
 1.00000
 0.00000
 0.00000
 0.00000

X, XD
 .213594367E+08
 .264828417E+07
 .804616523E+00
 .148089974E+04
 .81755575E+04
 .242595496E+05

X, XD - BF
 .145148497E+08
 .159457968E+08
 .804616523E+00
 .761081800E+04
 -.629825321E+04
 -.242995496E+05

ADBARV
 7.05476158
 .00000214
 88.96119198
 198.84921806
 .21562603E+08
 .25680749E+05

LAT, ... BF
 .00000215
 47.68950143
 104.83843728
 .00000215
 108.80199091
 227.68960070

REV, ...
 6.50800
 89.65779
 -.00767
 .17476

OSC MODE
 6.50800
 89.65779
 -.00767
 .17476

DELTA NODE = -.082 DELTA V = -.0014

DATE, ... ME, MM, ST, DT, ...
 70/ 6/27 643.83821
 4/27 1707.86151
 51.69044 16071.69044
 1.00000
 0.00000
 0.00000

X, XD
 .213591600E+08
 .271505225E+07
 .195712610E+01
 .150524536E+04
 .817124078E+04
 .242982392E+05

X, XD - BF
 .194798050E+08
 .924628832E+07
 .105712610E+01
 .465155802E+04
 .871542997E+04
 -.242982392E+05

ADBARV
 7.22939829
 .00000281
 88.96243023
 198.85097599
 .21563016E+08
 .25679552E+05

LAT, ... BF
 .00000283
 25.39162634
 104.89325314
 -.0000283
 108.85076564
 205.39162729

REV, ...
 7.50800
 89.64801
 -.08978
 .17482

OSC MODE
 7.50800
 89.64801
 -.08978
 .17482

DELTA NODE = -.050 DELTA V = -.0008

DATE, ... ME, MM, ST, DT, ...
 70/ 6/27 733.47438
 5/57 1797.49768
 29.86058 21449.86058
 1.00000
 0.00000
 0.00000

X, XD
 .213834991E+08
 .278846226E+07
 .465457882E+01
 .152915515E+04
 .816474083E+04
 .242971470E+05

X, XD - BF
 .215317973E+08
 .116429879E+07
 .465457882E+01
 .998256937E+03
 .982865865E+04
 -.242971470E+05

ADBARV
 7.40324268
 -.00001237
 88.96437666
 198.85127777
 .21563253E+08
 .25679499E+05

LAT, ... BF
 .00001245
 3.09516673
 104.93226575
 -.00001245
 108.84890896
 183.09517795

REV, ...
 8.50800
 89.63890
 -.00918
 .17436

OSC MODE
 8.50800
 89.63890
 -.00918
 .17436

DELTA NODE = .025 DELTA V = -.89.6236

TRAJECTORY TERMINATION

A = .21780897E+08 MEAN ANOM = .59888710E+02 APOGEE = .36578764E+74
 E = .20420730E-01 ECCENTRIC = .70994953E+02 HEIGHT = .22200649E+93
 I = .10888225E+03 TRUE ANOM = .72104969E+02 PERIGEE = .35114730E+74
 O = .18740337E+03 KEPL PER = .89721271E+02 HEIGHT = .75603138E+02
 U = .11819824E+03 ANCH PER = .89595851E+02 O-DCT = .28010077E+71
 TAU = .17826052E+04 NOCL PER = .89628018E+02 U-DCT = -.20714803E+91

*** END OF TRAJECTORY ***

EXIT SEGMENT 50 AT 12.6 SECONDS. EXECUTION TIME FOR SEGMENT 50 WAS .2 CP SECS.

TRACE-66 (A0104A)

[illegible]

(92/21/74)

MODEL DATA
DITIN 4
END

IMULTV2

LEMSP1

CARD 1
CARD 2

} ①

***** GENERAL PERTURBATIONS GRAVITY MODEL *****
GM = .553041774E-02 ER**3/MIN**2 = .1407660855E+17 FT**3/SEC**2 = .398604930E+15 M**3/SEC**2

***** ZONAL HARMONICS *****

EJ2 = .1082549000E-02 EJ3 = -.243500000000E-05 EJ4 = -.1232000000E-05

***** PHYSICAL CONSTANTS *****
GM(ER**3/MIN**2) = .953039350E-02 OMEGA(RAD/MIN) = .437526910E-02 GMLAT(DEG) = .763000000E+02
GNKM(KM**3/SEC**2) = 0. OMEGA(RAD/MIN) = .437526910E-02 GMLNG(DEG) = .291000000E+03
SGM(ER**3/MIN**2) = .680232550E-04 OMEGL(RAD/MIN) = 0. AM(ER) = .272506277E+03
ERFT(FT/ER) = .209257300E+08 ERKM(KM/ER) = .637616490E+04 ERNM(NM/ER) = .344393360E+04
FTKM(FT/KM) = .328083990E+04 FTNM(FT/NM) = .607611550E+04 AE(ER) = .100000000E+01
GSUB0(FT/SEC**2) = .321740000E+02 DGREE(DEG) = .572957795E+02 SLT(ER/MIN) = .202017630E+04
CKEP = .100000000E-10 F = .335232907E-02 PI = .314159265E+01

***** INPUT/OUTPUT CONVERSION FACTORS *****

DF(I/O-ER) = .209257308E+8 VF(I/O-ER/MIN) = .34876210E+06 AF(I/O-ER/MIN**2) = .58127050E+04

***** INTEGRATION INPUTS *****

ICENT = 1 NSTEP = 2
IR = 0 ER = .10000000E-09
HMIN = .15625000E-01 HMAX = .64000000E+02 H0 = .10000000E+01

***** SPECIAL OPTIONS *****

TAPE2 = 0 TAPE7 = 0 TELEM = 0 PTAPE = 0 NPDOT = 0
PRHO = 0 NODPR = 0 CLASS = 0 LEMSP = 1 PTNS = 10.00

REFERENCE
SECTION

DESCRIPTION

ITEM

1 Card images of the input MODEL data:

ITIN
MULTV
LEMSP

2.1
2.1.4
2.1.4

***** CRASH ALTITUDE TABLE *****
(IN FT)

ECI CRASH ALTITUDE = .300000000E+06 PCI CRASH ALTITUDE = .300000000E+04

***** INTERPLANETARY CRASH ALTITUDES TABLE *****
(IN FT)

BODY(1) CRASH ALTITUDE = .300000000E+06 BODY(2) CRASH ALTITUDE = 0.
 BODY(3) CRASH ALTITUDE = .300000000E+04 BODY(4) CRASH ALTITUDE = 0.
 BODY(5) CRASH ALTITUDE = 0. BODY(6) CRASH ALTITUDE = 0.
 BODY(7) CRASH ALTITUDE = 0.

***** STATION LOCATIONS *****
 STATION SIG REF RA-RBF DATUM TYPE LATITUDE LONGITUDE HEIGHT P 0

VTS -0 1 1 -0 -0 .34700000E+02 -.12050000E+03 -0.
 AND -0 1 1 -0 -0 .36800000E+02 -.75800000E+02 -0.
 OUM -0 -0 -0 -0 -0 -0. -0.

ENTER SEGMENT 01 AT .2 SECONDS. EXECUTION TIME FOR SEGMENT 0 WAS .2 CP SECS.

***** VEHICLE DATA FOR CASE 1 *****

IVEHID1	IBTAPE3	ICTYP2	CARD
IYEAR -1973	IMNTH 1	IDAY 1	CARD 1
IC -96.7506126	3.7345133	88.2980214	CARD 2
PTIM 0	134623991.	10361.7713	CARD 3
PTIM 0	1	0	CARD 4
PTIM 0	240		CARD 5
END			CARD 6
			CARD 7

ITEM	DESCRIPTION	REFERENCE SECTION
2	Printout of station locations as input. If CLASS #0, the actual locations are left blank. This example has a "dummy" station DUM, which is used to illustrate Data Set Types A and R	4 Item 4
3	Card images of input VEHICLE data. Emphasis is on the variable associated with simultaneous-vehicle data generation (ITIN=4), the others having been discussed earlier:	
	BTAPE	11.4

Preceding page blank

EPOCH
YR/MO/DAY
1973/ 1/ 1
TZME,HR,MIN,SEC
0.
0.
0.
0.
0.

INITIAL CONDITIONS
A,O,B,A,R,V
-46738612600E+02
-37344513300E+01
-86298821400E+02
-86672905700E+02
-13462399100E+09
-10361771300E+05
A,E,I,O,U,TAU
-13833420060E+09
-48000229570E-01
-49999999902E+03
-21500001307E+03
-3587404867E+03
-10426790660E+03
AF,AG,N,L,CHI,PSI
-33262674454E-01
-22217399790E-01
-4176749493E-02
-2599335223E+03
-2504286151E-01
-3576694485E-01

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

***** VEHICLE DATA FOR CASE 2 *****

IVEHID3
IC 280.619783
END 22.9501321
71.0381996
166569812.
8201.03786
CARD 1
CARD 2
CARD 3
CARD 4

EPOCH
YR/MO/DAY
1973/ 1/ 1
TZME,HR,MIN,SEC
0.
0.
0.
0.
0.

INITIAL CONDITIONS
A,O,B,A,R,V
-28061976300E+03
-22950132100E+02
-77038199600E+02
-72448793000E+02
-16656981200E+09
-82010376600E+04
A,E,I,O,U,TAU
-13833121061E+09
-29981109581E+00
-2860634287E+02
-22966614029E+03
-2780113993E+03
-47599867647E+03
AF,AG,N,L,CHI,PSI
-22850036562E+00
-19409434856E+00
-41782100534E-02
-2600965736E+03
-19430910442E+00
-16498361915E+00

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

***** VEHICLE DATA FOR CASE 3 *****

IVEHID3
IC -100.
END 90.
90.
13744.772
-28.6
96853470.
CARD 1
CARD 2
CARD 3
CARD 4

STATION	DATA GENERATION I		MAX.ELE. (DEG.)	MAX.RANGE (N.MI.)	START TIME			STOP TIME			AZIMUTH1 (DEG.)	AZIMUTH2 (DEG.)
	INTERVAL (SEC.)	MIN.ELE. (DEG.)			DA	HR	MIN	DA	HR	MIN		
VTS	900.00	-0.00	-0.00	-0.	-0.	15.0000	-0.	-0.	4.	-0.0000	-0.0	-0.0
AND	900.00	-0.00	-0.00	-0.	-0.	15.0000	-0.	-0.	4.	-0.0000	-0.0	-0.0
QUM	900.00	-0.00	-0.00	-0.	-0.	15.0000	-0.	-0.	4.	-0.0000	-0.0	-0.0

DATA GENERATION II

* SIMULTANEOUS VEHICLE DATA GENERATION II KEY/HEADER

```

* STA 1 -- PRIMARY STATION ID
* STA 2 -- SECOND STATION ID
* STA 3 -- THIRD STATION IC
* T -- OBSERVATION DATA SET TYPE - 1 7 J K L M N O P Q R S T U
* 01 -- OBSERVATION 1----- R RD V2 S2 S3 S3D V3 V3D TDOA TOA 3MR MP R2 A
* 02 -- OBSERVATION 2----- A V2D S2D RL RC E
* 03 -- OBSERVATION 3----- E
* V1 -- VEHICLE 1 ID NUMBER
* V2 -- VEHICLE 2 ID NUMBER
* V3 -- VEHICLE 3 ID NUMBER

```

[illegible]

1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. 32. 33. 34. 35. 36. 37. 38. 39. 40. 41. 42. 43. 44. 45. 46. 47. 48. 49. 50. 51. 52. 53. 54. 55. 56. 57. 58. 59. 60. 61. 62. 63. 64. 65. 66. 67. 68. 69. 70. 71. 72. 73. 74. 75. 76. 77. 78. 79. 80. 81. 82. 83. 84. 85. 86. 87. 88. 89. 90. 91. 92. 93. 94. 95. 96. 97. 98. 99. 100. 101. 102. 103. 104. 105. 106. 107. 108. 109. 110. 111. 112. 113. 114. 115. 116. 117. 118. 119. 120. 121. 122. 123. 124. 125. 126. 127. 128. 129. 130. 131. 132. 133. 134. 135. 136. 137. 138. 139. 140. 141. 142. 143. 144. 145. 146. 147. 148. 149. 150. 151. 152. 153. 154. 155. 156. 157. 158. 159. 160. 161. 162. 163. 164. 165. 166. 167. 168. 169. 170. 171. 172. 173. 174. 175. 176. 177. 178. 179. 180. 181. 182. 183. 184. 185. 186. 187. 188. 189. 190. 191. 192. 193. 194. 195. 196. 197. 198. 199. 200. 201. 202. 203. 204. 205. 206. 207. 208. 209. 210. 211. 212. 213. 214. 215. 216. 217. 218. 219. 220. 221. 222. 223. 224. 225. 226. 227. 228. 229. 230. 231. 232. 233. 234. 235. 236. 237. 238. 239. 240. 241. 242. 243. 244. 245. 246. 247. 248. 249. 250. 251. 252. 253. 254. 255. 256. 257. 258. 259. 260. 261. 262. 263. 264. 265. 266. 267. 268. 269. 270. 271. 272. 273. 274. 275. 276. 277. 278. 279. 280. 281. 282. 283. 284. 285. 286. 287. 288. 289. 290. 291. 292. 293. 294. 295. 296. 297. 298. 299. 300. 301. 302. 303. 304. 305. 306. 307. 308. 309. 310. 311. 312. 313. 314. 315. 316. 317. 318. 319. 320. 321. 322. 323. 324. 325. 326. 327. 328. 329. 330. 331. 332. 333. 334. 335. 336. 337. 338. 339. 340. 341. 342. 343. 344. 345. 346. 347. 348. 349. 350. 351. 352. 353. 354. 355. 356. 357. 358. 359. 360. 361. 362. 363. 364. 365. 366. 367. 368. 369. 370. 371. 372. 373. 374. 375. 376. 377. 378. 379. 380. 381. 382. 383. 384. 385. 386. 387. 388. 389. 390. 391. 392. 393. 394. 395. 396. 397. 398. 399. 400. 401. 402. 403. 404. 405. 406. 407. 408. 409. 410. 411. 412. 413. 414. 415. 416. 417. 418. 419. 420. 421. 422. 423. 424. 425. 426. 427. 428. 429. 430. 431. 432. 433. 434. 435. 436. 437. 438. 439. 440. 441. 442. 443. 444. 445. 446. 447. 448. 449. 450. 451. 452. 453. 454. 455. 456. 457. 458. 459. 460. 461. 462. 463. 464. 465. 466. 467. 468. 469. 470. 471. 472. 473. 474. 475. 476. 477. 478. 479. 480. 481. 482. 483. 484. 485. 486. 487. 488. 489. 490. 491. 492. 493. 494. 495. 496. 497. 498. 499. 500. 501. 502. 503. 504. 505. 506. 507. 508. 509. 510. 511. 512. 513. 514. 515. 516. 517. 518. 519. 520. 521. 522. 523. 524. 525. 526. 527. 528. 529. 530. 531. 532. 533. 534. 535. 536. 537. 538. 539. 540. 541. 542. 543. 544. 545. 546. 547. 548. 549. 550. 551. 552. 553. 554. 555. 556. 557. 558. 559. 560. 561. 562. 563. 564. 565. 566. 567. 568. 569. 570. 571. 572. 573. 574. 575. 576. 577. 578. 579. 580. 581. 582. 583. 584. 585. 586. 587. 588. 589. 590. 591. 592. 593. 594. 595. 596. 597. 598. 599. 600. 601. 602. 603. 604. 605. 606. 607. 608. 609. 610. 611. 612. 613. 614. 615. 616. 617. 618. 619. 620. 621. 622. 623. 624. 625. 626. 627. 628. 629. 630. 631. 632. 633. 634. 635. 636. 637. 638. 639. 640. 641. 642. 643. 644. 645. 646. 647. 648. 649. 650. 651. 652. 653. 654. 655. 656. 657. 658. 659. 660. 661. 662. 663. 664. 665. 666. 667. 668. 669. 670. 671. 672. 673. 674. 675. 676. 677. 678. 679. 680. 681. 682. 683. 684. 685. 686. 687. 688. 689. 690. 691. 692. 693. 694. 695. 696. 697. 698. 699. 700. 701. 702. 703. 704. 705. 706. 707. 708. 709. 710. 711. 712. 713. 714. 715. 716. 717. 718. 719. 720. 721. 722. 723. 724. 725. 726. 727. 728. 729. 730. 731. 732. 733. 734. 735. 736. 737. 738. 739. 740. 741. 742. 743. 744. 745. 746. 747. 748. 749. 750. 751. 752. 753. 754. 755. 756. 757. 758. 759. 760. 761. 762. 763. 764. 765. 766. 767. 768. 769. 770. 771. 772. 773. 774. 775. 776. 777. 778. 779. 780. 781. 782. 783. 784. 785. 786. 787. 788. 789. 790. 791. 792. 793. 794. 795. 796. 797. 798. 799. 800. 801. 802. 803. 804. 805. 806. 807. 808. 809. 810. 811. 812. 813. 814. 815. 816. 817. 818. 819. 820. 821. 822. 823. 824. 825. 826. 827. 828. 829. 830. 831. 832. 833. 834. 835. 836. 837. 838. 839. 840. 84

DESCRIPTION

Simultaneous-vehicle DATA GENERATION II key/header printout

The observation names are abbreviated as follows for each data set type:

| ITEM | 1 | R _a
A _a
E _a
RD
V2D
S2
S2D
S3
S3D
V3
O
P | Station-vehicle range
Station-vehicle azimuth
Station-vehicle elevation
Station-vehicle range rate
Vehicle-vehicle range rate
Station-vehicle-vehicle range rate
Station-vehicle-vehicle range rate sum
Station-vehicle-vehicle range rate sum
Station-vehicle-vehicle range rate sum
Vehicle-vehicle range rate sum
Vehicle-vehicle range rate sum
Time difference of arrival of two signals
Time from station to Vehicle 1 minus station to Vehicle 2 to Vehicle 1 | Q
R
S
T
U | TOA
3WR
MP
R2
RL
Ab
Eb
TOPb | Time difference of arrival of signal transmitted from vehicle to Station 2
Time of signal transmitted from Station 1 to Vehicle 1 plus time from Vehicle 1 to Station 2
Time from Vehicle 1 to earth to Vehicle 2 minus time from Vehicle 1 to Vehicle 2
Two-way range
C-band range
L-band range
Vehicle-vehicle azimuth
Vehicle-vehicle elevation
Topocentric |
|------|---|---|--|-----------------------|--|--|
|------|---|---|--|-----------------------|--|--|

a Observation output for Data Set Type 1.
b Observation output for Data Set Type U. If TOP is entered, A and E contain vehicle-vehicle topocentric right ascension and declination.

Consider the following segments of DATA GENERATION II printout:

| | a | b | c | d |
|----|----------------------------------|---|---|---|
| 1 | STA
1113
VTS
AND
DUM | TOA
1112:3
V1
V2
V3
STA
2 | TOA
1112:3
V1
V2
V3
STA
2 | TOA
1112:3
V1
V2
V3
STA
2 |
| 2 | 7K
1 | 1 | 1 | 1 |
| 3 | 7K
1 | 2 | 2 | 2 |
| 4 | 7K
2 | 3 | 3 | 3 |
| 5 | 7K
2 | 1 | 1 | 1 |
| 6 | 7K
2 | 2 | 2 | 2 |
| 7 | 7K
2 | 3 | 3 | 3 |
| 8 | 7K
2 | 1 | 1 | 1 |
| 9 | 7K
2 | 2 | 2 | 2 |
| 10 | 7K
2 | 3 | 3 | 3 |
| 11 | 7K
2 | 1 | 1 | 1 |

- (1a) Station-vehicle R, A, E data generated between Station VTS and Vehicle 1 (ID No. 1).
- (1b) Station-vehicle A, E data generated between Station VTS and Vehicle 1 (ID No. 3).
- (1c) Station-vehicle R data generated between Station VTS and Vehicle 1 (ID No. 2).
- (2a) Station-vehicle range rate data generated between Station AND and Vehicle 1 (ID No. 1).
- (2b) Station-vehicle range and range rate data generated between Vehicle 1 (ID No. 1) and Vehicle 2 (ID No. 2).
- (2c) Vehicle-vehicle range rate data generated between Vehicle 1 (ID No. 1), Vehicle 2 (ID No. 3), and Vehicle 3 (ID No. 2)
- (3a) Time-of-arrival data generated between Vehicle 1 (ID No. 1) to Station VTS minus Vehicle 1 (ID No. 1) and Station AND.
- (3b) Time-of-arrival data generated between Vehicle 1 (ID No. 2) to Station VTS minus Vehicle 1 (ID No. 2) and Station AND.

| EPOCH | | X, Y, Z, DX, DY, DZ | | INITIAL CONDITIONS | | AF, AG, AH, CHI, PSI | |
|-------------|--------------------|---------------------|--|--------------------|--|----------------------|--|
| YR/MO/DAY | TZNE, HR, MIN, SEC | | | A, E, I, C, U, IAU | | | |
| -1973/ 1/ 1 | | -0.14766293955E+08 | | 0.13233313361E+09 | | -0.5206900E+54E-01 | |
| 0. | | -0.83343814448E+08 | | 0.2935342290E+00 | | -0.29529797564E+00 | |
| 0. | | -0.46362967502E+08 | | 0.28600000000E+02 | | 0.41781232924E-02 | |
| 0. | | 0.13535958029E+05 | | 0.35000000000E+03 | | 0.26000000000E+03 | |
| 0. | | -0.23867546102E+04 | | 0.27000000000E+03 | | -0.44262365465E-01 | |
| 0. | | -0.48408647259E-10 | | -0.14360514470E+04 | | 0.25102434855E+00 | |

NO PLANETARY PERTURBATIONS.

** NO ATMOSPHERE MODEL **

| ENTER SEGMENT 02 AT | .4 SECONDS. | EXECUTION TIME FOR SEGMENT 1 WAS | .1 CP SECS. |
|---------------------|-------------|----------------------------------|-------------|
| ENTER SEGMENT 10 AT | .4 SECONDS. | EXECUTION TIME FOR SEGMENT 2 WAS | .0 CP SECS. |


```

***** TRAJECTORY INTEGRATION FOR CASE 1 *****
*** TRAJECTORY START
* * * * *
SEG11 ENTRY TIME IS .41100 ECI * * * * *
*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .067 SECONDS TO INTEGRATE A SPAN OF 247.000 MINUTES ***
*** FROM 0.000 TO 247.000 MINUTES FROM MIDNIGHT OF EPOCH ***
***** TRAJECTORY INTEGRATION FOR CASE 2 *****

*** TRAJECTORY START
* * * * *
SEG11 ENTRY TIME IS .48200 ECI * * * * *
*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .066 SECONDS TO INTEGRATE A SPAN OF 247.000 MINUTES ***
*** FROM 0.000 TO 247.000 MINUTES FROM MIDNIGHT OF EPOCH ***
***** TRAJECTORY INTEGRATION FOR CASE 3 *****

*** TRAJECTORY START
* * * * *
SEG11 ENTRY TIME IS .55500 ECI * * * * *
*** TRAJECTORY TERMINATION

*** THIS CASE TOOK .072 SECONDS TO INTEGRATE A SPAN OF 243.000 MINUTES ***
*** FROM 0.000 TO 243.000 MINUTES FROM MIDNIGHT OF EPOCH ***

ENTER SEGMENT 61 AT .6 SECONDS. EXECUTION TIME FOR SEGMENT 10 WAS .3 CP SECS.

```


REFERENCE
SECTION

ITEM

DESCRIPTION

Item 4

- 5 DATA GENERATION II output. Each line corresponds to a primary station, secondary station, year, month, day, hour, minute, second, data set type, generated observations, vehicle ID number, observation data abbreviations, and station and vehicle sequence numbers. The output description is:

| STA | ST2 | Y | M | D | H | M | SEC | OT | OB1 | OB2
(V3) | OB3
(V2) | V1 | Observation data sets | Station and vehicle sequence Nos. |
|--------------------|----------------------|------|-------|-----|------|--------|--------|------------------|---|---|---|-----------|-----------------------|-----------------------------------|
| Primary station ID | Secondary station ID | Year | Month | Day | Hour | Minute | Second | Observation type | Observation data for all data set types | Observation data for Data Set Types 1, J, K, T, and U
V3 ID No. for Data Set Types L, M, N, and O
Zero for other data set types | Observation data for Data Set Types 1 and T
O, P, S, and U
V2 ID No. for Data Set Types J, K, L, M, N,
Zero for other data set types | V1 ID No. | | |

| STA | ST2 | Y | M | D | H | M | SEC | OT | DB1 | DB2
(V3) | DB3
(V2) | V1 | 5 |
|-----|-----|----|---|---|---|----|---------|----|----------------|----------------|---------------|----|-----------------|
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | 1 | .11908033E+09 | .13875191E+03 | .45901570E+12 | 1 | RAE S-V1 |
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | K | .19232075E+09 | .00385037E+02 | .30000000E+01 | 1 | R RD S-V1-V2 |
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | K | .19317728E+09 | .15435345E+03 | .20000000E+01 | 1 | R RD S-V1-V2 |
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | H | -.08535707E+03 | .30000000E+01 | .20000000E+01 | 1 | R RD S-V1-V2-V3 |
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | 1 | .15182447E+09 | .96745079E+02 | .49046998E+12 | 3 | RAE S-V1 |
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | L | .36190448E+09 | .10000000E+01 | .20000000E+01 | 3 | R S-V1-V2-V3 |
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | 1 | .90991230E+08 | .15616627E+03 | .10431786E+12 | 2 | RAE S-V1 |
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | M | .43460611E+03 | .30000000E+01 | .10000000E+01 | 2 | R RD S-V1-V2-V3 |
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | K | .22697431E+09 | .10000000E+01 | .30000000E+01 | 2 | R RD S-V1-V2 |
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | L | .30021472E+09 | .10000000E+01 | .30000000E+01 | 2 | R RD S-V1-V2-V3 |
| VTS | AND | 73 | 1 | 1 | 0 | 15 | 0.00000 | 0 | -.44255651E+03 | 0. | 0. | 1 | TOA VS1-VS2 |
| VTS | AND | 73 | 1 | 1 | 0 | 15 | 0.00000 | 0 | .37450345E+02 | 0. | 0. | 3 | TOA VS1-VS2 |
| VTS | AND | 73 | 1 | 1 | 0 | 15 | 0.00000 | 0 | -.82450442E+03 | 0. | 0. | 2 | TOA VS1-VS2 |
| AND | | 73 | 1 | 1 | 0 | 15 | 0.00000 | 7 | .24319331E+03 | 0. | 0. | 1 | R RD S-V1 |
| AND | | 73 | 1 | 1 | 0 | 15 | 0.00000 | L | .32959550E+09 | .30000000E+01 | .20000000E+01 | 1 | R RD S-V1-V2-V3 |
| AND | | 73 | 1 | 1 | 0 | 15 | 0.00000 | H | .52080722E+03 | .10000000E+01 | .20000000E+01 | 3 | R RD S-V1-V2-V3 |
| AND | | 73 | 1 | 1 | 0 | 15 | 0.00000 | P | .10351092E+00 | 0. | .10000000E+01 | 2 | TOA SV1V2-SV2 |
| AND | | 73 | 1 | 1 | 0 | 15 | 0.00000 | L | .23913938E+09 | .30000000E+01 | .10000000E+01 | 2 | TOA SV1V2-SV2 |
| AND | | 73 | 1 | 1 | 0 | 15 | 0.00000 | P | .19553368E+00 | 0. | .30000000E+01 | 2 | R RD S-V1-V2-V3 |
| AND | | 73 | 1 | 1 | 0 | 15 | 0.00000 | M | -.14767996E+04 | .10000000E+01 | 0. | 2 | R RD S-V1-V2-V3 |
| AND | VTS | 73 | 1 | 1 | 0 | 15 | 0.00000 | R | .24258108E+00 | 0. | 0. | 1 | 3WR SV1V1-S1V2 |
| AND | VTS | 73 | 1 | 1 | 0 | 15 | 0.00000 | R | .30497605E+00 | 0. | 0. | 3 | 3WR SV1V1-S1V2 |
| DUM | | 73 | 1 | 1 | 0 | 15 | 0.00000 | R | .18584647E+00 | 0. | 0. | 2 | 3WR SV1V1-S1V2 |
| DUM | | 73 | 1 | 1 | 0 | 15 | 0.00000 | J | .73240415E+08 | 0. | .30000000E+01 | 1 | R RD V1-V2 |
| DUM | | 73 | 1 | 1 | 0 | 15 | 0.00000 | S | .19231125E+00 | 0. | .30000000E+01 | 1 | R RD V1-V2-V3 |
| DUM | | 73 | 1 | 1 | 0 | 15 | 0.00000 | N | .20922348E+09 | .20000000E+01 | .30000000E+01 | 1 | R RD V1-V2-V3 |
| DUM | | 73 | 1 | 1 | 0 | 15 | 0.00000 | J | -.12305741E+04 | 0. | .20000000E+01 | 1 | R RD V1-V2 |
| DUM | | 73 | 1 | 1 | 0 | 15 | 0.00000 | S | .74096949E+08 | -.14868231E+03 | .20000000E+01 | 1 | MULT V1EV2-V1V2 |
| DUM | | 73 | 1 | 1 | 0 | 15 | 0.00000 | S | .11999225E+00 | 0. | .20000000E+01 | 2 | R RD V1-V2 |
| VTS | | 73 | 1 | 1 | 0 | 15 | 0.00000 | J | .13598307E+09 | -.10079242E+04 | .30000000E+01 | 1 | RAE S-V1 |
| VTS | | 73 | 1 | 1 | 0 | 30 | 0.00000 | 1 | .11936148E+09 | .13831957E+03 | .45992510E+12 | 1 | R RD S-V1-V2 |
| VTS | | 73 | 1 | 1 | 0 | 30 | 0.00000 | K | .19243759E+09 | .17959777E+03 | .30000000E+01 | 1 | R RD S-V1-V2 |
| VTS | | 73 | 1 | 1 | 0 | 30 | 0.00000 | K | .1930217E+09 | .12276780E+03 | .20000000E+01 | 1 | R RD S-V1-V2-V3 |
| VTS | | 73 | 1 | 1 | 0 | 30 | 0.00000 | M | -.92418810E+03 | .30000000E+01 | .20000000E+01 | 1 | R RD S-V1-V2-V3 |
| VTS | | 73 | 1 | 1 | 0 | 30 | 0.00000 | 1 | .15301717E+09 | .96589886E+02 | .50530271E+12 | 3 | RAE S-V1 |
| VTS | | 73 | 1 | 1 | 0 | 30 | 0.00000 | L | .36201577E+09 | .10000000E+01 | .20000000E+01 | 3 | R S-V1-V2-V3 |
| VTS | | 73 | 1 | 1 | 0 | 30 | 0.00000 | 1 | .91846886E+08 | .15199145E+03 | .95632226E+11 | 2 | RAE S-V1 |
| VTS | | 73 | 1 | 1 | 0 | 30 | 0.00000 | M | .75184476E+03 | .30000000E+01 | .10000000E+01 | 2 | R RD S-V1-V2-V3 |
| VTS | | 73 | 1 | 1 | 0 | 30 | 0.00000 | K | .22690480E+09 | .45436889E+02 | .30000000E+01 | 2 | R RD S-V1-V2 |

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| | | | | | | | | | | | | | | | |
|-----|----|---|---|---|---|----|---------|---|---------------|----------------|---------------|---------------|---|------|------------|
| AND | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | P | .19478731E+00 | 0. | .10000000E+01 | .30000000E+01 | 2 | TD0A | SV1V2-SV2 |
| AND | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | M | .25741756E+03 | 0. | .30000000E+01 | .30000000E+01 | 2 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | K | .24551276E+03 | 0. | 0. | 0. | 1 | 3MR | S1V1-S1V2 |
| AND | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | R | .3167091E+00 | 0. | 0. | 0. | 3 | 3MR | S1V1-S1V2 |
| AND | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | R | .19483468E+00 | 0. | 0. | 0. | 2 | 3MR | S1V1-S1V2 |
| DUM | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | J | .73170498E+08 | .15299603E+03 | .30000000E+01 | .30000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | S | .20047196E+00 | 0. | .20000000E+01 | .30000000E+01 | 1 | MULT | V1E2-V1V2 |
| DUM | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | N | .20424163E+09 | .20000000E+01 | .30000000E+01 | .30000000E+01 | 1 | R | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | C | .96633197E+03 | .20000000E+01 | .30000000E+01 | .30000000E+01 | 1 | R RD | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | J | .72873174E+03 | -.38724718E+03 | .20000000E+01 | .20000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | S | .12882793E+00 | 0. | .30000000E+01 | .30000000E+01 | 1 | MULT | V1E2-V1V2 |
| DUM | 73 | 1 | 1 | 1 | 1 | 30 | 0.00000 | J | .13177113E+09 | -.11593280E+04 | .30000000E+01 | .30000000E+01 | 2 | R RD | V1-V2 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | I | .12097158E+09 | .13677603E+03 | .46297081E+12 | .46297081E+12 | 1 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | K | .19435150E+09 | .65807525E+03 | .30000000E+01 | .30000000E+01 | 1 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | K | .19347966E+09 | -.36374111E+02 | .20000000E+01 | .20000000E+01 | 1 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | M | .12179918E+04 | .30000000E+01 | .20000000E+01 | .20000000E+01 | 1 | RD | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | I | .15763189E+09 | .96806760E+02 | .57663450E+12 | .57663450E+12 | 3 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | L | .36015758E+09 | .10000000E+01 | .20000000E+01 | .20000000E+01 | 3 | R | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | I | .99421133E+08 | .13273377E+03 | .96605045E+01 | .96605045E+01 | 2 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | M | .20133077E+04 | .30000000E+01 | .10000000E+01 | .10000000E+01 | 2 | RD | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | K | .22943874E+09 | .98277818E+03 | .30000000E+01 | .30000000E+01 | 2 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | L | .30281866E+03 | .10000000E+01 | .30000000E+01 | .30000000E+01 | 2 | R | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | Q | .19969139E-03 | 0. | 0. | 0. | 1 | TOA | VS1-VS2 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | Q | .2329035E-02 | 0. | 0. | 0. | 3 | TOA | VS1-VS2 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | Q | .41849420E-02 | 0. | 0. | 0. | 2 | TOA | VS1-VS2 |
| AND | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | 7 | .35892990E+03 | 0. | .30000000E+01 | .30000000E+01 | 1 | R | S-V1 |
| AND | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | L | .32369355E+09 | .30000000E+01 | .20000000E+01 | .20000000E+01 | 1 | R | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | P | .51437327E+03 | .10000000E+01 | .20000000E+01 | .20000000E+01 | 3 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | F | .10031453E+00 | .30000000E+01 | .10000000E+01 | .10000000E+01 | 2 | TD0A | SV1V2-SV2 |
| AND | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | L | .24119277E+09 | .30000000E+01 | .10000000E+01 | .10000000E+01 | 2 | R | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | P | .19352426E+00 | 0. | .30000000E+01 | .30000000E+01 | 2 | TD0A | SV1V2-SV2 |
| AND | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | M | .56233790E+03 | .10000000E+01 | .30000000E+01 | .30000000E+01 | 2 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | R | .24618392E+00 | 0. | .30000000E+01 | .30000000E+01 | 2 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | R | .31849886E+00 | 0. | 0. | 0. | 1 | 3MR | S1V1-S1V2 |
| AND | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | R | .19797874E+00 | 0. | 0. | 0. | 3 | 3MR | S1V1-S1V2 |
| DUM | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | J | .73379915E+08 | .27168059E+03 | .30000000E+01 | .30000000E+01 | 2 | 3MR | S1V1-S1V2 |
| DUM | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | S | .23160609E+00 | 0. | .30000000E+01 | .30000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | N | .20339752E+09 | .20000000E+01 | .30000000E+01 | .30000000E+01 | 1 | MULT | V1E2-V1V2 |
| DUM | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | O | .91993707E+03 | .20000000E+01 | .30000000E+01 | .30000000E+01 | 1 | R | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | J | .72518074E+08 | -.42276877E+03 | .20000000E+01 | .20000000E+01 | 1 | RD | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | S | .13159454E+00 | 0. | .30000000E+01 | .30000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | J | .13031761E+09 | -.11816177E+04 | .30000000E+01 | .30000000E+01 | 1 | MULT | V1E2-V1V2 |
| VTS | 73 | 1 | 1 | 1 | 1 | 45 | 0.00000 | I | .12132278E+09 | .13660084E+03 | .46330219E+12 | .46330219E+12 | 2 | R RD | V1-V2 |

| | | | | | | | | | | | | | |
|-----|----|---|---|---|----|----------|---|----------------|----------------|---------------|---|------|------------|
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | K | .19490007E+09 | .73933330E+03 | .30000000E+01 | 1 | R RD | S-V1-V2 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | K | .19343767E+09 | -.55559274E+02 | .20000000E+01 | 1 | R RD | S-V1-V2 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | M | -.12502170E+04 | .30000000E+01 | .20000000E+01 | 1 | RAE | S-V1-V2-V3 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | L | .15827993E+09 | .97079441E+02 | .59035573E+02 | 3 | R | S-V1 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | L | .35933394E+09 | .10000000E+01 | .20000000E+01 | 3 | R | S-V1-V2-V3 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | M | .10143150E+09 | .12941962E+03 | .10435959E+02 | 2 | RAE | S-V1 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | M | .21950644E+04 | .30000000E+01 | .10000000E+01 | 2 | RD | S-V1-V2-V3 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | K | .23037609E+09 | .10960930E+04 | .30000000E+01 | 2 | R RD | S-V1-V2 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | L | .30403419E+09 | .10000000E+01 | .30000000E+01 | 2 | R | S-V1-V2-V3 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | Q | -.17727309E-03 | 0. | 0. | 1 | TOA | VS1-VS2 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | Q | .47775516E-02 | 0. | 0. | 3 | TOA | VS1-VS2 |
| VTs | 73 | 1 | 1 | 2 | 0 | 0.000000 | Q | .37221258E+03 | 0. | 0. | 2 | TOA | VS1-VS2 |
| AND | 73 | 1 | 1 | 2 | 0 | 0.000000 | 7 | .32255609E+09 | .30000000E+01 | .30000000E+01 | 1 | RD | S-V1 |
| AND | 73 | 1 | 1 | 2 | 0 | 0.000000 | L | -.66429403E+03 | .10000000E+01 | .20000000E+01 | 3 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 0 | 0.000000 | P | .98498121E-01 | 0. | .10000000E+01 | 2 | TDOA | SV1V2-V2 |
| AND | 73 | 1 | 1 | 2 | 0 | 0.000000 | L | .24250527E+09 | .30000000E+01 | .10000000E+01 | 2 | R | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 0 | 0.000000 | P | .19193239E+00 | 0. | .30000000E+01 | 2 | TDOA | SV1V2-SV2 |
| AND | 73 | 1 | 1 | 2 | 0 | 0.000000 | M | .63899815E+03 | .10000000E+01 | .30000000E+01 | 2 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 0 | 0.000000 | R | .24687563E+00 | 0. | 0. | 3 | 3MR | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 0 | 0.000000 | R | .32010604E+00 | 0. | 0. | 3 | 3MR | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 0 | 0.000000 | R | .20147407E+00 | 0. | 0. | 2 | 3MR | S-V1-V2-V3 |
| DUM | 73 | 1 | 1 | 2 | 0 | 0.000000 | J | .73658093E+08 | .34560303E+03 | .30000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 2 | 0 | 0.000000 | S | .20257490E+00 | 0. | .30000000E+01 | 1 | MULT | V1EV2-V1V2 |
| DUM | 73 | 1 | 1 | 2 | 0 | 0.000000 | N | .20260269E+09 | .20000000E+01 | .30000000E+01 | 1 | R | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 2 | 0 | 0.000000 | Q | -.85705472E+03 | .20000000E+01 | .30000000E+01 | 1 | RD | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 2 | 0 | 0.000000 | J | .72114807E+08 | -.44929014E+03 | .20000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 2 | 0 | 0.000000 | S | .13460225E+00 | 0. | .20000000E+01 | 1 | MULT | V1EV2-V1V2 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | J | .12894459E+09 | .12026570E+04 | .30000000E+01 | 2 | R RD | V1-V2 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | I | .12167973E+09 | .13647210E+03 | .46354953E+02 | 1 | RAE | S-V1 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | K | .19567997E+09 | .81284375E+03 | .30000000E+01 | 1 | R RD | S-V1-V2 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | K | .19338245E+09 | -.65424091E+02 | .20000000E+01 | 1 | R RD | S-V1-V2 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | H | -.12877473E+04 | .30000000E+01 | .20000000E+01 | 1 | R RD | S-V1-V2 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | L | .15883500E+09 | .97444505E+02 | .60390027E+02 | 3 | RAE | S-V1 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | L | .35839096E+09 | .10000000E+01 | .20000000E+01 | 3 | R | S-V1-V2-V3 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | M | .10355129E+09 | .12632100E+03 | .11401183E+02 | 2 | RAE | S-V1 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | M | .23568868E+04 | .30000000E+01 | .10000000E+01 | 2 | RD | S-V1-V2-V3 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | K | .23140453E+09 | .11054852E+04 | .30000000E+01 | 2 | R RD | S-V1-V2 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | L | .30540477E+09 | .10000000E+01 | .30000000E+01 | 2 | R | S-V1-V2-V3 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | Q | -.16033571E-03 | 0. | 0. | 1 | TOA | VS1-VS2 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | Q | .14488456E-02 | 0. | 0. | 3 | TOA | VS1-VS2 |
| VTs | 73 | 1 | 1 | 2 | 15 | 0.000000 | Q | .52880903E-02 | 0. | 0. | 2 | TOA | VS1-VS2 |
| AND | 73 | 1 | 1 | 2 | 15 | 0.000000 | 7 | .38368086E+03 | 0. | 0. | 1 | RD | S-V1 |

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|-----|----|---|---|---|----|----------|---|----------------|----------------|---------------|---|------|------------|
| AND | 73 | 1 | 1 | 2 | 15 | 0.000000 | L | .32139325E+09 | .30000000E+01 | .20000000E+01 | 1 | R | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 15 | 2.300000 | M | -.60171509E+03 | .10000000E+01 | .20000000E+01 | 3 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 15 | 0.000000 | P | .96780416E-01 | 0. | .10000000E+01 | 2 | TOA | SV1V2-SV2 |
| AND | 73 | 1 | 1 | 2 | 15 | 0.000000 | L | .24435289E+09 | .30000000E+01 | .10000000E+01 | 2 | R | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 15 | 0.000000 | F | .19003510E+00 | 0. | .30000000E+01 | 2 | TOA | SV1V2-SV2 |
| AND | 73 | 1 | 1 | 2 | 15 | 0.000000 | M | .10856871E+04 | .10000000E+01 | .30000000E+01 | 2 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 15 | 0.000000 | R | .24758452E+00 | 0. | 0. | 1 | 3MR | S1V1-S1V2 |
| AND | 73 | 1 | 1 | 2 | 15 | 0.000000 | R | .32152726E+00 | 0. | 0. | 3 | 3MR | S1V1-S1V2 |
| AND | 73 | 1 | 1 | 2 | 15 | 0.000000 | R | .20527397E+00 | 0. | 0. | 2 | 3MR | S1V1-S1V2 |
| AND | 73 | 1 | 1 | 2 | 15 | 0.000000 | R | .74000243E+08 | .41367313E+03 | .30000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 2 | 15 | 0.000000 | J | .20338112E+00 | 0. | .30000000E+01 | 1 | MULT | V1EV2-V1V2 |
| DUM | 73 | 1 | 1 | 2 | 15 | 0.000000 | S | .20195348E+09 | .20000000E+01 | .30000000E+01 | 1 | R | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 2 | 15 | 0.000000 | N | -.80865004E+03 | .20000000E+01 | .30000000E+01 | 1 | R | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 2 | 15 | 0.000000 | O | .71702719E+08 | -.46459478E+03 | .20000000E+01 | 1 | RD | V1-V2 |
| DUM | 73 | 1 | 1 | 2 | 15 | 0.000000 | J | .13780630E+00 | 0. | .20000000E+01 | 1 | MULT | V1EV2-V1V2 |
| DUM | 73 | 1 | 1 | 2 | 15 | 0.000000 | S | .12785324E+09 | -.12223232E+04 | .30000000E+01 | 2 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 2 | 15 | 0.000000 | J | .12204073E+09 | .13639037E+03 | .46371649E+02 | 1 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | K | .19644140E+09 | .87771709E+03 | .30000000E+01 | 1 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | K | .19332331E+09 | -.63967282E+02 | .20000000E+01 | 1 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | M | -.13041250E+04 | .30000000E+01 | .20000000E+01 | 1 | RD | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | L | .15929667E+09 | .97912020E+02 | .61726804E+02 | 3 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | L | .35732420E+09 | .10000000E+01 | .20000000E+01 | 3 | R | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | L | .10575846E+09 | .12343942E+03 | .12528176E+02 | 2 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | K | .25015015E+04 | .30000000E+01 | .10000000E+01 | 2 | RD | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | K | .23250342E+09 | .12530574E+04 | .30000000E+01 | 2 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | L | .30690409E+09 | .10000000E+01 | .30000000E+01 | 2 | R | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | Q | -.14894119E-03 | 0. | 0. | 1 | TOA | VS1-VS2 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | Q | .11553282E-02 | 0. | 0. | 3 | TOA | VS1-VS2 |
| VTS | 73 | 1 | 1 | 2 | 30 | 0.000000 | Q | .57181029E-02 | 0. | 0. | 2 | TOA | VS1-VS2 |
| AND | 73 | 1 | 1 | 2 | 30 | 0.000000 | 7 | .39332379E+03 | 0. | 0. | 1 | RD | S-V1 |
| AND | 73 | 1 | 1 | 2 | 30 | 0.000000 | L | .32021463E+09 | .30000000E+01 | .20000000E+01 | 1 | R | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 30 | 0.000000 | M | -.92468045E+03 | .10000000E+01 | .20000000E+01 | 3 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 30 | 0.000000 | P | .94894303E-01 | 0. | .10000000E+01 | 2 | TOA | SV1V2-SV2 |
| AND | 73 | 1 | 1 | 2 | 30 | 0.000000 | L | .24581741E+09 | .30000000E+01 | .10000000E+01 | 2 | R | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 30 | 0.000000 | F | .18785724E+00 | 0. | .30000000E+01 | 2 | TOA | SV1V2-SV2 |
| AND | 73 | 1 | 1 | 2 | 30 | 0.000000 | M | .13010256E+04 | .10000000E+01 | .30000000E+01 | 2 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 30 | 0.000000 | R | .24830718E+00 | 0. | 0. | 1 | 3MR | S1V1-S1V2 |
| AND | 73 | 1 | 1 | 2 | 30 | 0.000000 | R | .32275950E+00 | 0. | 0. | 3 | 3MR | S1V1-S1V2 |
| AND | 73 | 1 | 1 | 2 | 30 | 0.000000 | R | .20933320E+00 | 0. | 0. | 2 | 3MR | S1V1-S1V2 |
| DUM | 73 | 1 | 1 | 2 | 30 | 0.000000 | J | .74400875E+08 | .47498540E+03 | .30000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 2 | 30 | 0.000000 | S | .20402845E+00 | 0. | .30000000E+01 | 1 | MULT | V1EV2-V1V2 |
| DUM | 73 | 1 | 1 | 2 | 30 | 0.000000 | N | .20114563E+09 | .20000000E+01 | .30000000E+01 | 1 | R | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 2 | 30 | 0.000000 | O | -.76517233E+03 | .20000000E+01 | .30000000E+01 | 1 | RD | V1-V2-V3 |

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|-----|----|---|---|---|----|----------|---|-----------------|------------------|----------------|---|------|-------------|
| DUM | 73 | 1 | 1 | 2 | 30 | 0.000000 | J | .71262561E+08 | --.466696897E+03 | .200000000E+1 | 1 | R RD | V1-V1 |
| DUM | 73 | 1 | 1 | 2 | 30 | 0.000000 | S | .14116155E+00 | 0. | .200000000E+1 | 1 | MULT | V1E2-V1V2 |
| DUM | 73 | 1 | 1 | 2 | 30 | 0.000000 | J | .12674496E+09 | --.12401577E+04 | .200000000E+1 | 1 | R RD | V1-V2 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | K | .12240409E+09 | .13635547E+03 | .46380655E+02 | 1 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | K | .19725706E+09 | .93326284E+03 | .300000000E+1 | 1 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | K | .19327120E+09 | --.49545634E+02 | .200000000E+1 | 1 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | M | --.13050001E+04 | .300000000E+01 | .200000000E+01 | 1 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | L | .15966456E+09 | .98494202E+02 | .63045695E+02 | 3 | K | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | L | .35611538E+09 | .100000000E+01 | .200000000E+01 | 3 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | L | .10803254E+09 | .12077175E+03 | .13790574E+02 | 2 | RD | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | M | .26316706E+04 | .300000000E+01 | .100000000E+01 | 2 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | K | .23365425E+09 | .13013821E+04 | .300000000E+01 | 2 | R | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | L | .30850723E+09 | .100000000E+01 | .300000000E+01 | 2 | TOA | VS1-VS2 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | Q | --.14312540E-03 | 0. | 0. | 1 | TOA | VS1-VS2 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | Q | .86096704E-03 | 0. | 0. | 3 | TOA | VS1-VS2 |
| VTS | 73 | 1 | 1 | 2 | 45 | 0.000000 | C | .63709253E-02 | 0. | 0. | 2 | TOA | VS1-VS2 |
| AND | 73 | 1 | 1 | 2 | 45 | 0.000000 | Q | .471114054E+03 | 0. | 0. | 1 | R | S-V1 |
| AND | 73 | 1 | 1 | 2 | 45 | 0.000000 | L | .31903356E+09 | .300000000E+01 | .200000000E+1 | 1 | R | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 45 | 0.000000 | H | .471114054E+04 | .100000000E+01 | .200000000E+1 | 3 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 45 | 0.000000 | F | --.10307644E+04 | 0. | .100000000E+1 | 2 | TDOA | SV1V2-V2 |
| AND | 73 | 1 | 1 | 2 | 45 | 0.000000 | L | .92876895E-01 | .300000000E+01 | .100000000E+1 | 2 | R | SV1V2-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 45 | 0.000000 | P | .24778130E+09 | .300000000E+01 | .300000000E+01 | 2 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 2 | 45 | 0.000000 | H | .18542443E+00 | 0. | .300000000E+1 | 2 | 3MR | SV1V2-S1V2 |
| AND | 73 | 1 | 1 | 2 | 45 | 0.000000 | R | .24904023E+00 | .100000000E+01 | .300000000E+1 | 1 | 3MR | SV1V2-S1V2 |
| AND | 73 | 1 | 1 | 2 | 45 | 0.000000 | R | .32380190E+00 | 0. | 0. | 3 | 3MR | SV1V2-S1V2 |
| AND | 73 | 1 | 1 | 2 | 45 | 0.000000 | R | .21360342E+00 | 0. | 0. | 2 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 2 | 45 | 0.000000 | J | .74852972E+08 | .52882125E+03 | .300000000E+1 | 1 | MULT | V1E2-V1V2 |
| DUM | 73 | 1 | 1 | 2 | 45 | 0.000000 | S | .20452135E+00 | 0. | .300000000E+1 | 1 | R | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 2 | 45 | 0.000000 | N | .20047468E+09 | .200000000E+01 | .300000000E+1 | 1 | RD | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 2 | 45 | 0.000000 | O | --.72663324E+03 | .200000000E+01 | .300000000E+1 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 2 | 45 | 0.000000 | J | .70867111E+08 | --.45398721E+03 | .200000000E+01 | 1 | MULT | V1E2-V1V2 |
| DUM | 73 | 1 | 1 | 2 | 45 | 0.000000 | S | .14462348E+00 | 0. | .200000000E+1 | 2 | R RD | V1-V2 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | J | .12562171E+09 | --.12554545E+04 | .300000000E+1 | 1 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | K | .12276818E+09 | .13636733E+03 | .46382294E+02 | 1 | R RD | S-V1-V3 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | K | .19811832E+09 | .97898113E+03 | .300000000E+01 | 1 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | K | .19323337E+09 | --.20978677E+02 | .200000000E+1 | 1 | RD | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | P | --.12883216E+04 | .300000000E+01 | .200000000E+01 | 3 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | L | .15993836E+09 | .99205832E+02 | .64346221E+02 | 3 | R | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | L | .35489472E+09 | .100000000E+01 | .200000000E+1 | 2 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | P | .11035482E+09 | .11031111E+03 | .15164279E+12 | 2 | RD | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | P | .27499977E+04 | .300000000E+01 | .100000000E+1 | 2 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | K | .23494098E+09 | .13332861E+04 | .300000000E+1 | 2 | R | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 3 | 0 | 0.000000 | L | .31019113E+09 | .100000000E+01 | .300000000E+1 | 2 | R | S-V1-V2-V3 |

| | | | | | | | | | | | | | |
|---------|----|---|---|---|----|----------|---|----------------|----------------|---------------|---|------|------------|
| DUM | 73 | 1 | 1 | 3 | 15 | 0.000000 | J | .7584816E+03 | .61208955E+03 | .30000000E+01 | 1 | R RD | V1-V? |
| DUM | 73 | 1 | 1 | 3 | 15 | 0.000000 | S | .20503646E+00 | 0. | .30000000E+01 | 1 | MULT | V1E2-V1V2 |
| DUM | 73 | 1 | 1 | 3 | 15 | 0.000000 | N | .19922662E+09 | .20000000E+01 | .30000000E+01 | 1 | R | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 3 | 15 | 0.000000 | O | -.66276114E+03 | .20000000E+01 | .30000000E+01 | 1 | R RD | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 3 | 15 | 0.000000 | J | .7106517E+00 | -.30000000E+01 | .20000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 3 | 15 | 0.000000 | S | .15169669E+00 | 0. | .20000000E+01 | 1 | MULT | V1E2-V1V2 |
| DUM | 73 | 1 | 1 | 3 | 15 | 0.000000 | J | .12334180E+09 | -.12748707E+04 | .30000000E+01 | 2 | R RD | V1-V2 |
| VTS | 73 | 1 | 1 | 3 | 30 | 0.000000 | I | .12349209E+09 | .13652920E+03 | .46364595E+02 | 1 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 3 | 30 | 0.000000 | K | .19994142E+09 | .10398193E+04 | .30000000E+01 | 1 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 3 | 30 | 0.000000 | K | .19328312E+09 | .80598180E+02 | .20000000E+01 | 1 | R RD | S-V1-V? |
| VTS | 73 | 1 | 1 | 3 | 30 | 0.000000 | M | -.11964747E+04 | .30000000E+01 | .20000000E+01 | 1 | R RD | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 3 | 30 | 0.000000 | I | .16020275E+09 | .10109263E+03 | .66888391E+02 | 3 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 3 | 30 | 0.000000 | L | .35218677E+09 | .10000000E+01 | .20000000E+01 | 3 | R | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 3 | 30 | 0.000000 | I | .11517780E+09 | .11397144E+03 | .18162231E+02 | 2 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 3 | 30 | 0.000000 | M | .29591537E+04 | .30000000E+01 | .10000000E+01 | 2 | R RD | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 3 | 30 | 0.000000 | K | .23727080E+09 | .13594026E+04 | .30000000E+01 | 2 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 3 | 30 | 0.000000 | L | .31372013E+09 | .10000000E+01 | .30000000E+01 | 2 | R | S-V1-V2-V3 |
| VTS AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | Q | -.15912185E-03 | 0. | 0. | 1 | TOA | VS1-VS2 |
| VTS AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | Q | -.26590424E-04 | 0. | 0. | 3 | TOA | VS1-VS2 |
| VTS AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | Q | .67154003E-02 | 0. | 0. | 2 | TOA | VS1-VS2 |
| AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | 7 | .41375919E+03 | 0. | 0. | 1 | R | S-V1 |
| AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | L | .31563249E+09 | .30000000E+01 | .20000000E+01 | 1 | R | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | M | -.12290785E+04 | .10000000E+01 | .20000000E+01 | 3 | RD | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | P | .86336616E-01 | 0. | .10000000E+01 | 2 | TOA | V1V2-SV2 |
| AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | F | .25471297E+09 | .30000000E+01 | .10000000E+01 | 2 | R | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | H | .17685485E+00 | 0. | .30000000E+01 | 2 | TOA | SV1V2-SV2 |
| AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | R | .25126858E+00 | 0. | 0. | 1 | 3MR | S-V1-V2-V3 |
| AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | R | .32578373E+00 | 0. | 0. | 3 | 3MR | S1V1-S1V2 |
| AND | 73 | 1 | 1 | 3 | 30 | 0.000000 | R | .22728490E+00 | 0. | 0. | 2 | 3MR | S1V1-S1V2 |
| DUM | 73 | 1 | 1 | 3 | 30 | 0.000000 | J | .76449332E+00 | .64094564E+03 | .30000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 3 | 30 | 0.000000 | S | .20512644E+00 | 0. | .30000000E+01 | 1 | MULT | V1E2-V1V2 |
| DUM | 73 | 1 | 1 | 3 | 30 | 0.000000 | N | .19864232E+09 | .20000000E+01 | .30000000E+01 | 1 | R | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 3 | 30 | 0.000000 | C | -.63612328E+03 | .20000000E+01 | .30000000E+01 | 1 | R RD | V1-V2-V3 |
| DUM | 73 | 1 | 1 | 3 | 30 | 0.000000 | J | .69791027E+08 | -.31827148E+03 | .20000000E+01 | 1 | R RD | V1-V2 |
| DUM | 73 | 1 | 1 | 3 | 30 | 0.000000 | S | .15522807E+00 | 0. | .20000000E+01 | 1 | MULT | V1E2-V1V2 |
| DUM | 73 | 1 | 1 | 3 | 30 | 0.000000 | J | .12219299E+09 | -.12770729E+04 | .30000000E+01 | 2 | R RD | V1-V2 |
| VTS | 73 | 1 | 1 | 3 | 45 | 0.000000 | I | .12384883E+09 | .13667774E+03 | .46345725E+02 | 1 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 3 | 45 | 0.000000 | K | .20088476E+09 | .10547731E+04 | .30000000E+01 | 1 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 3 | 45 | 0.000000 | K | .19338727E+09 | .15316026E+03 | .20000000E+01 | 1 | R RD | S-V1-V2 |
| VTS | 73 | 1 | 1 | 3 | 45 | 0.000000 | M | -.11198670E+04 | .30000000E+01 | .20000000E+01 | 1 | R RD | S-V1-V2-V3 |
| VTS | 73 | 1 | 1 | 3 | 45 | 0.000000 | L | .16019300E+09 | .10231545E+03 | .68126840E+02 | 3 | RAE | S-V1 |
| VTS | 73 | 1 | 1 | 3 | 45 | 0.000000 | L | .35077638E+09 | .10000000E+01 | .20000000E+01 | 3 | R | S-V1-V2-V3 |

| | | | | | | | | | | | | | | | |
|-----|----|---|---|---|---|----|----------|---|--------------|--------------|--------------|---|------|------------|------------|
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | 1 | 11744971E+09 | 11206942E+03 | 19751355E+12 | 2 | RAE | S-V1 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | M | 30528921E+04 | 30000000E+01 | 10000000E+01 | 2 | RD | S-V1-V2-V3 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | K | 23049465E+09 | 13591647E+04 | 30000000E+01 | 2 | R | S-V1-V2 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | L | 31553058E+09 | 10000000E+01 | 30000000E+01 | 2 | R | S-V1-V2-V3 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | Q | 17546611E-03 | 0. | 0. | 1 | TDA | VS1-VS2 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | Q | 3234544E-03 | 0. | 0. | 1 | TDA | VS1-VS2 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | Q | 60109566E-02 | 0. | 0. | 2 | TDA | VS1-VS2 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | 7 | 41443551E+03 | 0. | 0. | 1 | RD | S-V1 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | L | 31460467E+09 | 30000000E+01 | 20000000E+11 | 1 | R | S-V1-V2-V3 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | M | 12517182E+04 | 10000000E+01 | 20000000E+11 | 3 | RD | S-V1-V2-V3 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | F | 84192903E-01 | 0. | 10000000E+11 | 2 | TDDA | SV1V2-SV2 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | L | 25732490E+09 | 30000000E+01 | 10000000E+11 | 2 | R | S-V1-V2-V3 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | P | 17355905E+00 | 0. | 30000000E+11 | 2 | TDOA | SV1V2-SV2 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | M | 19443000E+04 | 10000000E+01 | 30000000E+11 | 2 | RD | S-V1-V2-V3 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | R | 25210333E+00 | 0. | 0. | 1 | 3MR | SV1V1-SV2 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | R | 32606112E+00 | 0. | 0. | 3 | 3MR | SV1V1-SV2 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | R | 23201241E+00 | 0. | 0. | 2 | 3MR | SV1V1-SV2 | |
| DUM | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | J | 77035928E+08 | 66115652E+03 | 30000000E+11 | 1 | R | RD | V1-V2 |
| DUM | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | S | 20515634E+00 | 20000000E+01 | 30000000E+11 | 1 | MULT | V1EV2-V1V2 | |
| DUM | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | N | 19080807E+09 | 20000000E+01 | 30000000E+11 | 1 | R | V1-V2-V3 | |
| DUM | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | Q | 61187073E+03 | 20000000E+01 | 30000000E+11 | 1 | RD | V1-V2-V3 | |
| DUM | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | J | 69538435E+08 | 2405636E+03 | 20000000E+11 | 1 | R | RD | V1-V2 |
| DUM | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | S | 15870724E+00 | 0. | 20000000E+01 | 1 | MULT | V1EV2-V1V2 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | J | 12104495E+09 | 12730272E+04 | 30000000E+01 | 2 | R | RD | V1-V2 |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | 1 | 12420012E+09 | 13686996E+03 | 30000000E+01 | 1 | RAE | S-V1 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | K | 20133696E+09 | 10595292E+04 | 20000000E+11 | 1 | R | RD | S-V1-V2 |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | K | 19356279E+09 | 23897568E+03 | 20000000E+11 | 1 | R | RD | S-V1-V2 |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | M | 10229190E+04 | 30000000E+01 | 20000000E+01 | 1 | RD | S-V1-V2-V3 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | 1 | 16008849E+09 | 10376463E+03 | 69340220E+02 | 3 | RAE | S-V1 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | L | 34935483E+09 | 10000000E+01 | 20000000E+01 | 3 | R | S-V1-V2-V3 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | 1 | 11901198E+09 | 11032978E+03 | 21301320E+02 | 2 | RAE | S-V1 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | M | 31493094E+04 | 30000000E+01 | 10000000E+01 | 2 | RD | S-V1-V2-V3 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | K | 23971565E+09 | 13534423E+04 | 30000000E+01 | 2 | R | RD | S-V1-V2 |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | L | 31735248E+09 | 10000000E+01 | 30000000E+01 | 2 | R | RD | S-V1-V2-V3 |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | Q | 19718713E-03 | 0. | 0. | 1 | TDA | VS1-VS2 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | Q | 62179390E-03 | 0. | 0. | 3 | TDA | VS1-VS2 | |
| VTs | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | Q | 41340363E+03 | 0. | 0. | 2 | TDA | VS1-VS2 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | 7 | 31366028E+09 | 30000000E+01 | 20000000E+11 | 1 | RD | S-V1 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | L | 12524770E+04 | 10000000E+01 | 20000000E+11 | 1 | R | S-V1-V2-V3 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | M | 82036786E-01 | 0. | 10000000E+11 | 3 | RD | S-V1-V2-V3 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | P | 26036763E+09 | 30000000E+01 | 10000000E+11 | 2 | TDOA | SV1V2-SV2 | |
| AND | 73 | 1 | 1 | 1 | 3 | 45 | 0.000000 | L | 17033413E+00 | 0. | 30000000E+11 | 2 | TDOA | SV1V2-SV2 | |

| AND | VTS | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | M | .20019679E+04 | .10000000E+01 | 0. | 0. | 30000000E+01 | 2 | RD | S-V1-V2-V3 |
|-----|-----|----|---|---|---|---|---|----------|---|----------------|----------------|----|----|--------------|------|-----------|------------|
| AND | VTS | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | R | .25274636E+00 | 0. | 0. | 0. | 0. | 1 | 3MR | S1V1-S1V2 |
| AND | VTS | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | R | .32614652E+00 | 0. | 0. | 0. | 0. | 3 | 3MR | S1V1-S1V2 |
| AND | VTS | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | R | .23677046E+00 | 0. | 0. | 0. | 2 | 3MR | S1V1-S1V2 | |
| DUM | | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | J | .77636833E+00 | .67276291E+03 | 0. | 0. | 0. | 1 | R RD | V1-V2 |
| DUM | | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | S | .20436045E+00 | 0. | 0. | 0. | 1 | MULT | V1E2-V1V2 | |
| DUM | | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | N | .19754050E+09 | .20000000E+01 | 0. | 0. | 0. | 1 | R | V1-V2-V3 |
| DUM | | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | O | -.58913181E+03 | .20000000E+01 | 0. | 0. | 0. | 1 | R RD | V1-V2-V3 |
| DUM | | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | J | .69362666E+00 | -.14779062E+03 | 0. | 0. | 0. | 1 | R RD | V1-V2 |
| DUM | | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | S | .16210166E+00 | 0. | 0. | 0. | 1 | MULT | V1E2-V1V2 | |
| DUM | | 73 | 1 | 1 | 1 | 4 | 0 | 0.000000 | J | .11990367E+09 | -.12618947E+04 | 0. | 0. | 0. | 2 | R RD | V1-V2 |

EXIT SEGMENT 61 AT 1.2 SECONDS. EXECUTION TIME FOR SEGMENT 61 MAC .5 CP SECS.

D. TRACE INPUT FORMS

| | |
|---|------|
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APPENDIX D

TRACE INPUT FORMS

INTRODUCTION

The engineering specification forms and load sheets that follow are very useful in expediting the preparation of TRACE input. Some of these forms bear former TRACE designations (TRACE-66 and TRACE66), which will be removed when the forms are updated.

TRAJECTORY ANALYSIS AND PROGRAMMING DEPARTMENT

TRACE66 (AD104A)

ENGINEERING REQUEST FORM

GENERAL INFORMATION:

REQUESTER _____ TELEPHONE _____ DATE _____

PROBLEM NUMBER OR J.O. _____ DATE _____

PROJECT _____

TYPE OF TRACE RUN:

EPHEMERIS GENERATION ()
ORBIT DETERMINATION ()
DATA GENERATION ()
COVARIANCE ANALYSIS ()

GENERAL INSTRUCTIONS:

IF A RERUN, USE OATA DECK LABELED _____

NEW OATA DECK TO BE SAVED: () YES () NO

DISPOSITION (TO BE COMPLETED BY PRODUCTION COORDINATOR)

SET UP BY _____ RUN IO _____ DATE _____

TAPE SAVED IF REQUIRED _____

JOB DISPOSITION AND RESULTS:

NOTE: ALL SPECIFIED INPUT UNITS MUST BE CONSISTENT.

TIME OF RUN:

CP _____ PP _____

OATE JOB COMPLETED _____

OATA DECK LABELED AS _____

TRACE 66
ORBIT AND FORCE MODEL SPECIFICATIONS

RUN TITLE: _____

| EPOCH: | | INITIAL CONDITIONS:
INDICATE THE TYPE USED | | | | | | | | VALUES |
|-----------|-------|---|----------|----------|----------|------------|----------|----------------|----------------|--------|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | |
| YEAR | _____ | a | a | a | A | ℓ_p | A | A ₁ | \dot{r}_{HE} | _____ |
| MONTH | _____ | y | δ | e | δ | δ_p | e | A ₂ | \dot{r}_{HE} | _____ |
| DAY | _____ | x | β | i | β | δ_p | i | n | \dot{r}_{HE} | _____ |
| TIME ZONE | _____ | b | A | Ω | A | δ_p | Ω | L | \dot{r}_{HE} | _____ |
| HOUR | _____ | y | i | ω | i | δ_p | ω | X | \dot{r}_{HE} | _____ |
| MINUTE | _____ | b | v | r | v | δ_p | r | Ψ | \dot{r}_{HE} | _____ |
| SECOND | _____ | | | | | | | | | |

NOTE: IF TYPE IS NEGATIVE, THEN THE UNITS OF THE INITIAL CONDITIONS ARE ASSUMED TO BE INTERNAL.
LUNAR INITIAL CONDITIONS ARE TYPES 11 THROUGH 18, CORRESPONDING TO THE ABOVE EARTH-REFERENCED TYPES 1 THROUGH 8.

GRAVITY MODEL: CHECK ONE.

SPHERICAL () STANDARD 6.6 () STANDARD 7.6 ()
C₂, C₃, C₄ () STANDARD 8.8 () OTHER (ATTACH) ()

SUN-MOON ATTRACTIONS: NO () YES ()

DRAG COEFFICIENT: C_DA/W = _____ FT²/LB

SEGMENTED DRAG COEFFICIENTS:

(C_DA/W)₁ = _____ (C_DA/W)₂ = _____
(C_DA/W)₃ = _____ (C_DA/W)₄ = _____
(C_DA/W)₅ = _____ (C_DA/W)₆ = _____
(C_DA/W)₇ = _____ (C_DA/W)₈ = _____
(C_DA/W)₉ = _____ (C_DA/W)₁₀ = _____

C_D TABLES: INDICATE THE OPTION TO BE USED AND ATTACH TABLES IF ANY

() NONE () C_D = f(v) () C_D = f(h)

LINEAR WEIGHT LOSS: NO () YES () W₀ = _____ LBS
W = _____ LBS/MIN t₀ = _____ MME t₁ = _____ MME

INSTANTANEOUS WEIGHT CHANGES: NO () YES () ATTACH TABLES

ATMOSPHERE MODEL: CHECK ONE AND PROVIDE INPUTS AS REQUIRED

ARDC 1959 () US STD 1962 ()
EXPONENTIAL () P₀ = _____ β = _____ h = _____
NRL () c₁ = _____ c₂ = _____ c₃ = _____
c₄ = _____ c₅ = _____ c₆ = _____
n = _____
LOCKHEED-JACCHIA () D1 = _____ D2 = _____ FLUX = _____
FMS 1967 () F₁₀ = _____ F₁₀ = _____ k_p = _____
JACCHIA 1964 () F₁₀ = _____ F₁₀ = _____ a_p = _____
JACCHIA 1964 (MOD) () F₁₀ = _____ F₁₀ = _____ a_p = _____
CRL () F₁₀ = _____ F₁₀ = _____ k_i = _____

IF a_p, F₁₀, k_p, OR k_i ARE TO BE FUNCTIONS OF TIME, ATTACH TABLES

SOLAR RADIATION PRESSURE: NO () YES ()

A = _____ FT²/LB C_p = _____ LBS/FT² C_pA/W = _____

ONBOARD ACCELEROMETER: NO () YES () ATTACH TABLES

FINITE THRUSTING: NO () YES () ATTACH TABLES

ORBIT ADJUSTS: NO () YES () ATTACH TABLES

INPUT LENGTH UNITS ARE IN _____ (ft, m, cm, km, etc.)

AEROSPACE FORM 6134 REV 9-71

TRACE66

Check one: No normalization ()
 APL normalization ()
 KAULA normalization ()

[illegible]

ATMOSPHERE AND C_D TABLES

() k_p = f(t); with a maximum of 50 entries

() $k_c = f(t)$; with a maximum of 50 entries

() $F_{10.7} = f(t)$; with a maximum of 12 entries

() $C_D = f(t)$, with a maximum of 25 entries

() $C_D = f(h)$; with a maximum of 25 entries

[illegible]

AEROSPACE FORM 4400

TRACE66
EVENT SPECIFICATIONS

ONBOARD ACCELEROMETER:

| T
MME | SCALE
FACTOR | BIAS
FT/SEC ² | T
MME | SCALE
FACTOR | BIAS
FT/SEC ² |
|----------|-----------------|-----------------------------|----------|-----------------|-----------------------------|
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

FINITE THRUSTING:

| DATA REQUESTING | | | | | | |
|----------------------|---------------------------------------|-----------------------------------|-----------------------------------|----------------|----------------|----------------|
| TYPE | P ₁ | P ₂ | P ₃ | P ₄ | | |
| 1 | T ₁ (FT/SEC ²) | T ₂ (1/MIN) | NOT USED | V (± FT/SEC) | | |
| 2 | T/W | C FT/SEC | A/G ₀ | V (± FT/SEC) | | |
| 3 | A (FT/SEC ²) | a | β | γ | | |
| 4 | A (FT/SEC ²) | θ _Y ⁺ (DEG) | θ _P ⁺ (DEG) | V (± FT/SEC) | | |
| 5 | A (FT/SEC ²) | θ _Y (DEG) | θ _P (DEG) | V (± FT/SEC) | | |
| 6 | T (LB) | ℓ | m | n | | |
| 7 | T (LB) | θ _Y ⁺ (DEG) | θ _P ⁺ (DEG) | ± V (± FT/SEC) | | |
| 8 | T (LB) | θ _Y (DEG) | θ _P (DEG) | ± V (± FT/SEC) | | |
| T _S (MME) | T _F (MME) | TYPE | P ₁ | P ₂ | P ₃ | P ₄ |

INSTANTANEOUS WEIGHT CHANGES:

| T(MME) | ΔW(LBS) | T(MME) | ΔW(LBS) | T(MME) | ΔW(LBS) |
|--------|---------|--------|---------|--------|---------|
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

ORBIT ADJUSTS:

| T(MME) | TYPE | P ₁ | P ₂ | P ₃ | TYPE | P ₁ | P ₂ | P ₃ |
|--------|------|----------------|----------------|----------------|------|----------------|----------------------|----------------------|
| | | | | | 1 | ΔR(FT/SEC) | ΔT(FT/SEC) | ΔC(FT/SEC) |
| | | | | | 2 | K (FT/SEC) | θ _Y (DEG) | θ _P (DEG) |
| | | | | | 3 | β (DEG) | A (DEG) | V(FT/SEC) |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |

TRACE-66
PARAMETER SPECIFICATIONS

[illegible]

* THIS VALUE FIELD IS USED ONLY FOR OBSERVATION BIASES AND SCALE FACTORS.

AEROSPACE FORM 4140

TRACE66 **ORBIT DETERMINATION SPECIFICATIONS**

ALL PARAMETERS MUST BE SPECIFIED ON THE TRACE66 PARAMETER SPECIFICATION FORM.

OBSERVATIONS ARE TO BE INPUT BY:

- () CARDS
 - () CARD IMAGE TAPE
 - () BINARY OBSERVATION TAPE
- IF CARDS OR A CARD IMAGE TAPE ARE BEING USED AND THE OBSERVATION DATA TO BE USED IS A SUBSET OF THE DATA PROVIDED, THE BEGINNING AND END OF THE INTERVAL TO BE USED ARE GIVEN BY:

BEGINNING YEAR _____ MONTH _____ DAY _____ HOUR _____ MIN _____ SEC _____
END YEAR _____ MONTH _____ DAY _____ HOUR _____ MIN _____ SEC _____

STATION INPUTS: η_E AND η_R ARE THE INDICES OF REFRACTION USED TO COMPUTE REFRACTION CORRECTIONS FOR ELEVATION AND RANGE DATA. A "V" INDICATES THE NOMINAL VALUES ARE TO BE USED, A "O" INDICATES NO CORRECTIONS AND IF A NON-STANDARD INDEX OF REFRACTION IS TO BE USED, IT MUST BE PROVIDED.

| STA
NAME | LAT
(DEG) | LONG
(DEG) | HEIGHT
(FEET) | INTERFEROMETER | | η_E
(312×10^{-6}) | η_R
(330×10^{-6}) |
|-------------|--------------|---------------|------------------|----------------|-------|--------------------------------------|--------------------------------------|
| | | | | P | Q | | |
| _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |

OBSERVATION WEIGHTS (σ 's):

| STA | DATA
TYPE | σ | DATA
TYPE | σ | DATA
TYPE | σ | DATA
TYPE | σ |
|-------|--------------|----------|--------------|----------|--------------|----------|--------------|----------|
| _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |

SUPPLY THE REQUIRED INPUTS FOR THE FOLLOWING IF OTHER THAN NOMINAL.

_____ MAXIMUM NUMBER OF ITERATIONS
 _____ RELATIVE CONVERGENCE TEST (.001)
 _____ ABSOLUTE CONVERGENCE TEST (0)
 _____ n FOR n-SIGMA EDITOR (100)

OPTIONS: CHECK THE OPTIONS DESIRED AND SUPPLY THE REQUIRED INPUT

- () SPEED OF LIGHT CORRECTION
 - () POSITIVE CORRECTION
 - () NEGATIVE CORRECTION
- () PRINT OBSERVATION RESIDUALS
- () PRINT OBSERVATION PARTIAL DERIVATIVES
- () PRINT ORDERED CORRELATION MATRIX
- () PRINT CORRELATION MATRIX AFTER LAST ITERATION
- () SUPPRESS CORRELATION MATRICES
- () PRINT $A^T A$ AND $(A^T A)^{-1}$ AFTER EACH ITERATION, OR LAST ITERATION ONLY
- () PUNCH $A^T A$ AFTER LAST ITERATION
- () PUNCH SOLUTION VECTOR
- () PRINTER PLOT OF OBSERVATION RESIDUALS AFTER LAST ITERATION
- DATA RATE IS _____ SEC
- () GENERATE AND SAVE OBSERVATION RESIDUAL TAPE

TRACE-66
TRAJECTORY OUTPUT SPECIFICATIONS

OUTPUT TIMES: TIMES ARE GIVEN AS MINUTES FROM EPOCH () OR MIDNIGHT ()

| | | |
|------------|----------|-----------------|
| FROM _____ | TO _____ | EVERY _____ MIN |
| _____ | _____ | _____ |
| _____ | _____ | _____ |
| _____ | _____ | _____ |
| _____ | _____ | _____ |
| _____ | _____ | _____ |
| _____ | _____ | _____ |
| _____ | _____ | _____ |

SPECIAL OUTPUT TIMES: (✓)

$\beta = 90$ ()
 MIN , MAX. ALTITUDE ()
 SPECIAL LATITUDES ()
 SPECIAL LONGITUDES ()
 SPECIAL ALTITUDES ()
 OBSERVATION TIMES ()

SPECIAL

| LAT. | LONG. | ALT. |
|-------|-------|-------|
| _____ | _____ | _____ |
| _____ | _____ | _____ |
| _____ | _____ | _____ |
| _____ | _____ | _____ |
| _____ | _____ | _____ |

OUTPUT REQUESTED: (✓)

STANDARD

a) EVERY TIME ()
 b) NOOES ONLY ()

ECLIPSING

a) STANDARD ()
 b) OPTIONAL ()

ELEMENTS

a) EVERY TIME ()
 b) NOOES ONLY ()

VARIATIONAL EQUATIONS

a) STANDARD ()
 b) OPTION B ()
 c) OPTION C ()

GEOMAGNETIC LAT. AND LONG. ()
 SUN-MOON ANGLES

a) STANDARD ()
 b) OPTION Y ()
 c) OPTION Z ()

GROUND TRACK TAPE ()
 DIFFERENCE TAPE ()

TRACE66

COVARIANCE ANALYSIS SPECIFICATIONS

ALL PARAMETERS MUST BE SPECIFIED ON THE TRACE66 PARAMETER SPECIFICATION FORM.

OBSERVATION GENERATION SPECIFICATIONS MUST BE SUPPLIED ON THE TRACE66 DATA GENERATION SPECIFICATIONS - SHEET 1.

IF OBSERVATIONS ARE TO BE INPUT RATHER THAN GENERATED, INDICATE THE SOURCE

() CARDS

() CARD IMAGE TAPE

() BINARY OBSERVATION TAPE

IF CARDS OR A CARD IMAGE TAPE ARE BEING USED AND THE OBSERVATION DATA TO BE USED IS A SUBSET OF THE DATA PROVIDED, THE BEGINNING AND END OF THE INTERVAL TO BE USED ARE GIVEN BY:

BEGINNING YEAR _____ MONTH _____ DAY _____ HOUR _____ MIN _____ SEC _____
 END YEAR _____ MONTH _____ DAY _____ HOUR _____ MIN _____ SEC _____

STATION INPUTS: η_E AND η_R ARE THE INDICES OF REFRACTION USED TO COMPUTE REFRACTION CORRECTIONS FOR ELEVATION AND RANGE DATA. A "V" INDICATES THE NOMINAL VALUES ARE TO BE USED, A "O" INDICATES NO CORRECTIONS, AND IF A NON-STANDARD INDEX IS TO BE USED, IT MUST BE PROVIDED.

| STA
NAME | LAT
(DEG) | LONG
(DEG) | HEIGHT
(FEET) | INTERFEROMETER
P Q | η_E
(112×10^{-6}) | η_R
(150×10^{-6}) |
|-------------|--------------|---------------|------------------|-----------------------|--------------------------------------|--------------------------------------|
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |

OBSERVATION WEIGHTS (σ^2 's):

| STA | DATA
TYPE | σ | DATA
TYPE | σ | DATA
TYPE | σ |
|-----|--------------|----------|--------------|----------|--------------|----------|
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |
| | | | | | | |

OUTPUT TIMES: TIMES ARE GIVEN IN MINUTES FROM EPOCH () OR MIDNIGHT ()

FROM _____ TO _____ EVERY _____ MIN

OUTPUT REQUESTED: () P Q

(P_0) = ($A^T A$)⁻¹ () ()
 CARTESIAN () ()
 ORBIT PLANE () ()
 SPHERICAL () ()
 ELEMENT () ()
 PERIOD, A PER () ()
 EQUINOCTIAL () ()
 MEASUREMENT COVARIANCE () ()
 PRINT $\partial P / \partial Q$ ()
 SAVE PLOT TAPE ()

IF A "V" IS USED THE ENTIRE COVARIANCE MATRIX WILL BE PRINTED. IF A "D" IS USED, ONLY THE SQUARE ROOT OF THE DIAGONAL WILL BE PRINTED.

INPUT A PRIORI UNCERTAINTIES

NO A PRIORI INFORMATION
 $A^T A$ MATRIX GIVEN
 $(A^T A)^{-1}$ MATRIX GIVEN
 σ^2 's GIVEN
 $C(Q)$ MATRIX GIVEN

P PARAMETER

()
 ()
 ()
 ()
 ()

Q PARAMETER

()
 ()
 ()
 ()
 ()

TRACE66
DATA GENERATION SPECIFICATION SHEET 1

| STATIONS | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
|--|-----|-------|-------|-------|-------|-------|-------|-------|-------|
| SUPPLY VALUES FOR | | | | | | | | | |
| Δt (SEC) | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| E MIN (DEG) | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| E MAX (DEG) | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| R MAX (NM) | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| START TIME | | | | | | | | | |
| FROM | DAY | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| MIDNIGHT | HR | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| OF EPOCH | MIN | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| STOP TIME | | | | | | | | | |
| FROM | DAY | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| MIDNIGHT | HR | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| OF EPOCH | MIN | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| A_1 (DEG) | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| A_2 (DEG) | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| INDICATE THE REQUESTED DATA WITH A "✓" | | | | | | | | | |
| RANGE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| AZIMUTH | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| ELEVATION | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| RANGE RATE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| INTERFEROMETER \dot{P} | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| INTERFEROMETER \dot{Q} | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| INTERFEROMETER P | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| INTERFEROMETER Q | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| AZIMUTH RATE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| ELEVATION RATE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| f_r | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| LATITUDE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| LONGITUDE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| SURFACE RANGE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| HEIGHT | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| DOPPLER RATE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| LOOK ANGLE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| KAPPA | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| ASPECT ANGLES | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| ATTENUATION | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| δ, γ, ϵ | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| TOPOCENTRIC RT. | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| ASC. AND DEC. | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| GEOCENTRIC RT. | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| ASC. AND DEC. | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| HOOR ANGLE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| u, v | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| \hat{A} | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| \hat{E} | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| TWO-WAY DOPPLER | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| ANTENNA X, Y ANGLES | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| TRANET DOPPLER | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| GEOCEIVER RANGE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| Ranging or Diff(s) | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |
| SGLS RANGE RATE | | _____ | _____ | _____ | _____ | _____ | _____ | _____ | _____ |

| SYMBOL | DEFINITION |
|-----------|---|
| R | Range |
| AZ | Azimuth |
| EL | Elevation |
| \dot{R} | Range rate |
| Ax, Ay | Antenna angles |
| V2 | Vehicle to vehicle range |
| V2D | Vehicle to vehicle range rate |
| S2 | Station to vehicle to vehicle range sum |
| S2D | Station to vehicle to vehicle range rate sum |
| S3 | Station to vehicle to vehicle to vehicle range sum |
| S3D | Station to vehicle to vehicle to vehicle range rate sum |
| V3 | Vehicle to vehicle to vehicle range sum |
| V3D | Vehicle to vehicle to vehicle range rate sum |
| TDOA | Time difference of arrival |
| TOA | Time of arrival |
| 3WR | Three way range |
| MP | Multi-path |

[illegible]

STATION CARDS

1. THE LOCATION FIELDS MUST HAVE A DECIMAL POINT.
2. THE EXPONENT FIELDS ARE OPTIONAL, BUT IF USED MUST BE OF THE FORM $\pm XX$.

| PROGRAMMER | | KEYPUNCHED | | VERIFIED | | DATE | | PAGE | | OF | |
|--|--|--|----------|----------|---|------|---|------|----|----|----|
| ST | 1 2 3 | I | 5 | E | 7 | R | 9 | D | 11 | T | 13 |
| FIELD 1 | | FIELD 2 | | FIELD 3 | | EXP. | | EXP. | | Q | |
| 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 | 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 | 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 | 64 65 66 | 68 69 70 | | | | | | | |

TRACE - 66: SENSOR PARAMETER CARDS

1. THE INITIAL VALUE, BOUND AND SIGMA FIELDS MUST HAVE A DECIMAL POINT
2. THE EXPONENT FIELDS ARE OPTIONAL, BUT IF USED MUST BE OF THE FORM .XX.

| PROGRAMMER | | KEYPUNCHED | | VERIFIED | | DATE | | PAGE | | OF | |
|---|---------------|------------|----|--|-----|--|-----|--|-----|----|--|
| ST | PASS | NAME | Q | INITIAL VALUE | EXP | BOUND | EXP | SIGMA | EXP | | |
| 1 2 3 4 5 6 7 | 1 2 3 4 5 6 7 | 9 10 11 12 | 14 | 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 | | 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 | | 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 | | | |
| <div style="display: flex; justify-content: space-between;"> <div style="width: 20%;"> <p>1 2 3 4 5 6 7</p> </div> <div style="width: 20%;"> <p>9 10 11 12</p> </div> <div style="width: 20%;"> <p>16 17 18 19 20 21 22 23 24 25 26 27 28 29 30</p> </div> <div style="width: 20%;"> <p>32 33 34 35 36 37 38 39 40 41 42 43 44 45 46</p> </div> <div style="width: 20%;"> <p>48 49 50 51 52 53 54 55 56 57 58 59 60 61 62</p> </div> </div> | | | | | | | | | | | |

PROGRAMMER _____ KEYPUNCHED _____ VERIFIED _____ DATE _____ PAGE _____ OF _____

| | | | | |
|---|---|---|--|----|
| 1 | 2 | 7 | | ?? |
| H | 1 | | | |

[illegible]

VEHID VEHICLE NUMBER
0 ≤ VEHID ≤ 9999

TZNE/HR/MIN/SEC: EPOCH TIME

| | | | | | | |
|---|-------------|--------------|-----------|-------------|-------------|-----------|
| 1 | x , | y , | z , | \bar{x} , | \bar{y} , | \bar{z} |
| 2 | α , | δ , | β , | Λ , | r , | v |
| 3 | a , | e , | i , | Ω , | ω , | r |
| 4 | λ , | δ , | β , | Λ , | r , | v |
| 5 | h_p , | δ_p , | h_p , | h_a , | i , | z |
| 6 | a , | e , | i , | Ω , | ω , | μ |
| 7 | a_f , | a_s , | N , | L , | X , | Ψ |

$$x_{BF}, y_{BF}, z_{BF}, \dot{x}_{BF}, \dot{y}_{BF}, \dot{z}_{BF}$$

Negative value of ICTYP indicates that initial conditions are in internal units.

NOTE: Above initial conditions refer to Earth as the central body. If $ICTYP = ICTYP + 10$, the above initial conditions refer to the Moon as the central body.

IDRAG: ATMOSPHERE MODEL

0 ARDC 1959
1 LOCKHEED JACCHIA
2 JACCHIA 1964
3 U. S. STANDARD 1962
6 LMSC 1967
7 EXPONENTIAL
8 CAMBRIDGE RESEARCH LABOP TORY
9 NWL

DRAG: $C_D A / W$ (FT² / LB)

2 IF THE EXPONENT IS TO BE USED IN THE $\mathbb{R}_{m \times n}$ FIELD, IT MUST BE OF THE FORM $\frac{p}{q} \times x$

PROGRAMMER -

1200922 1006 3978 984 567

| PROGRAMMER | | KEYPUNCHED | | VERIFIED | | DATE | | PAGE | | OF | |
|-----------------------|-----|------------|-----|----------|-----|------|-------|------|-----|-----|-----|
| RANGE | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| AZIMUTH | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| ELEVATION | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 |
| RANGE RATE | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 |
| P DOT | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 |
| Q DOT | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 |
| 0 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 |
| AZIMUTH RATE | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 |
| ELEVATION RATE | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 | 101 | 102 | 103 |
| DOUBLE DOTT | 104 | 105 | 106 | 107 | 108 | 109 | 110 | 111 | 112 | 113 | 114 |
| MUTUAL VISIBILITY | 115 | 116 | 117 | 118 | 119 | 120 | 121 | 122 | 123 | 124 | 125 |
| LATITUDE | 126 | 127 | 128 | 129 | 130 | 131 | 132 | 133 | 134 | 135 | 136 |
| LONGITUDE | 137 | 138 | 139 | 140 | 141 | 142 | 143 | 144 | 145 | 146 | 147 |
| SURFACE RANGE | 148 | 149 | 150 | 151 | 152 | 153 | 154 | 155 | 156 | 157 | 158 |
| HEIGHT | 159 | 160 | 161 | 162 | 163 | 164 | 165 | 166 | 167 | 168 | 169 |
| DOPPLER RATE | 170 | 171 | 172 | 173 | 174 | 175 | 176 | 177 | 178 | 179 | 180 |
| LOOK ANGLE | 181 | 182 | 183 | 184 | 185 | 186 | 187 | 188 | 189 | 190 | 191 |
| DISERVATION VARIANCES | 192 | 193 | 194 | 195 | 196 | 197 | 198 | 199 | 200 | 201 | 202 |
| KAPPA | 203 | 204 | 205 | 206 | 207 | 208 | 209 | 210 | 211 | 212 | 213 |
| ASPECT ANGLES | 214 | 215 | 216 | 217 | 218 | 219 | 220 | 221 | 222 | 223 | 224 |
| ATTENUATION | 225 | 226 | 227 | 228 | 229 | 230 | 231 | 232 | 233 | 234 | 235 |
| X, Y, Z | 236 | 237 | 238 | 239 | 240 | 241 | 242 | 243 | 244 | 245 | 246 |
| TOPOCENTRIC RA, O | 247 | 248 | 249 | 250 | 251 | 252 | 253 | 254 | 255 | 256 | 257 |
| GEOCENTRIC RA, O | 258 | 259 | 260 | 261 | 262 | 263 | 264 | 265 | 266 | 267 | 268 |
| HOURLY ANGLE | 269 | 270 | 271 | 272 | 273 | 274 | 275 | 276 | 277 | 278 | 279 |
| U, V | 280 | 281 | 282 | 283 | 284 | 285 | 286 | 287 | 288 | 289 | 290 |
| ACCELEROMETER | 291 | 292 | 293 | 294 | 295 | 296 | 297 | 298 | 299 | 300 | 301 |
| A DOUBLE DOTT | 302 | 303 | 304 | 305 | 306 | 307 | 308 | 309 | 310 | 311 | 312 |
| E DOUBLE DOTT | 313 | 314 | 315 | 316 | 317 | 318 | 319 | 320 | 321 | 322 | 323 |
| 3 WAY DOPPLER | 324 | 325 | 326 | 327 | 328 | 329 | 330 | 331 | 332 | 333 | 334 |
| ANTENNA | 335 | 336 | 337 | 338 | 339 | 340 | 341 | 342 | 343 | 344 | 345 |
| TRANSET | 346 | 347 | 348 | 349 | 350 | 351 | 352 | 353 | 354 | 355 | 356 |
| CODECIVER | 357 | 358 | 359 | 360 | 361 | 362 | 363 | 364 | 365 | 366 | 367 |
| SCLS | 368 | 369 | 370 | 371 | 372 | 373 | 374 | 375 | 376 | 377 | 378 |
| SAT. TRACKER DOPPLER | 379 | 380 | 381 | 382 | 383 | 384 | 385 | 386 | 387 | 388 | 389 |
| TIME OF ARRIVAL | 390 | 391 | 392 | 393 | 394 | 395 | 396</ | | | | |

**SIMULTANEOUS VEHICLE
DATA GENERATION II CARDS**

RENO SPACE FORM 4454 REV 4-71

1. A DECIMAL POINT MUST BE USED IN ALL FIELDS FLAGGED BY AN *.

ATMOSPHERE FROM 4448 REV 10-71

TRACE66 OBSERVATION DATA

1. A DECIMAL POINT MUST BE USED IN ALL FIELDS FLAGGED BY AN "D".

2. THE EXPONENT FIELDS ARE OPTIONAL, BUT IF USED, MUST BE OF THE FORM $\pm XX$.

CONTACT FROM 1990 BY B-7D